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## THESIS

AN INVESTIGATION INTO THE CONTROL  
LIMITATIONS OF A BANK TO TURN MISSILE  
IN THE TERMINAL HOMING PHASE

by

Barton P. Anderson

September 1984

Thesis Advisor:

M. D. Hewett

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An Investigation into the Control  
Limitations of a Bank to Turn Missile  
in the Terminal Homing Phase

by

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Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN AERONAUTICAL ENGINEERING

from the

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## ABSTRACT

The purpose of this thesis was to examine guidance and control deficiencies in a bank to turn (BTT) cruise missile with limited roll authority in the terminal homing phase of its mission. A six degree of freedom simulation of a typical BTT missile was translated into FORTRAN H from the Continuous System Modelling Program (CSMP) simulation language and run on the IBM System 370 computer. Tests were conducted with the revised simulation program to examine the effects of electronic countermeasures (ECM) blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. In addition to the standard attack profile involving a popout attack, several other attack profiles were tested including skid-to-turn (STT) control laws and a ballistic trajectory. Miss distances varied from 3.7 feet without ECM or glint to 85 feet with ECM operating. Susceptibility of the missile to ECM blinking varied with the blinking frequency. The largest miss distances occurred with ECM frequencies below 0.2 Hz and near 6.0 Hz. Analysis of the data showed that errors at the low frequencies were primarily caused by the bank command loop of the autopilot. Those at the higher frequency were due to the roll rate command loop. Variation of the geometry of the missile's flight profile had no significant impact upon missile accuracy except that, without a popup maneuver, the roll rate channel demonstrated a marked decrease in effectiveness. Variation of the autopilot gain in the roll rate control loop changed the frequency at which degradation occurred but actually increased its effects. Skid to turn control laws were tested

however the missile was unable to produce the necessary sideforce needed to track a passive target and produced undesirable coupling in the flight controls. An attempt to use the altitude command channel to fly a ballistic profile was unsuccessful due to instabilities created in the control system. It is recommended that a popup maneuver be included in the terminal guidance of a BTT cruise missile and that further tests be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a BTT missile.



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## I. INTRODUCTION

### A. BACKGROUND

Bank-To-Turn (BTT) control is utilized extensively on missiles which must cruise for long ranges within the atmosphere. These missiles utilize a primary lifting surface (wing) and smaller controlling surfaces as on a conventional airplane. This method has two primary advantages. First, the wing provides lift to support the missile's weight at a relatively high efficiency thereby permitting longer ranges for a given size engine and fuel load. Second, the lift vector can be positioned by banking the missile to provide large lateral accelerations resulting in excellent turn performance. Certain BTT cruise missile configurations, however, use differential tail for roll control as opposed to ailerons and suffer from poor roll rate and acceleration performance. It is the investigation into the control limitations of a BTT cruise missile configured this way in the terminal homing phase which is the subject of this thesis.

### B. STATEMENT OF THE PROBLEM

In order to provide compact storage of a BTT missile, the main wings are usually folded back and designed to snap into position as the missile emerges from its cannister at launch. Because of this feature, it is generally not feasible to install roll control devices at the extremities of the wings. Roll control is normally provided by differential actuation of the tail fins of the missile. Because of their short moment arm and small area and because the main wing has a relatively large degree of roll damping, BTT missiles are limited in their ability to roll rapidly.

Because of the need to bank the missile in order to align its lift vector in the desired direction it has been suggested that the requirement for rapid roll maneuvering in the terminal phase of flight would limit the accuracy of the missile. In addition, natural fluctuations in the position of the radar target, known as glint, and artificial fluctuations due to the presence of electronic countermeasures (ECM) might further degrade the performance of a ETT missile.

## C. MISSION SCENARIO

### 1. Control Configuration

The missile simulated in this thesis is a hypothetical bank to turn cruise missile with limited roll control authority. Its design incorporates characteristics typical of many similar designs. The missile is equipped with a standard rudder for yaw control and stabilators for both roll and pitch control. Inner loop closures for stabilization and command are included in the simulation. Command loop closures consist of normal acceleration, bank angle, and lateral acceleration. The lateral acceleration command system can be used as a turn coordinator in the bank-to-turn mode (normal) mode or as a lateral load factor (NY) command system in a skid-to-turn mode. Outer loop closures are provided for altitude and flight path angle. The autopilot control loop design is presented in detail in [Ref. 1].

### 2. Target

The target is assumed to be a surface combatant ship located initially 24,000 feet due North from the missile and moving East at a constant speed of 20 knots. It is assumed that the missile seeker tracks an aim point perfectly. The aim point is located nominally 10 feet above the ship's

waterline and amidships. This aim point continually shifts as a function of ECM blinking and a random glint simulation.

### 3. ECM Simulation

The ECM blinker simulation shifts the radar target seen by the missile's seeker forward and aft from the true target aim point by  $\pm 75$  feet along the ships longitudinal axis at a specified frequency. The aim point is simultaneously shifted vertically  $\pm 10$  feet at the same frequency.

### 4. Attack Profiles

The attack profile used as a baseline for this simulation began at 50 feet of altitude at a speed of Mach 0.75. The missile tracked toward the target using proportional navigation in azimuth and altitude hold at 50 feet. At a range of 18000 feet the missile rolled to 60 degrees of bank and turned away from the target to the right until the target line of sight was offset by 10 degrees. When the offset was reached, the missile climbed to an altitude of approximately 250 feet and then dove toward the target using proportional navigation in both azimuth and elevation. This mission profile is often referred to as a popout attack.

Variations of this mission included eliminating the 10 degree offset turn and/or the climb to altitude and substituting skid-to-turn control laws for some phase of the mission. A ballistic altitude profile was also attempted.

## D. EXISTING WORK

In order to examine the existence of such problems and to test several proposed solutions, a six degree of freedom simulation of a typical BTT cruise missile was produced by LCDR Kent Watterson and published in [Ref. 1]. This simulation was produced using the IBM Continuous System Modelling



Program (CSMP III) simulation language. A detailed description of this language and its constructions is presented in [Ref. 2] and [Ref. 3]. The simulation included dynamics, autopilot, guidance and mission profiles. It did not represent any specific missile but, rather, included characteristics typical of missiles configured in this way. In order to overcome limitations imposed upon the simulation program by the available computer installation, this CSMP program was rewritten in extended FORTRAN H. This allowed greater flexibility and full utilization of the DISSPLA graphics programming package available at NPS. A complete copy of the program listing is presented in Appendix D.

#### F. SCOPE OF TESTS

The tests conducted with the revised simulation program were limited to examining the effects of ECM blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. Alternate attack profiles using modified flight geometry and, in some cases, skid-to-turn control laws were also tested. A listing of the different flight profiles examined is presented in table I.

For all flight tests of the missile, certain parameters were held constant. A list of these values is presented in table II.

TABLE I  
Missile Attack Profile Test Configurations

	OFFSET TURN	POP-UP	ROLL RATE	TURN
BASELINE	X	X	0.5	BTT
II		X	0.5	BTT
III			0.5	BTT
IV		X	0.1	BTT
V		X	0.5	STT
VI		X	0.5	*

\* 90 degree bank on ballistic terminal trajectory

TABLE II  
Simulation Variables Held Constant

Variable Name	Value
*****	*****
Radar Burn-Through Range	500 ft
ECM Blinker Shifts:	
Longitudinal	± 75 ft
Lateral	± 00 ft
Vertical	± 10 ft
Baseline guidance scheme:	
Offset	10 deg
Popup Altitude	100 ft
Popup Range	18000 ft
Roll rate limit	75 dps
*****	*****

## II. PROGRAM DESCRIPTION

### A. INTEGRATION OF THE EQUATIONS OF MOTION

This simulation uses the linear, six degree of freedom equations of flight developed by Roskam in [Ref. 5:vol 1] and modified by Hewett in [Ref. 4]. The CSMP program developed by Watterson [Ref. 1] used a variable step Runge-Kutta integration method. The FORTRAN translation program uses a

$$\text{INTEGRAL}(\text{YDOT DT}) = Y + (\text{YDOT}) * \text{DT} \quad (\text{eqn 2.1})$$

simple Eulerian integration which is given by equation 2.1. The incremental time element, DT, is fixed at 0.01 seconds and the integration period lasts for less than 30 seconds.

### B. PROGRAM NOMENCLATURE

A detailed description of the nomenclature used throughout the simulation program is presented in Appendix C. The variable names used in the FORTRAN translation are, with few exceptions, the same as those used in the CSMP simulation.

### C. AXIS SYSTEM

The simulation uses a right handed earth reference frame where the x-axis points North, the y-axis points East and the z-axis points down. However, altitude and vertical velocity are always given as positive upwards (i.e. ALTITUDE = -Z). For plotting the geographical track in the output routines, the axes are transformed so that the X,Y, and Z axes point East, North and upward, respectively.

## D. PROGRAM ARCHITECTURE

The FORTFAN simulation program consists of an executive program which calls seven major subroutines which are briefly described as follows.

### 1. Executive Program

The main calling program is short and handles only three tasks. It increments the TIME variable for each integration cycle. It calls the output data storage routine, PREPAR, at the specified output interval and it controls the execution of multiple flights within a single program run changing one or more key variables between the runs.

### 2. Subroutine INIT

This subroutine contains a small section of executable statements which resets variables to their initial value when more than one flight is flown during a program run. Included with this subroutine is the BLOCK DATA subroutine which must be used to initialize all variables in named common areas. The majority of the BLOCK DATA subprogram is taken up with arrays listed in table form which contain the aerodynamic coefficient data for the missile. Static coefficients which are functions of one variable are shown in figures A.2 through A.9 Static coefficients which are functions of two parameters are presented in figures A.10 through A.13 Dynamic coefficients are assumed to be constant and are not presented graphically.

### 3. Subroutine MISSN

This subroutine dictates the mission profile. It is divided into sections which activate in sequence as the mission progresses. Each section takes the flight dynamics data for the missile, compares it with the target

acquisition data (generated in subroutine TGTNAV) and outputs vertical and horizontal acceleration commands in the geographic earth reference frame. These in turn are translated into commanded bank angle and normal load factor for the missile according to equations 2.2 and 2.3. A diagram

$$PHIC = ARCTAN (AYC/AZC) \quad (\text{eqn 2.2})$$

$$NZC = AZC \cos (PHI) + AYC \sin (PHI) \quad (\text{eqn 2.3})$$

of these vectors is given in figure A.1. Different terminal attack profiles are implemented using variations of this subroutine, MISSN1 and MISSN2, which are presented in Appendices E and F.

#### 4. Subroutine APILOT

This subroutine takes the commanded normal load factor and bank angle and applies them to the missile autopilot system. A detailed discription of the design of the missile's autopilct is presented in reference [Ref. 1]. The output of the control system is delivered in terms of conventional airplane elevator, aileron and rudder control positions. These are mixed to obtain the commanded missile fin positions. The control limits of  $\pm 15$  degrees are applied to the fins and these controls are then unmixed to obtain the limited conventicnal control positions. The dynamics of the servc actuators that move the tail surfaces are modelled as a first order real pole. Although CSMP-III provides macros that perform the simulation of many types of transfer functions within the control system only the first order real pole transfer function was necessary for this program. It is modelled in the FORTRAN translation using subroutine REALPL, presented in the program listing in Appendix C.



## 5. Subroutine AEFC

Subroutine AEFC uses two table lookup routines to retrieve the aerodynamic coefficients from the data presented in figures A.2 through A.18. Linear interpolations are used to obtain values between given parameters. Error messages are printed when the input parameters are outside the bounds of the data in the lookup table and these are suppressed after about 5 successive integration cycles. AEFC completes the buildup process, uses these data to compute the forces and moments on the aircraft and then integrates the equations of motion to update all of the aircraft's flight parameters and position information.

## 6. Subroutine TGTNAV

The TGTNAV subroutine navigates the target vessel on a course of East at a steady speed of 20 knots. It shifts the position of the radar target relative to its real position according to the ECM and GLINT parameters. The GLINT offset is produced by multiplying the GLINT shift in each axis by a random number between -1 and 1. The GLINT offset is calculated every output interval rather than 100 times per second. The ECM offset is switched according to the sign of a sine wave which runs at the ECM blinking frequency, FREQ. These offsets are then added to the actual target position to produce the radar target position. Line of sight angles and rates are calculated from this information with the assumption that the seeker has perfect pointing capability.

## 7. Subroutine PREPAR

At intervals specified by the output counter, this subroutine is called and stores up to 20 variables in a large array call PTS. The output interval used for all tests

was 0.20 sec. The PTS array is passed to the output routines when the simulation run is completed. This subroutine also converts output variables from radian to degree format and, in the final attack phase, calculates four error functions. These error functions are time averaged differences between commanded variables (e.g. PANK or ROLL RATE) and their actual counterparts. These are later used to analyse the performance of the control system under various conditions.

#### 8. Subroutine OUTPUT

OUTPUT produces 3 forms of output information. The primary data output lists the value of MISDST (the distance at which the missile passed the target at its closest approach), the value of the error functions at the end of the mission, and the ranges of all the variables stored. These data are also printed to another file followed by the full contents of the PTS array in tabular form. This gives a numerical history of all the output variables from the start to the finish of the mission. (Normally, to save disk space, this file was routed to a dummy variable. It was needed only when detailed data histories of a portion of the mission were required.)

CUTPUT also calls the necessary DISSPLA routines to print graphs of the output variables. The independent variable in six graphs is TIME. In the seventh graph the positions of the missile and the target ship are plotted in three dimensional space for each output interval. Each of the graphs in this subroutine are controlled by the setting of 7 flags in the first column of the data statement at the beginning of the routine (0 to pass over and 1 to plot).

### III. BASELINE ATTACK CONFIGURATION

#### A. AUTOPILCT ROLL RATE COMMAND LOOP ADJUSTMENT

Initial testing of the simulation was conducted on the CSMP version of the program. The frequency of the ECM blinker was varied from 0.2 Hz to a maximum of 2.0 Hz and the roll performance of the missile was graphed. Figure A.19 shows the commanded roll rate and actual roll rate plotted against time for the duration of a thirty second flight straight toward the target at a constant altitude of 50 feet. The target's radar position was blinked at a rate of 0.4 Hz and roll rate command was limited to 75 degrees per sec. In the figure, the command oscillations increased in magnitude as the target range decreased and, after 24 seconds, the autopilot commanded the maximum rate with every shift of the target's apparent position. While the commanded roll rate remained at 75 degrees per second, the actual roll rate never exceeded 35 degrees per second. Figure A.20, which plots the fin positions as a function of time, shows that the fin servos never used more than 3 degrees (of the maximum 15) of travel in either direction. To remedy this problem, the missile autopilot roll rate command loop gain (KRCLET in the program) was increased from 0.1 to 0.5. The value of this gain had been set by Watterson [Ref. 1] using root locus based upon the perturbation equations of motion [Ref. 4] in steady state level flight. Figures A.21 and A.22 show the results of a subsequent run with the revised guidance loop. Steady state error in roll rate was significantly reduced and the full range of available flight controls ( $\pm 15$  deg.) was used. This difference in the autopilot was incorporated into the baseline program and remained throughout all subsequent tests.

## E. BASELINE PROGRAM

In order to provide a baseline performance record against which to examine the effects of ECM and glint and/or alternate attack profiles on the accuracy of the missile and the performance of its control system, a standard, pop-out attack with an offset turn was selected and flown and is used as a standard for comparison. The parameters which apply to this baseline are listed in table II. Figures A.23 through A.28 are a complete record of the baseline program run without any ECM or glint offsets applied to the target. Figures A.29 through A.35 are a complete record of the baseline program run with the ECM blinker operating at 0.2 HZ and the glint feature operating. The complete tabular data output from this latter run is presented in Appendix B.

#### IV. FREQUENCY SCAN TESTS

##### A. ERROR FUNCTIONS

For testing the effects of glint and ECM at various blinking frequencies against the control system of the missile, a quantitative measure of the system's effectiveness was needed. Four error functions were developed for this purpose. The time weighted difference between the commanded value and the actual value of a variable was computed according to equation 4.1. This time weighted error was summed over all of the time intervals and divided by the

$$ERR = DT * ABS(COMMAND - VARIABLE) \quad (\text{eqn 4.1})$$

total time to produce the error function for the variable. The variables for which these functions were computed are

TABLE III  
Error Function Variables

VARIABLE	COMMAND VARIABLE
*****	*****
1. BANK	BANK
2. ROLL RATE	ROLRT
3. AZIMUTH LOS RATE	0.0
4. ELEVATION LOS RATE	0.0
*****	*****

listed in Table III. In the terminal phase where proportional guidance is used in both the azimuth and elevation channels, the commanded azimuth and elevation angle rates are zero to produce a constant bearing intercept.



## B. ECM PHASING

At low frequency blinking rates, the phase of the ECM blinker at the start of the mission had a very large effect on the miss distance. To minimize the distortion of the data due to this effect, a phase variable was added to the ECM generator to change the phase of the blinker at the start of each run. Four runs were conducted at each frequency using values of 0.0,  $\pi/2$ ,  $\pi$ ,  $(3/2)\pi$  for the phase variable. The data for each frequency were averaged to get mean values for the miss distance and each error function.

## C. BASELINE TEST RESULTS

### 1. ECM Frequency Scans

Four simulated flights were conducted at each frequency from 0.0 to 30 Hz. Glint was disabled for the course of these tests. The attack profile flown was the baseline popout attack mission. A graph of the mean value of the miss distance (MISDST) versus frequency is presented in figure A.36. The data show that maximum miss distance occurs in the very low frequency range of the order of 0.2 Hz and again to a lesser degree in the vicinity of 6 Hz. Figures A.40 and A.44 are plots of the error function means against frequency for the autopilot command errors and the tracking errors respectively. These data show that the bank angle command loop is susceptible to ECM frequencies of the order of 0.2 Hz while the roll rate command loop is primarily responsible for the errors that occur at the higher frequencies in the range of 5 to 10 Hz. Figure A.44 also demonstrates that the time averaged tracking errors follow the same basic pattern.

Figures A.48 through A.53 demonstrate these effects in flight. Figures A.48 and A.51 show the bank angle and

roll rate performance of the baseline missile without ECM. Both variables track closely to their commanded values with the exception of a small, steady state error in the rate channel which is most evident at large commanded rates. Figures A.49 and A.50 show the effects of ECM at 0.4 and 6.0 Hz upon the bank channel. In figure A.49 significant errors exist in bank as the system cannot keep up with the large, sudden changes in commanded bank caused by the ECM shift of the target. The bracket in figure A.49 is drawn between two corresponding points to emphasize the large lag present in the channel. Roll rate tracks close to its commanded level at this frequency.

At 6.0 Hz, figures A.52 and A.53 show the opposite effect. In figure A.53 the bracket emphasizes the large lag that exists in the aircraft roll response to the rapid changes in rate command. The bank command loop at this frequency has effectively filtered out most of the high frequency input.

The results of the frequency scan tests showed that the baseline BTT cruise missile simulated by the program was more susceptible to ECM frequencies in the vicinity of 0.2 and 6.0 Hz due to the excitation of the bank and roll rate command loops respectively. If distances greater than 20 ft from the center of the target are considered likely misses, then the excitation of the roll rate command loop did not produce enough error to cause a likely miss. The best results, from the target's point of view, will be obtained with low blinking frequencies in the vicinity of 0.2 Hz.

## 2. Effects of Glint

In order to isolate the effects of glint, the baseline configuration was flown without ECM or glint and again with glint only. Figure A.33 shows a trace of the random glint

displacement applied to the target's position as a function of time. Figures A.23 through A.28, which trace the missile's load factor, bank angle, roll rate and flight controls without glint, may be compared with figures A.54 through A.57 which show the same traces for the mission with glint.

The miss distance recorded without glint and an ECM phase of 0 was 3.7 feet. The distance measured with glint was 9.4 feet. Although these distances are very small compared with the miss distances achieved with ECM, the degradation induced by glint was large (154 percent) compared to the best obtainable value. Ways of minimizing the effect of random perturbations in the target position due to radar glint will make a significant improvement in the missile's accuracy in the absence of ECM and should be developed.

Since the miss distances without ECM and glint were very small compared to those obtained with very slow blinking frequencies (0.05 to 0.2 Hz), further tests should be run concentrating on ECM in the very low frequency range. These tests should obtain a much larger sample of ECM phases in order to best define the shape of the miss distance curve below 0.2 Hz.

#### D. ALTERNATE CONFIGURATION FREQUENCY SCAN RESULTS

##### 1. Mission Profile

Similar frequency scan profiles were flown using the MISSN1 (Appendix E) subroutine to generate the guidance commands for configurations II, III and IV. These attack profiles committed the offset turn and proceeded straight toward the target using proportional navigation in azimuth from start to finish. The popup maneuver was commenced at 15000 feet from the target. Of ranges from 20,000 to 5,000

feet which were tested, 15,000 feet produced the most consistent hits with a 200 foot popup altitude command. All subsequent tests of these missile attack configurations used 15,000 ft. popup range and a 200 ft. altitude command when the maneuver was performed.

An algorithm was added to the baseline proportional guidance scheme for the terminal phase which ensured that the missile rolled to place the nearest of the positive or negative Z-axis vectors on the direction commanded by the guidance system. This ensured that the missile would command negative load factor rather than trying to roll the missile upside down as it reached the apex of its climb. Azimuthal accelerations commanded by the guidance were still achieved by banking the missile except for configuration V.

A complete set of mission profile graphs for configurations II, III, and IV against a target with glint and ECM blinking at 0.2 Hz are presented in figures A.58 through A.75

## 2. Frequency Scan Results

### a. Miss Distances

Each configuration was flown against the target four times per test frequency. The tests covered a range of blinker frequencies from 0.05 through 30.0 Hz. The mean miss distances recorded are graphically presented as a function of frequency in figures A.37 through A.39. The results obtained were very similar to those obtained from the baseline configuration. There were two areas of higher than normal errors, one at low frequency below 0.2 Hz and another at a higher frequency near 6.0 Hz. Table IV compares the miss distances for each of the configurations.

The maximum values that occurred for all configurations appeared at the same frequencies with one



TABLE IV  
Maximum Miss Distances

CONFIGURATION	FREQ. RANGE (HZ)	LOCATION (HZ)	MAGNITUDE
BASLINE	0.20 - 20.0	$\leq 0.20$ 6.00	$\geq 45$ 22
II	0.05 - 21.0	$\leq 0.05$ 6.00	$\geq 75$ 17
III	0.10 - 30.0	$\leq 0.10$ 5.50	$\geq 75$ 17
IV	0.10 - 30.0	$\leq 0.10$ N/A	$\geq 75$ N/A

exception: changing the roll rate gain from 0.5 to 0.1 eliminated the maximum at the higher frequency. In addition, the magnitude of the errors did not differ significantly. (The baseline shows a smaller magnitude because the data do not extend below 0.2 Hz. while the other configurations were tested down to 0.1 and 0.05 Hz). Changing the attack geometry of the missile did not significantly alter its susceptibility to ECM jamming within the scope of these tests. Altering the gain of the roll rate command channel in the missile autopilot significantly decreased its susceptibility to ECM blinking at higher frequencies. Further testing should be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a bank to turn missile.

#### b. Autopilot Errors

Figures A.40 through A.43 graphically present the error functions for both the bank angle and roll rate command loops within the autopilot. These functions are representative of the ability of the missile to follow the



commands given it by the autopilot (the higher the function, the poorer the performance). As with the baseline configuration these figures demonstrate that the bank angle loop contributed most to the errors at low frequency and the roll rate loop contributed most at the higher frequency. Table V

**TABLE V**  
**Autopilot Errors**

CONFIGURATION	BANK ERROR		RATE ERROR	
	FREQ . (HZ)	MAGNI- TUDE	FREQ . (HZ)	MAGNI- TUDE
=====	=====	=====	=====	=====
BASLINE	0.4	0.22	7.0	0.19
II	0.6	0.17	8.0	0.18
III	0.5	0.18	8.0	0.27
IV	0.6	0.21	2.0	0.37
=====	=====	=====	=====	=====

is a summary of these graphs.

Magnitude of the bank error function and the frequency at which it occurred were not significantly altered in any one of the tested configurations. Changing the geometry of the attack had no effect on the frequency at which ECM was most effective against the roll rate control system, however the magnitude of the errors were increased by approximately 50 percent when the popup maneuver was eliminated (configuration III).

Decreasing the roll rate autopilot gain from 0.5 to 0.1 (configuration IV) moved the resonant frequency for the roll rate command system to a lower frequency but

increased the magnitude of the errors by more than 100 percent. This effect is reflected in the miss distance graphs (figures A.36 through A.39) in the disappearance of the distinct maximum at 6 HZ and a widening of the lower maximum (figure A.39). Altering the autopilot gain was effective at moving the resonant frequency to a different region but could not eliminate its effect.

### c. Tracking System Errors

Errors in the tracking loops are charted in figures A.44 through A.47. These errors follow the trends of the autopilot and miss distance errors. At the lower frequencies, azimuth performance was dominant while at higher frequencies the elevation tracking loop experienced the largest degradation.

## 3. Skid To Turn Guidance Results

The MISSN1 subroutine was further modified to allow the lateral load factor command variable, NYC, to be set according to guidance commands rather than being kept at zero for turn coordination purposes. The commanded bank angle was set to zero in the terminal phase in order to examine the effectiveness of lateral G command. No changes to the basic dynamics of the autopilot were made. The missile was flown in this configuration against a passive target. Figures A.76 through A.81 present the full data set from this test. The missile splashed into the water 99 feet left and short of the target. Once the missile came within 5 seconds of impact, cross coupling between the rudder channel and normal load factor, roll rate and bank can be seen in the figures. Although the rudder commands were never saturated, neither could the lateral load factor control loop create enough sideforce to follow the ship's lateral drift to the right. The addition of ECM and/or glint would have

only worsened the performance of the missile in this configuration. No further tests of this configuration were conducted. The use of skid-to-turn control laws could not produce sufficient sideforce to adequately follow a passive crossing target and produced excessive coupling into the longitudinal and lateral flight controls of the missile.

#### 4. Ballistic Trajectory

Because the majority of the apparent target shift with ECM blinking occurs in the horizontal plane, an attempt was made to place the missile on a ballistic trajectory and then roll the aircraft to 90 degrees angle of bank until impact using the primary load factor to follow the ECM target and lateral load factor to maintain the ballistic trajectory. In order to fly the ballistic trajectory, the altitude hold system was driven by a commanded altitude slaved to a parabolic trajectory derived from the missile's vertical speed and range to the target according to equation

$$ALT = HMDOT * RANGE / V_H + (G/2) * (RANGE / V_T)^2 + 10 \quad (\text{eqn 4.2})$$

4.2. where HMDOT,  $V_H$  and  $V_T$  are the vertical, horizontal and total speeds of the missile. The controlling subroutine used for this mission was MISSN2 and is presented in Appendix F.

Figures A.82 through A.85 show that the addition of the dynamics of the altitude command loop made the missile's control system unstable. Oscillations to the limits occurred in normal load factor and in roll rate. Considerable cross coupling occurred between the lateral-directional and longitudinal dynamics of the missile. The attempt to fly a ballistic trajectory using the existing altitude control system was unsuccessful. In order to fly the attempted profile, a major redesign of the missile's autopilot would be necessary.

## V. CONCLUSIONS

The conclusions listed below were derived from analysis of the results of simulated flights conducted using the baseline popout attack profile configuration, three variations of the baseline attack, a skid-to-turn control configuration and a ballistic altitude trajectory.

### A. BASELINE CONFIGURATION TESTS

At low frequency blinking rates, the phase of the ECM blinker had a very large effect on the miss distance.

The best obtainable performance for the baseline mission without ECM or glint was a miss distance of 3.7 feet. The addition of GLINT produced a miss distance of 9.7 feet, a degradation of 154 percent.

The bank angle command loop of the missile autopilot in the baseline configuration was especially susceptible to ECM frequencies of the order of 0.2 Hz while the roll rate command loop was primarily affected at the higher frequencies in the range of 5 to 10 Hz. The time averaged tracking errors also followed the same basic pattern.

If distances greater than 20 ft from the center of the target are considered likely misses, then the excitation of the roll rate command loop did not produce enough error to cause a likely miss. The best results, from the target's point of view, will be obtained with low blinking frequencies in the vicinity of 0.2 Hz.

### B. ALTERNATE ATTACK PROFILE CONFIGURATIONS

In terms of the average miss distances measured, changing the flight geometry of the missile did not signifi-



cantly alter its susceptibility to ECM jamming within the scope of these tests.

Altering the gain of the roll rate command channel in the baseline missile autopilot significantly decreased its susceptibility to ECM blinking at higher frequencies.

Changing the geometry of the attack had no effect on the magnitude of the bank error function and the frequency at which its maximum occurred.

Changing the roll rate gain from 0.5 to 0.1 had no noticeable affect on the magnitude of the bank error function and the frequency at which its maximum occurred.

Changing the geometry of the attack had no effect on the frequency at which ECM was most effective against the roll rate control system, however the magnitude of the errors were increased by approximately 50 percent when the popup maneuver was eliminated (configuration III).

Decreasing the roll rate autopilot gain from 0.5 to 0.1 (configuration IV) moved the resonant frequency for the roll rate command system to a lower frequency but increased the magnitude of the errors by more than 100 percent. This effect was reflected in the miss distance data by the disappearance of the distinct maximum at 6 HZ and a widening of the lower maximum. Altering the autopilot gain was effective at moving the resonant frequency to a different region but could not eliminate its effect and, in this case enlarged it.

Errors in the azimuth and elevation tracking loops closely followed the trends of the autopilot and miss distance errors. At the lower frequencies, azimuth performance was dominant while at higher frequencies the elevation tracking loop experienced the largest degradation.



#### C. SKID TO TURN CONTROL

The use of skid-to-turn control laws could not produce sufficient sideforce to adequately follow a passive crossing target and produced excessive coupling into the longitudinal and lateral flight controls of the missile.

#### D. BALLISTIC ATTACK PROFILE

The attempt to fly a ballistic trajectory using the existing altitude control system was unsuccessful. In order to fly the attempted profile, a major redesign of the missile's autopilot would be necessary.

## VI. RECOMMENDATIONS

Ways of minimizing the effect of random perturbations in the target position due to radar glint will make a significant improvement in the missile's accuracy in the absence of ECM and should be developed.

Further testing should be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a bank to turn missile.

Since the elimination of a popup increased roll rate errors by 50 percent, a popup profile is recommended for the terminal phase of a BTT cruise missile. Further testing should be conducted to determine the effects of different popup profiles on the susceptibility of the roll rate command system to ECM blinking.

Since the miss distances without ECM and glint were very small compared to those with very slow blinking frequencies (0.05 to 0.2 Hz), further tests should be run concentrating on ECM in the very low frequency range. These tests should obtain a much larger sample of ECM phases in order to best define the shape of the miss distance curve below 0.2 Hz.

APPENDIX A  
FIGURES

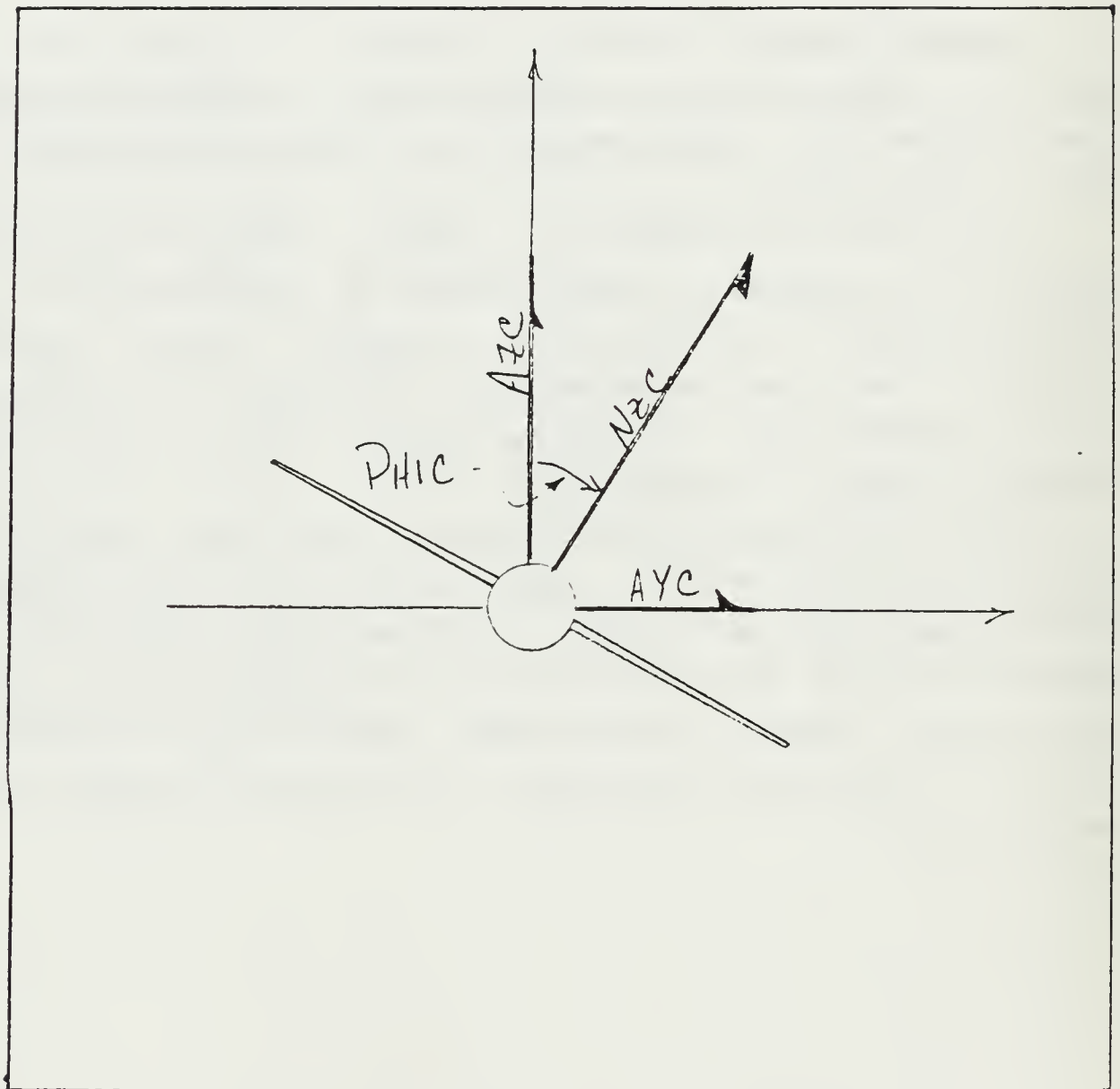


Figure A.1 Load Factor Commands.

# STATIC AERODYNAMIC COEFFICIENTS

## LIFT COEFFICIENT DATA

BASIC CL VS. AOA

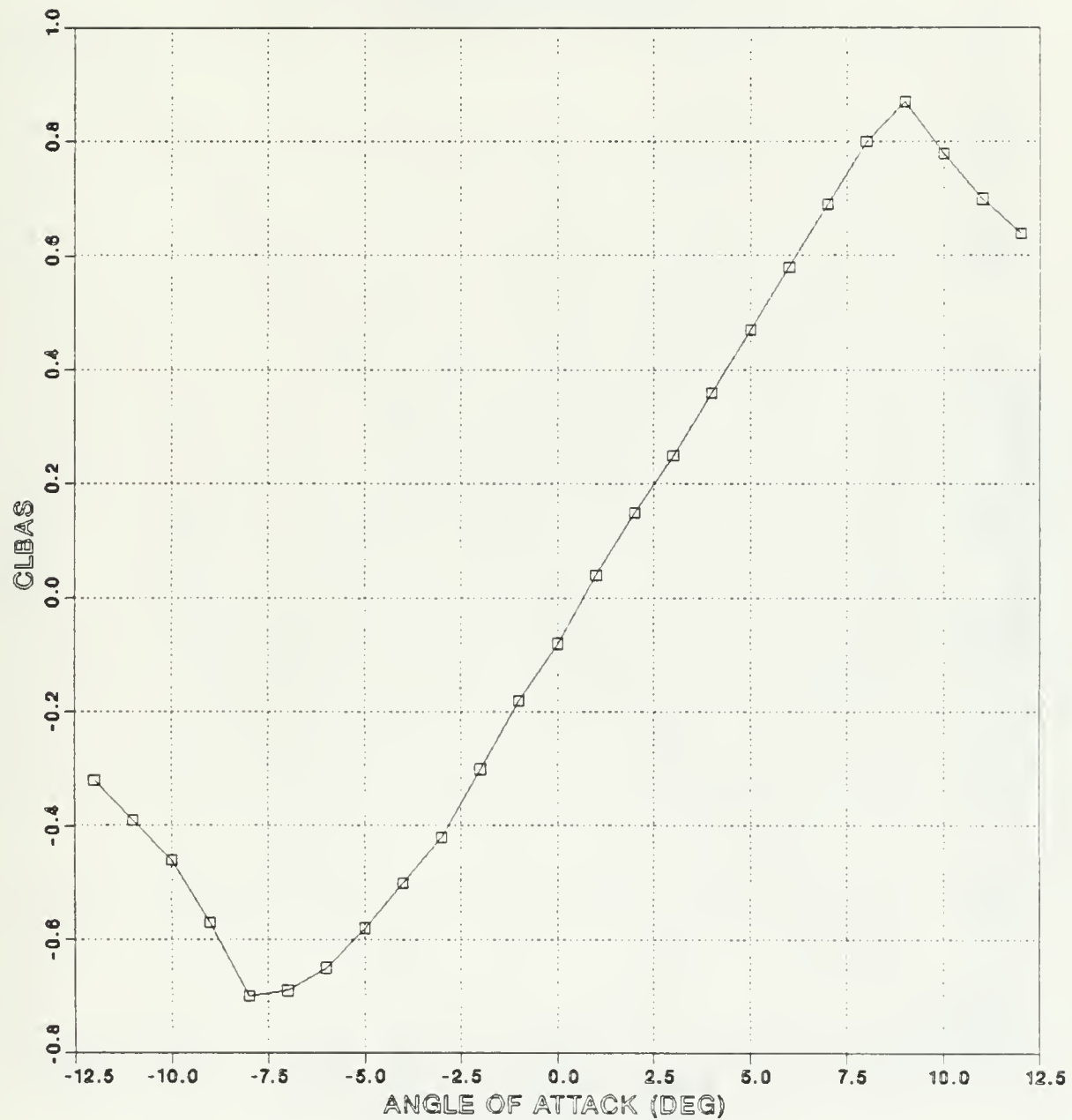


Figure A.2 Data Array LFT1.

STATIC AERODYNAMIC COEFFICIENTS

LIFT COEFFICIENT DATA

DELTA CL VS SYMMETRIC STABILATOR

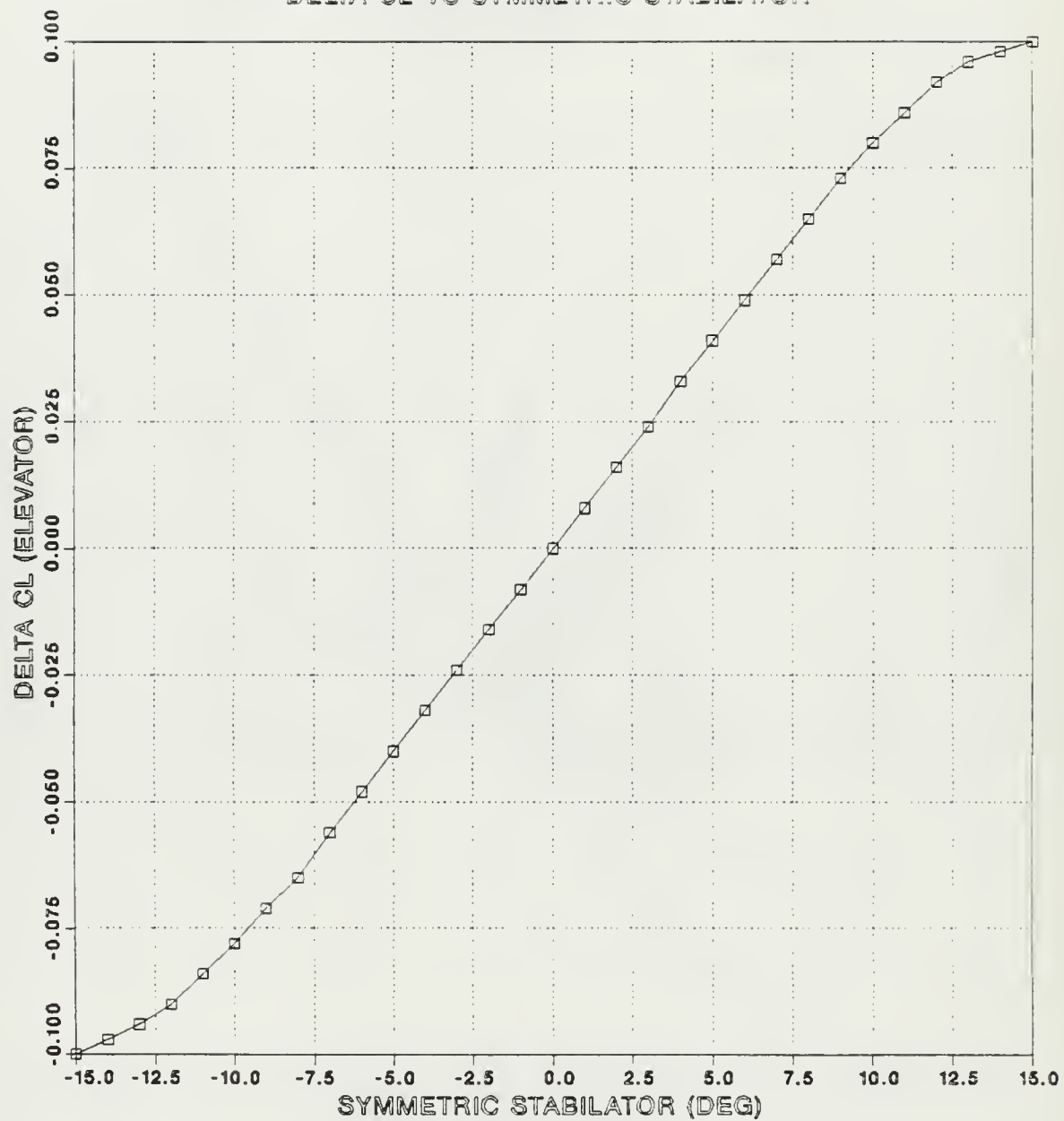


Figure A.3 Data Array LFT2.



STATIC AERODYNAMIC COEFFICIENTS

DRAG COEFFICIENT DATA

BASIC CD VS. AOA

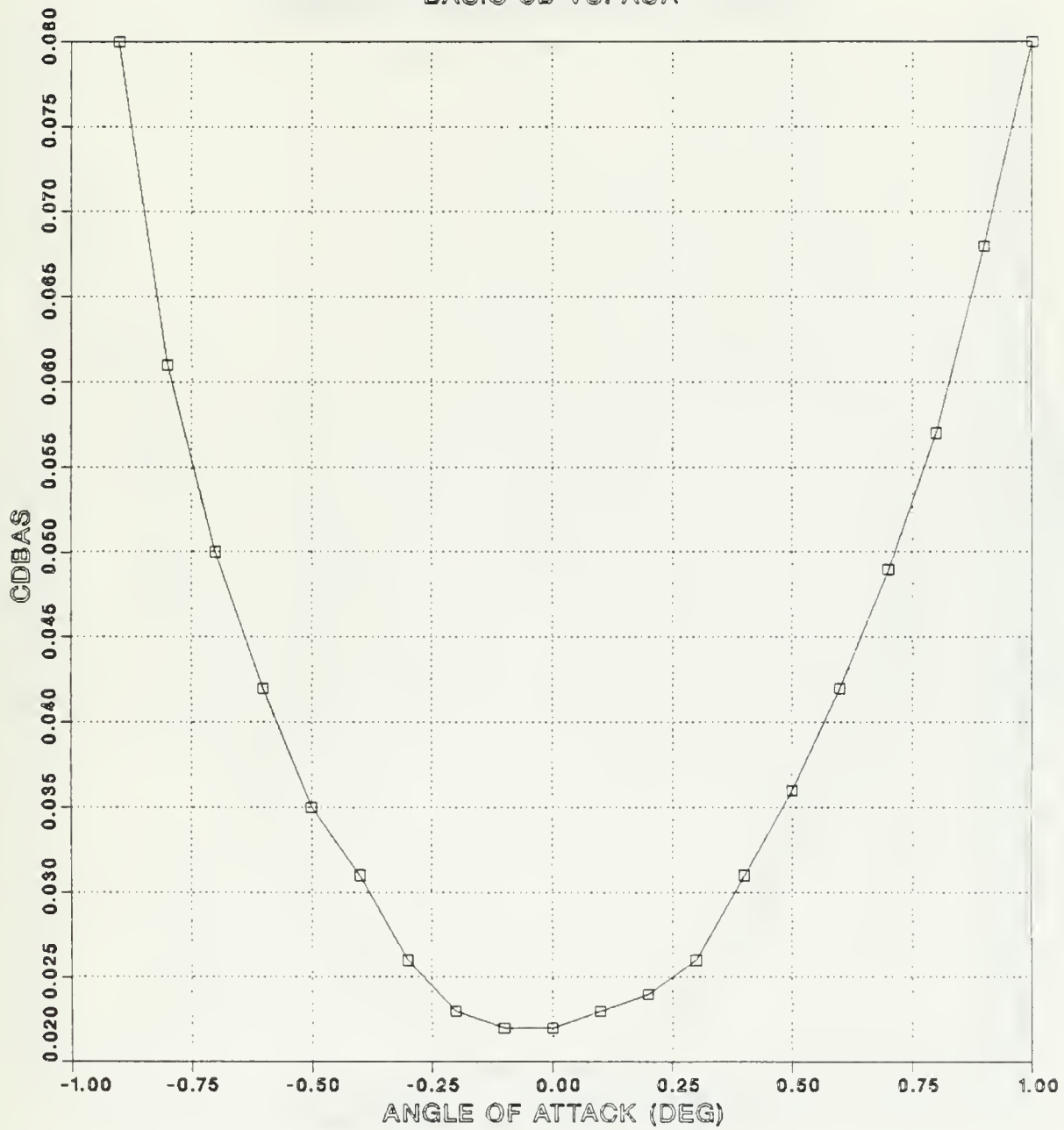


Figure A.4 Data Array DRG1.

STATIC AERODYNAMIC COEFFICIENTS

DRAG COEFFICIENT DATA

DELTA CD VS SYMMETRIC STABILATOR

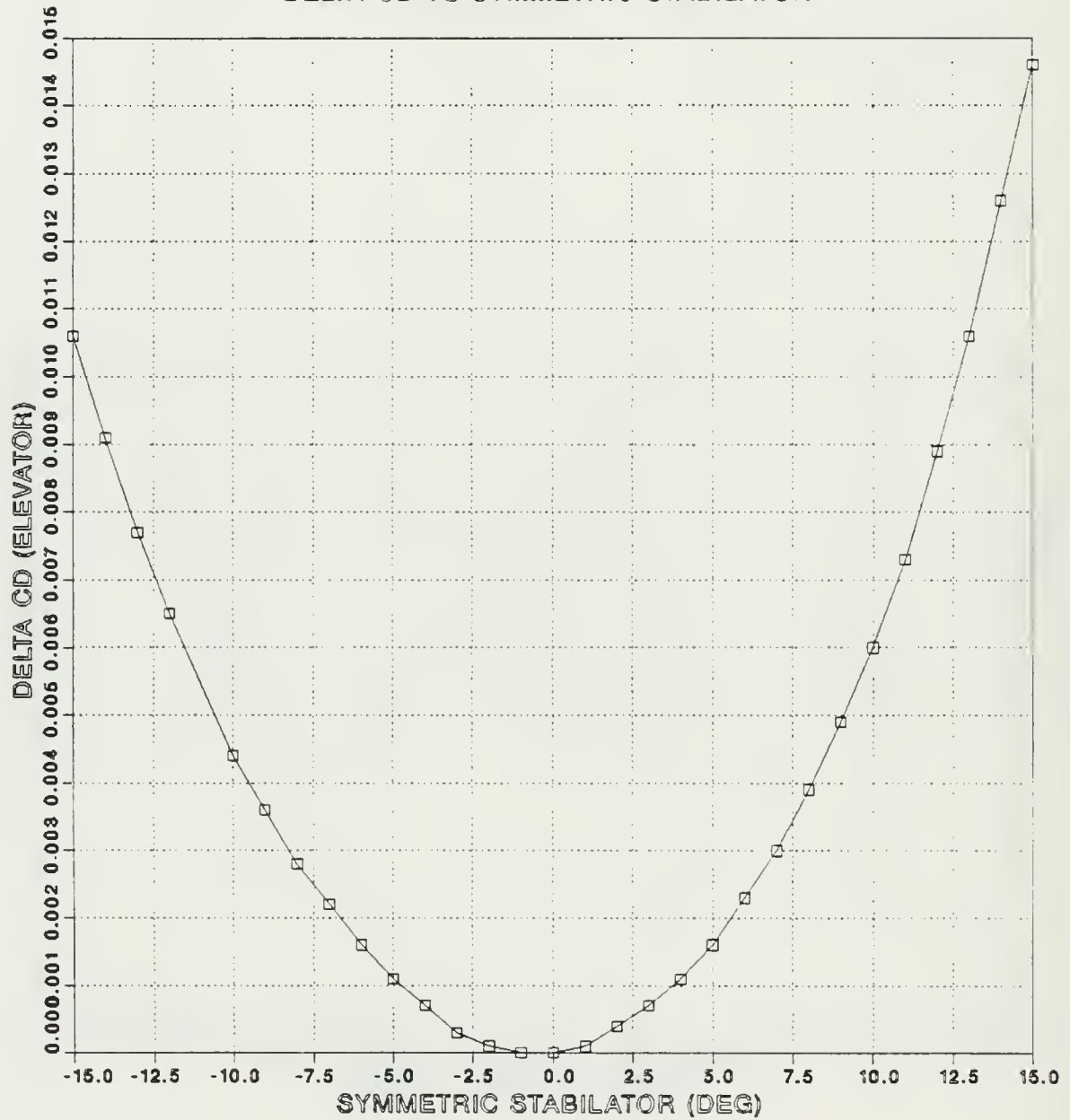


Figure A.5 Data Array DRG2.

STATIC AERODYNAMIC COEFFICIENTS

DRAG COEFFICIENT DATA

DELTA CD VS ASYMMETRIC STABILATOR

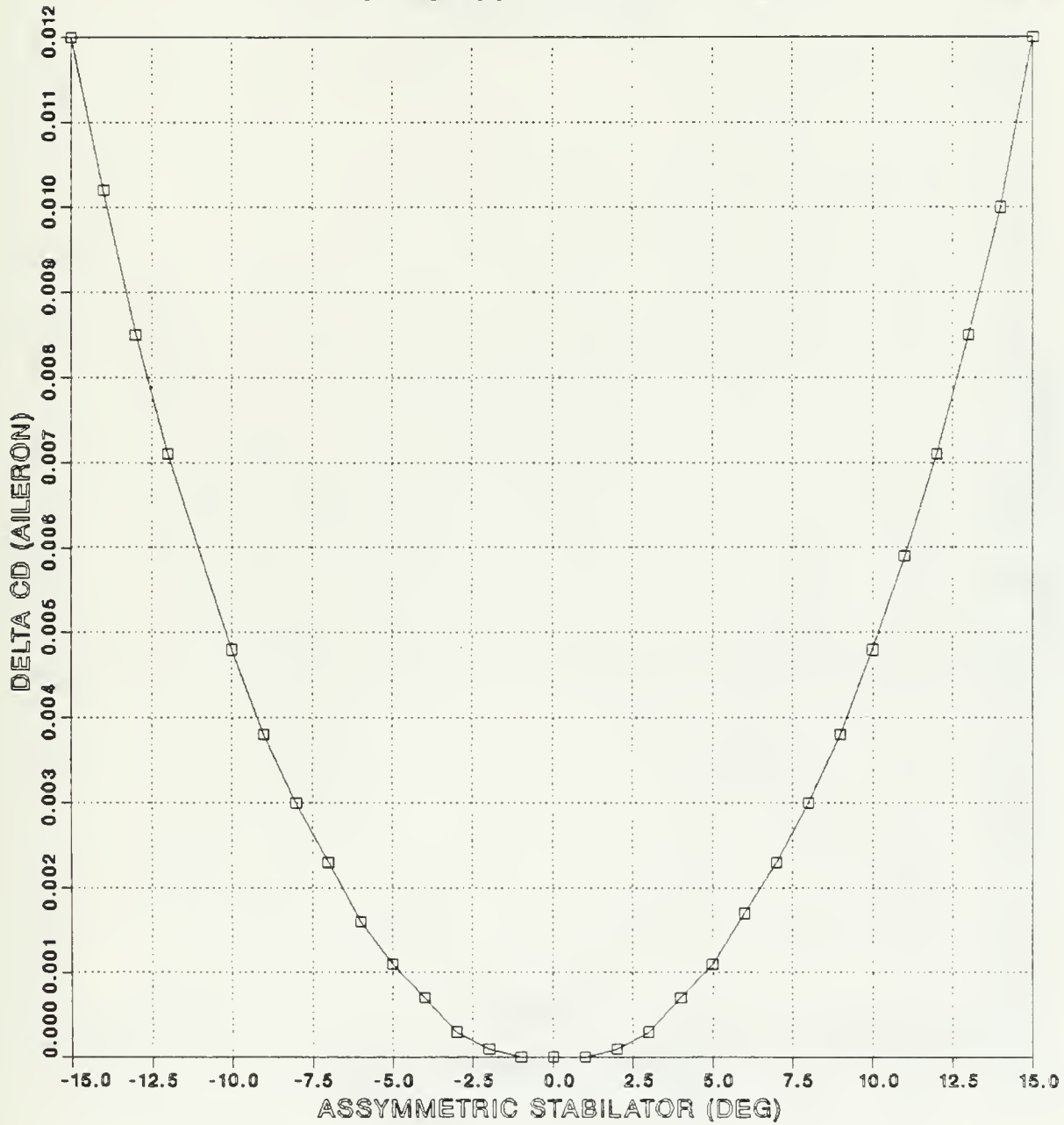


Figure A.6 Data Array DRG3.

# STATIC AERODYNAMIC COEFFICIENTS

## DRAG COEFFICIENT DATA

DELTA CD VS RUDDER

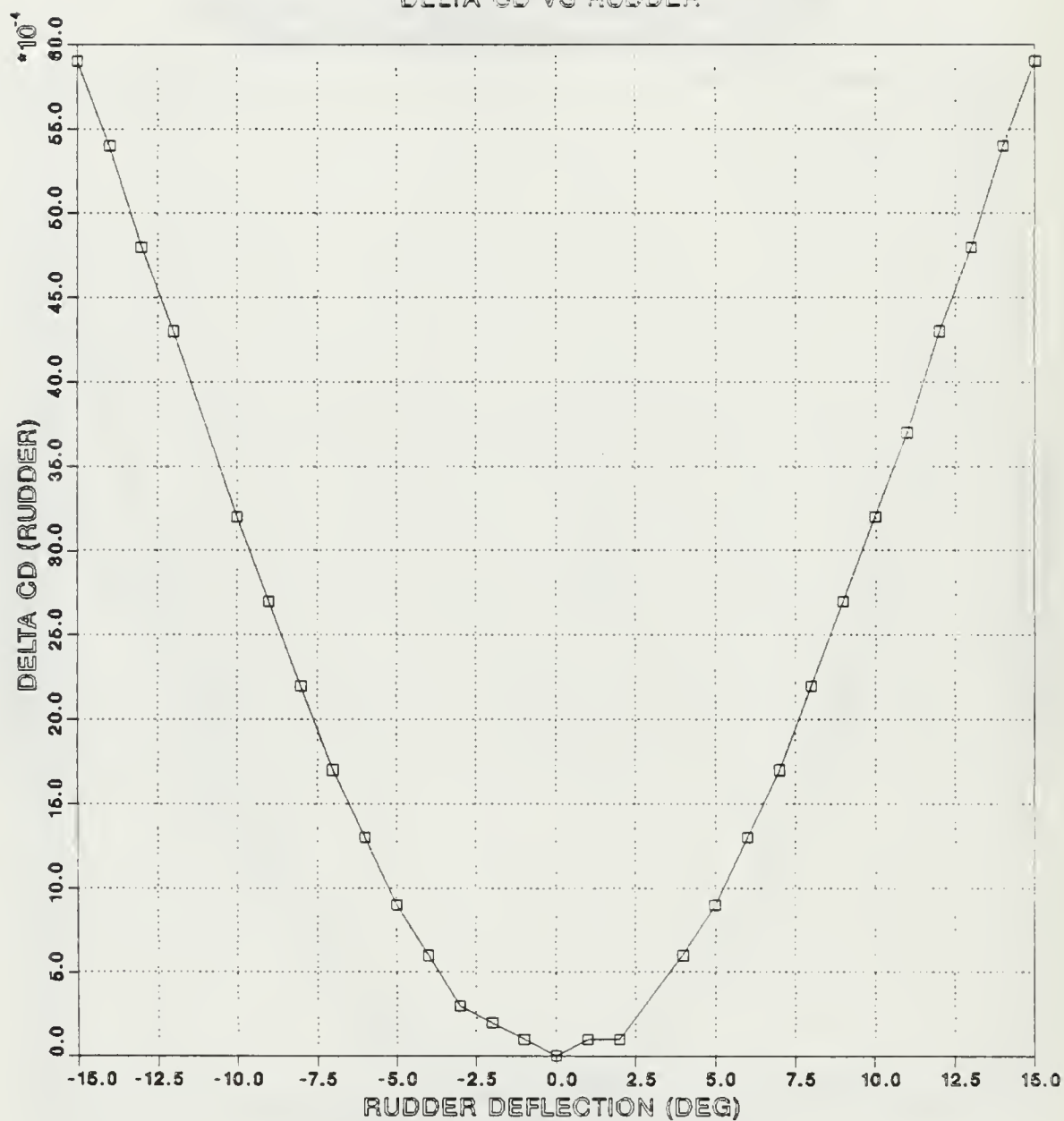


Figure A.7 Data Array DRG4.

STATIC AERODYNAMIC COEFFICIENTS  
**PITCHING MOMENT COEFFICIENT DATA**  
BASIC CM VS. AOA

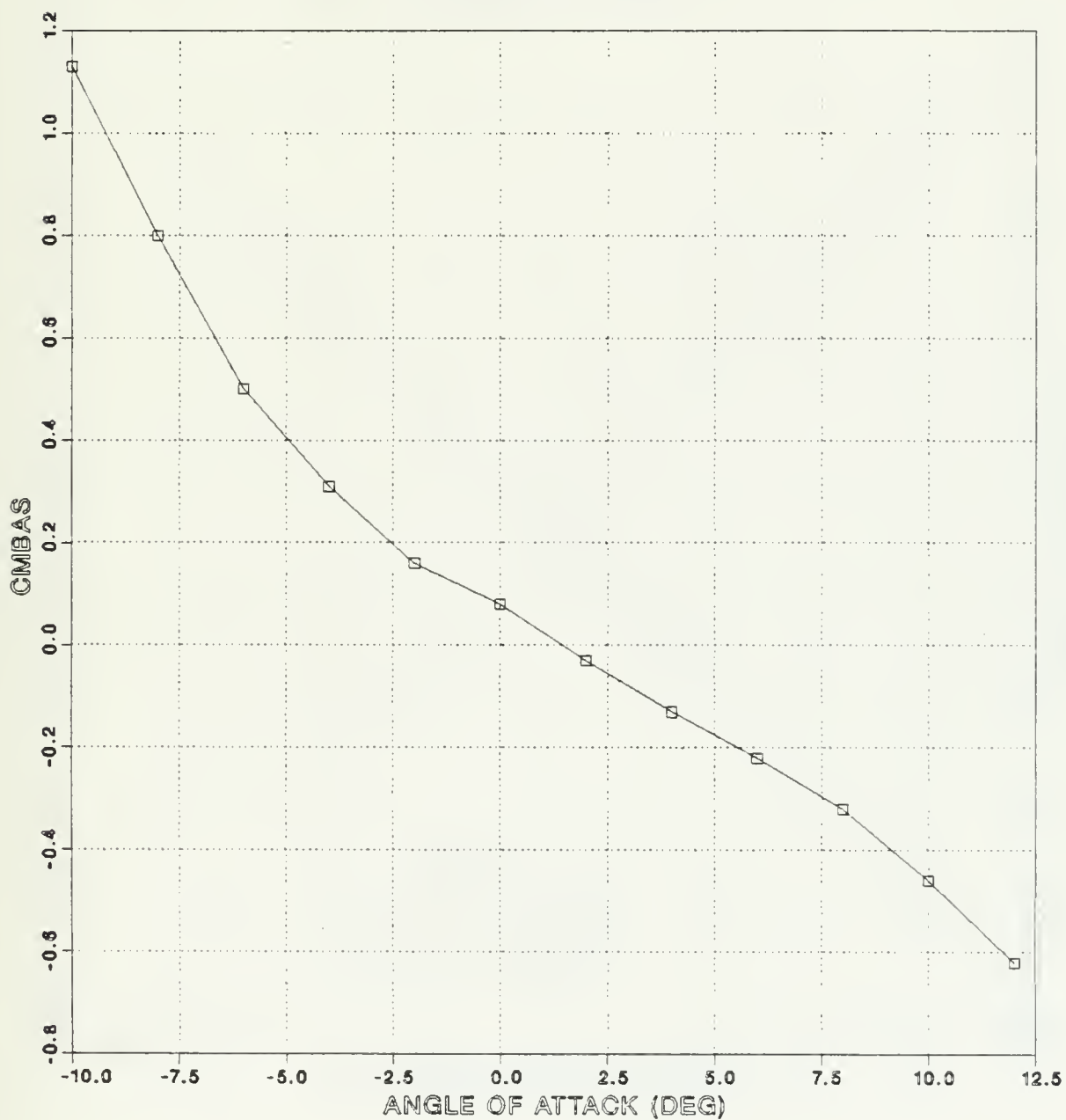


Figure A.8 Data Array PTCH1.



STATIC AERODYNAMIC COEFFICIENTS  
**PITCHING MOMENT COEFFICIENT DATA**  
DELTA CM VS SYMMETRIC STABILATOR

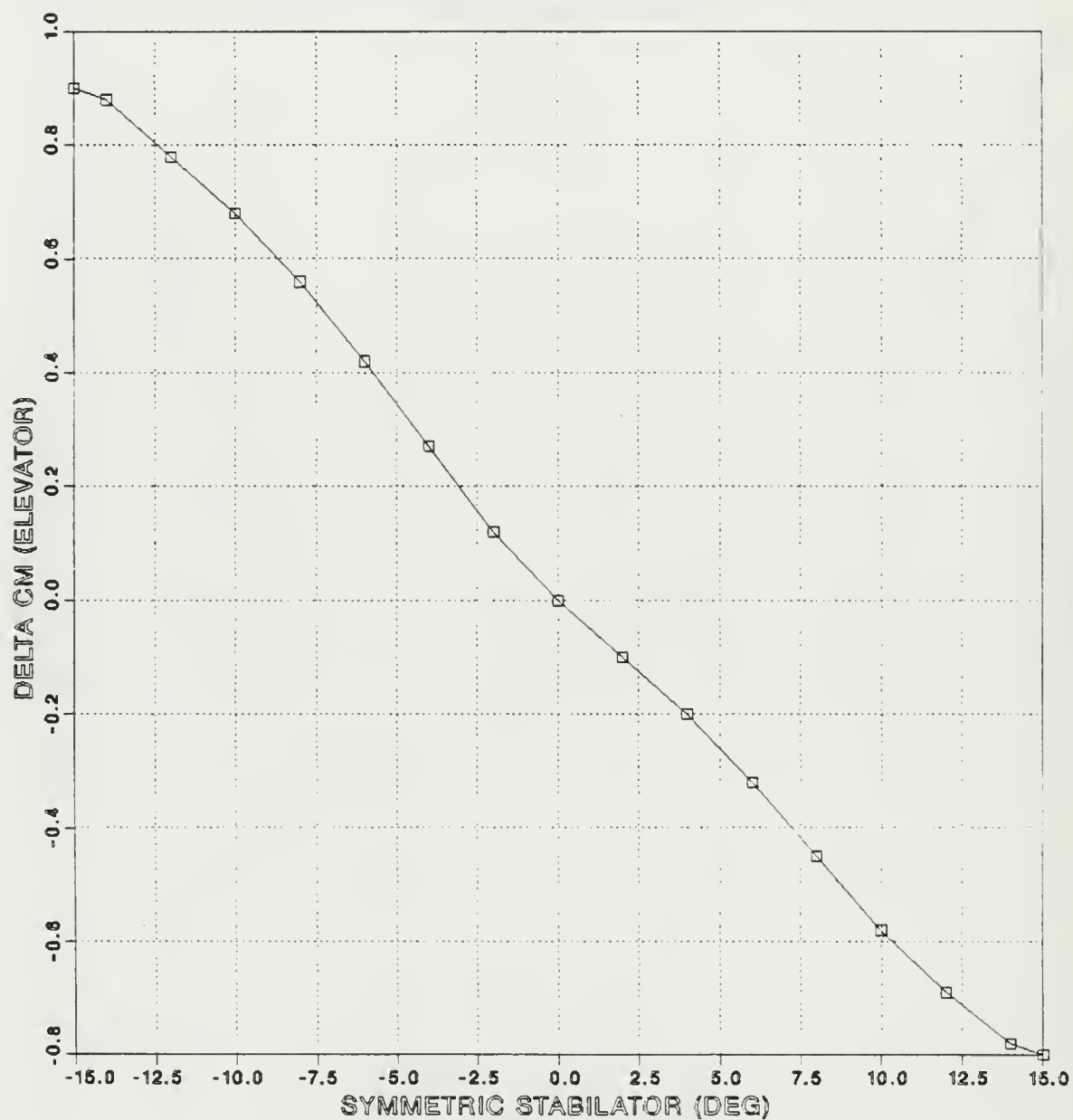


Figure A.9 Data Array PTCH2.

STATIC AERODYNAMIC COEFFICIENTS  
SIDESLIP COEFFICIENT DATA  
BASIC CY VS. BETA

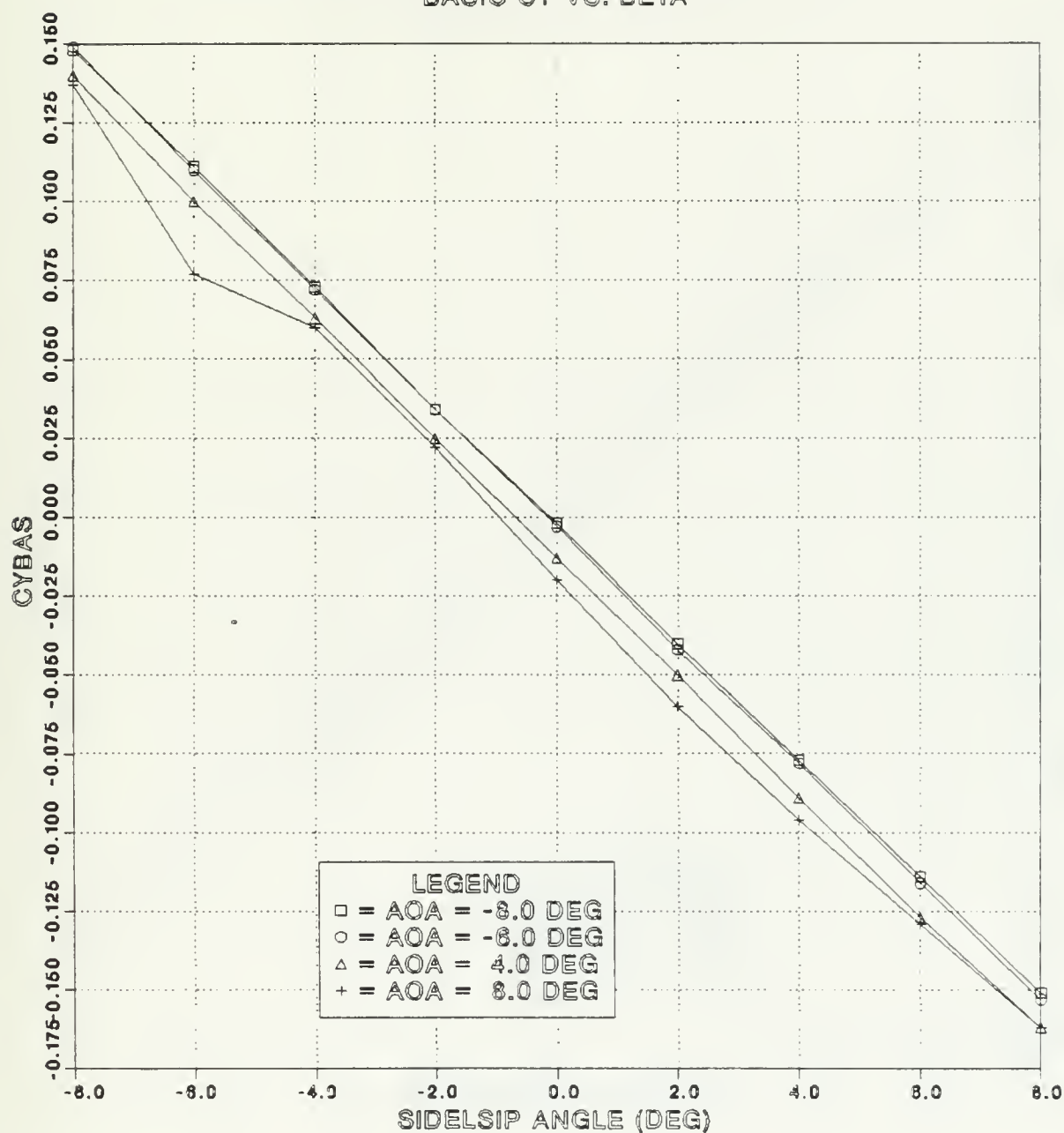


Figure A.10 Data Array SID1.

STATIC AERODYNAMIC COEFFICIENTS  
**SIDELIP COEFFICIENT DATA**  
 BASIC CROLL VS. BETA

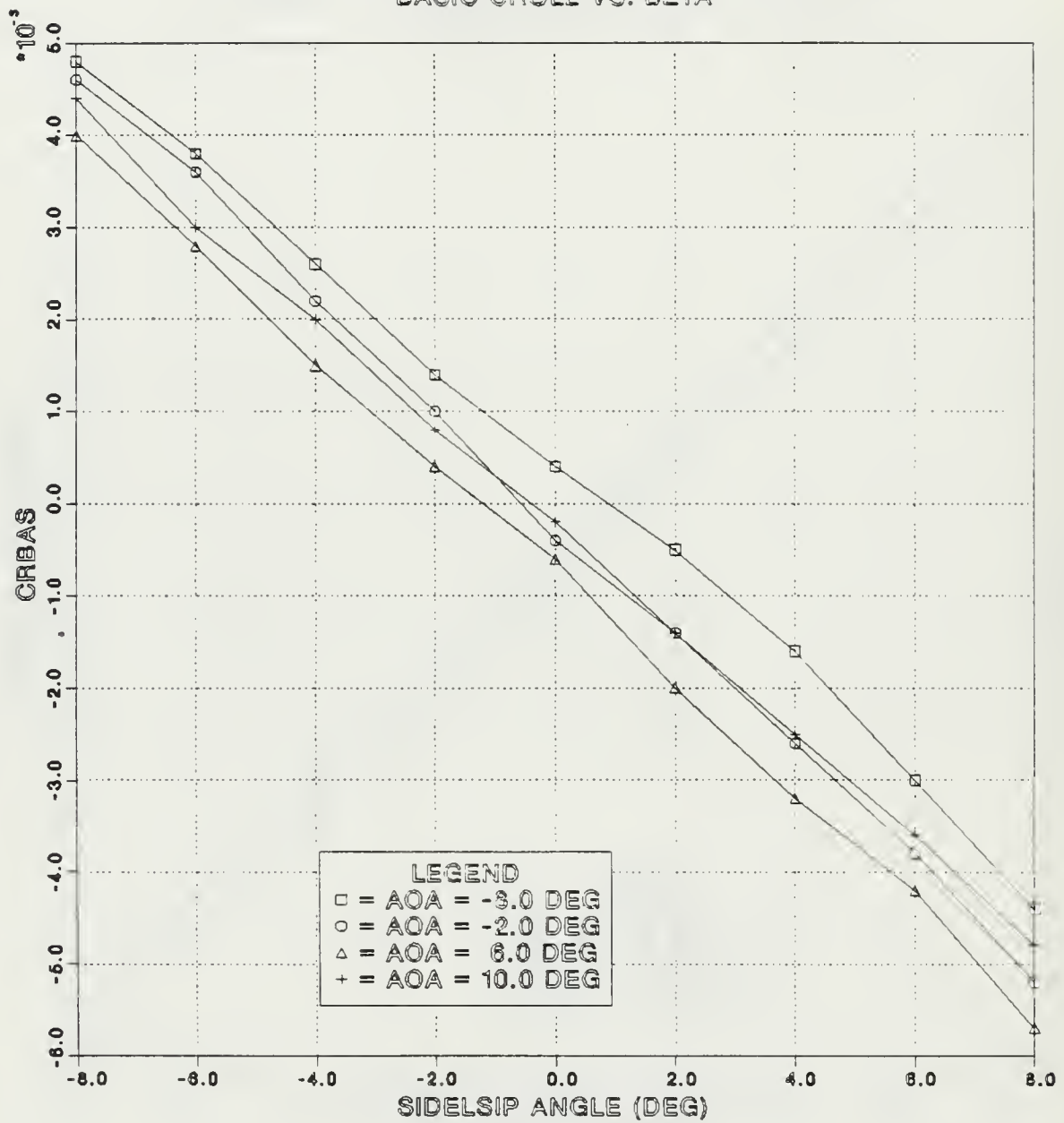


Figure A.11 Data Array SID2.

STATIC AERODYNAMIC COEFFICIENTS  
**SIDESLIP COEFFICIENT DATA**  
 BASIC CYAW VS. BETA

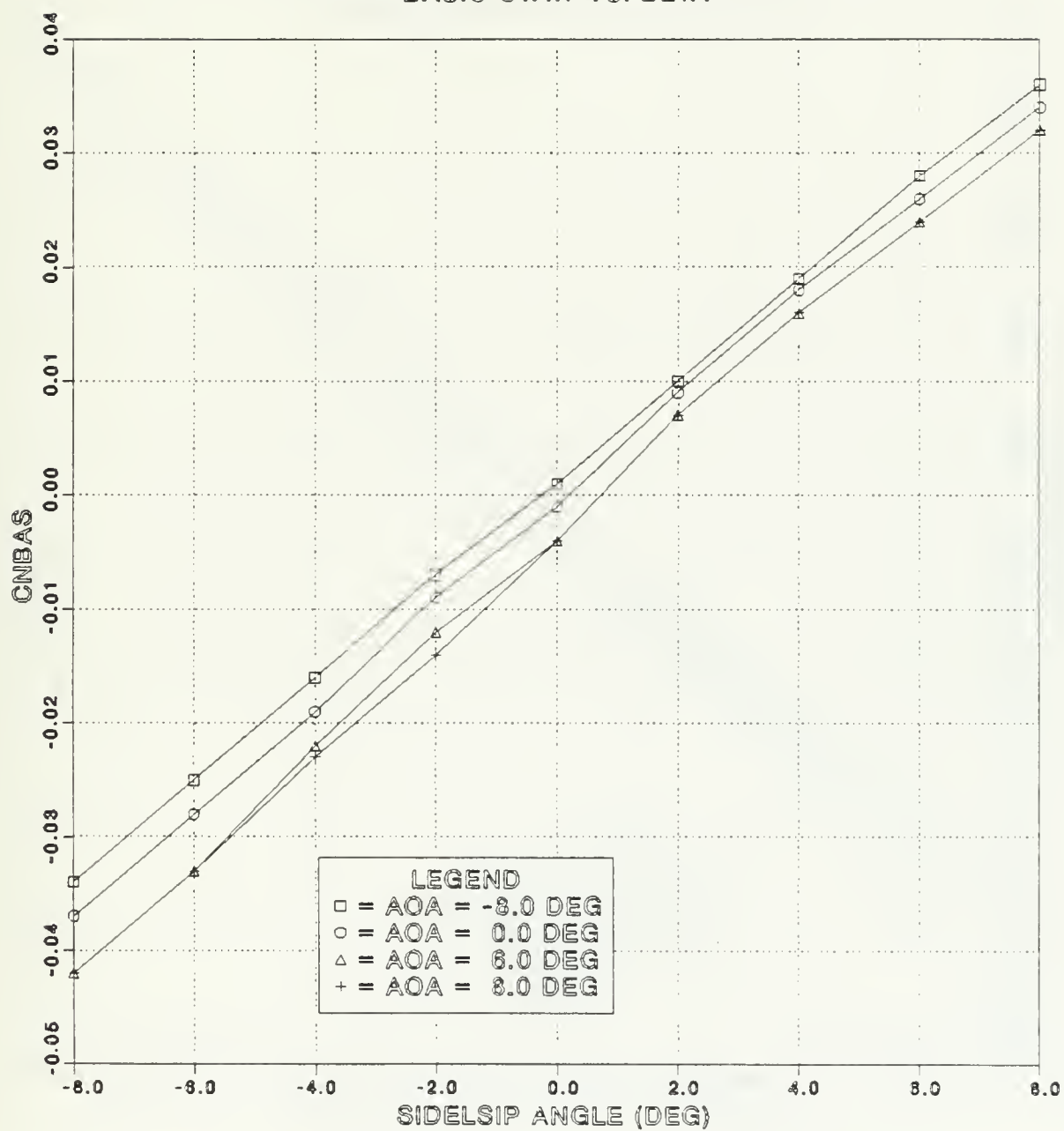


Figure A.12 Data Array SID3.

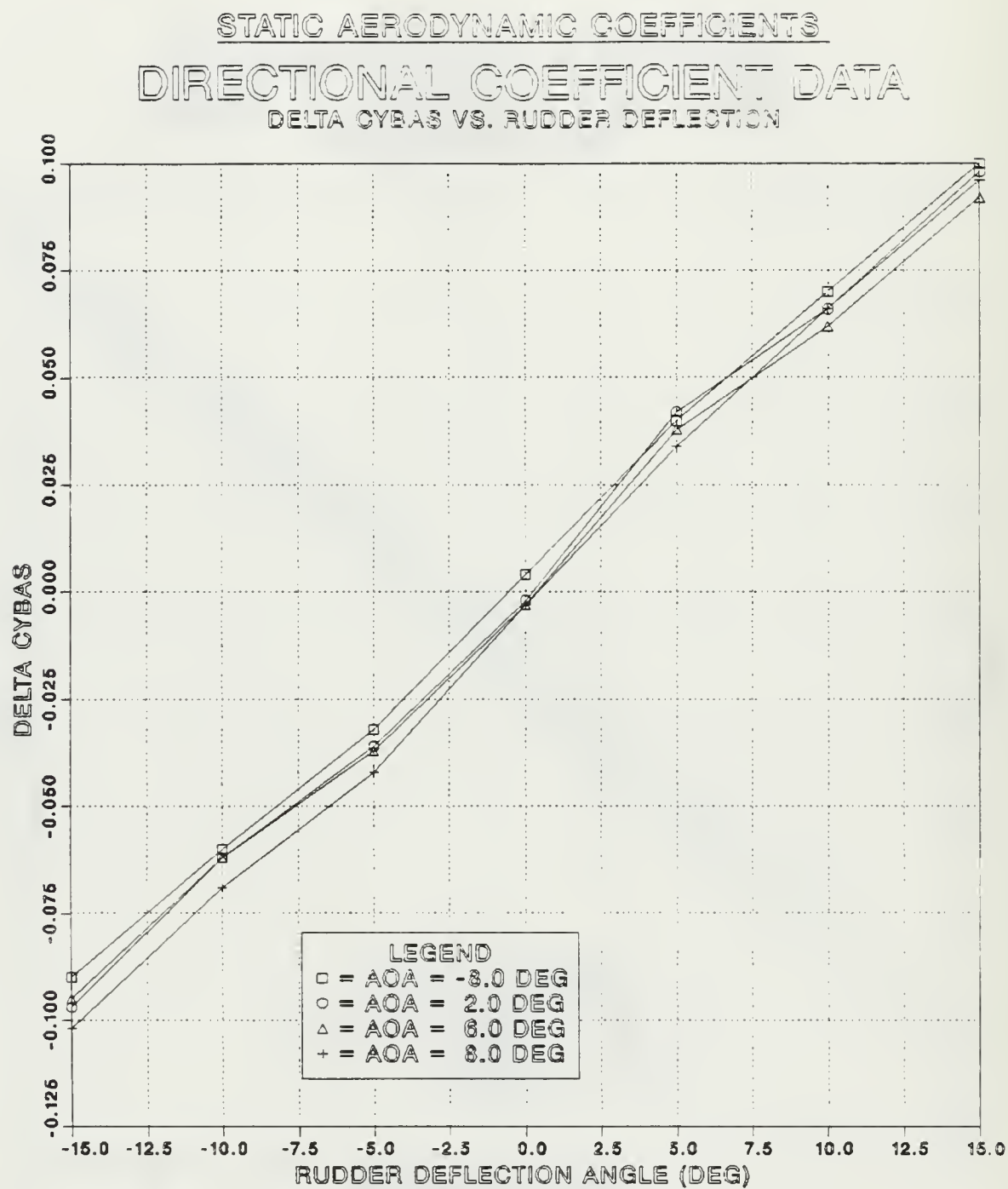


Figure A.13 Data Array DREC1.



STATIC AERODYNAMIC COEFFICIENTS  
DIRECTIONAL COEFFICIENT DATA  
DELTA CN VS. RUDDER DEFLECTION

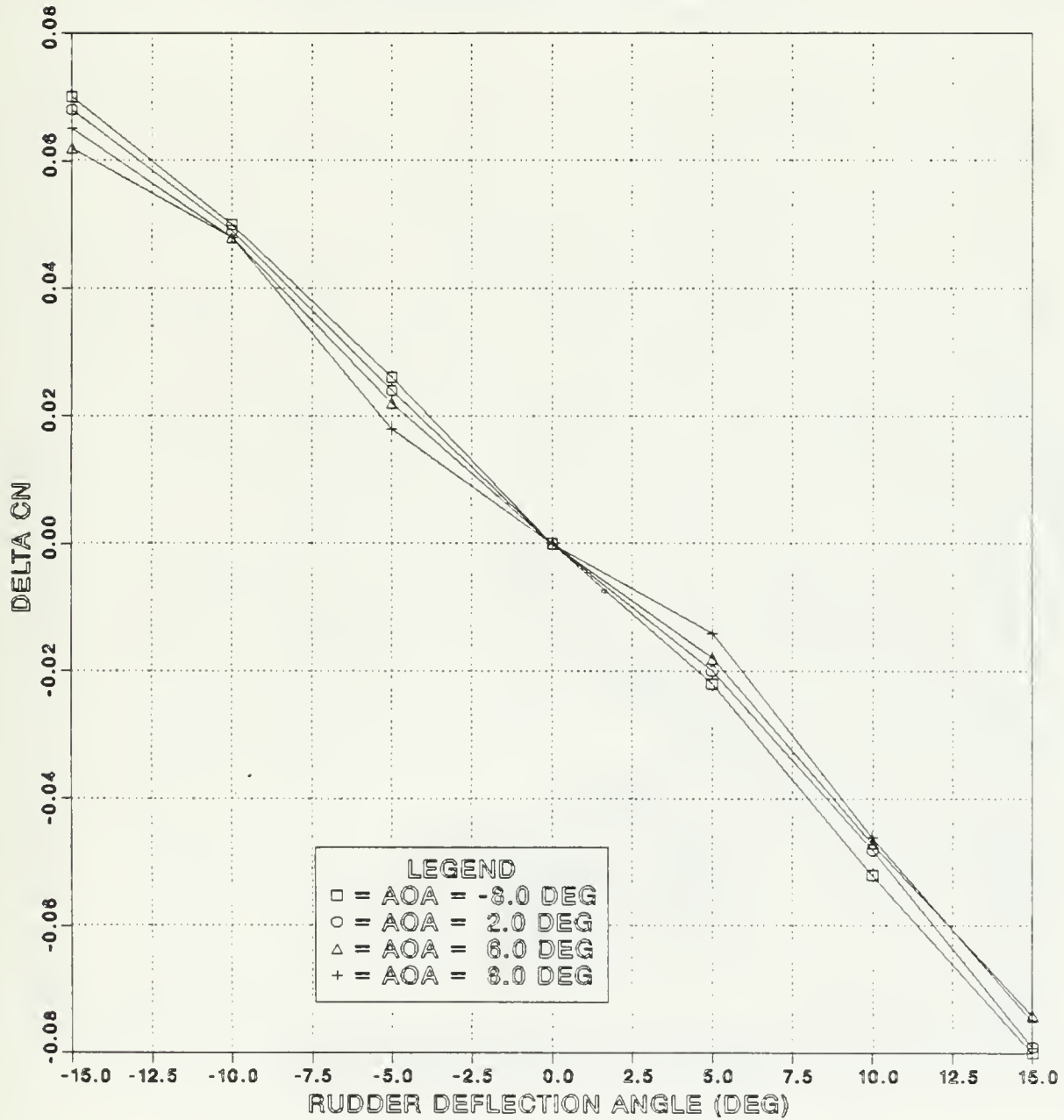


Figure A.14 Data Array DREC2.

STATIC AERODYNAMIC COEFFICIENTS  
DIRECTIONAL COEFFICIENT DATA  
DELTA CROLL VS. RUDDER DEFLECTION

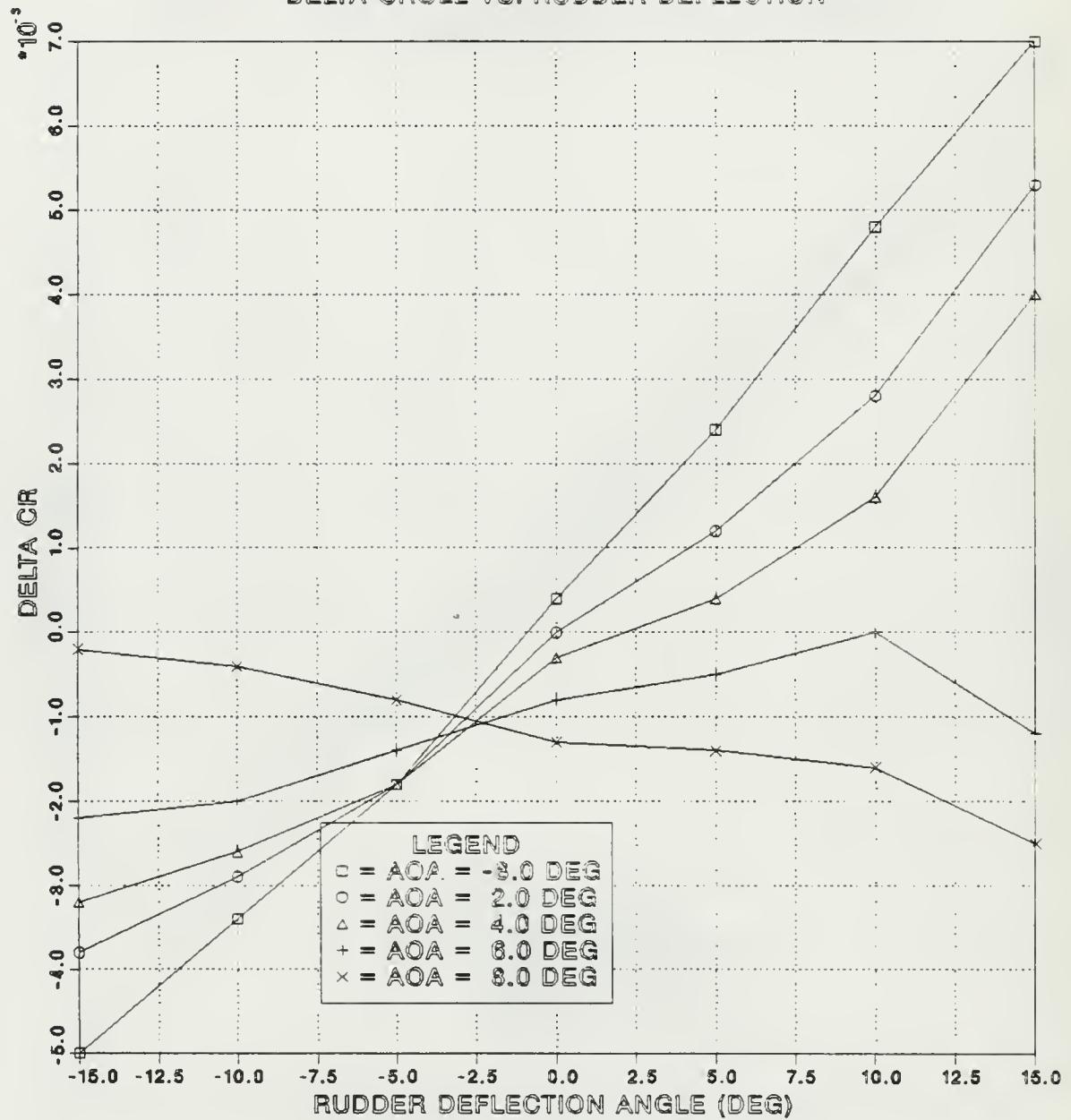


Figure A.15 Data Array DREC3.

STATIC AERODYNAMIC COEFFICIENTS  
LATERAL COEFFICIENT DATA  
DELTA CYBAS VS. ASYMMETRIC STABILATOR

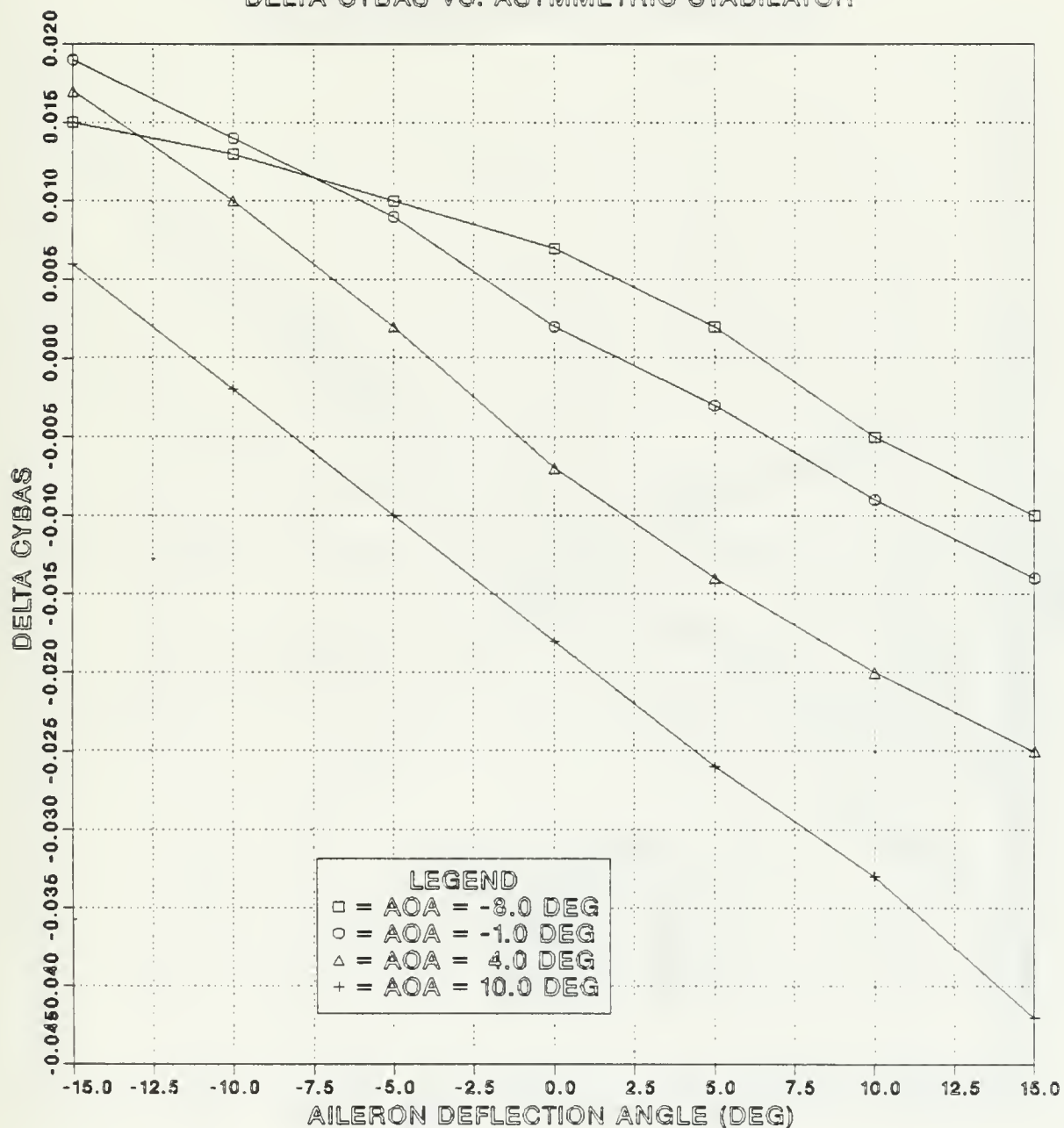


Figure A.16 Data Array LTRL1.

STATIC AERODYNAMIC COEFFICIENTS  
LATERAL COEFFICIENT DATA  
DELTA CN VS. ASYMMETRIC STABILATOR

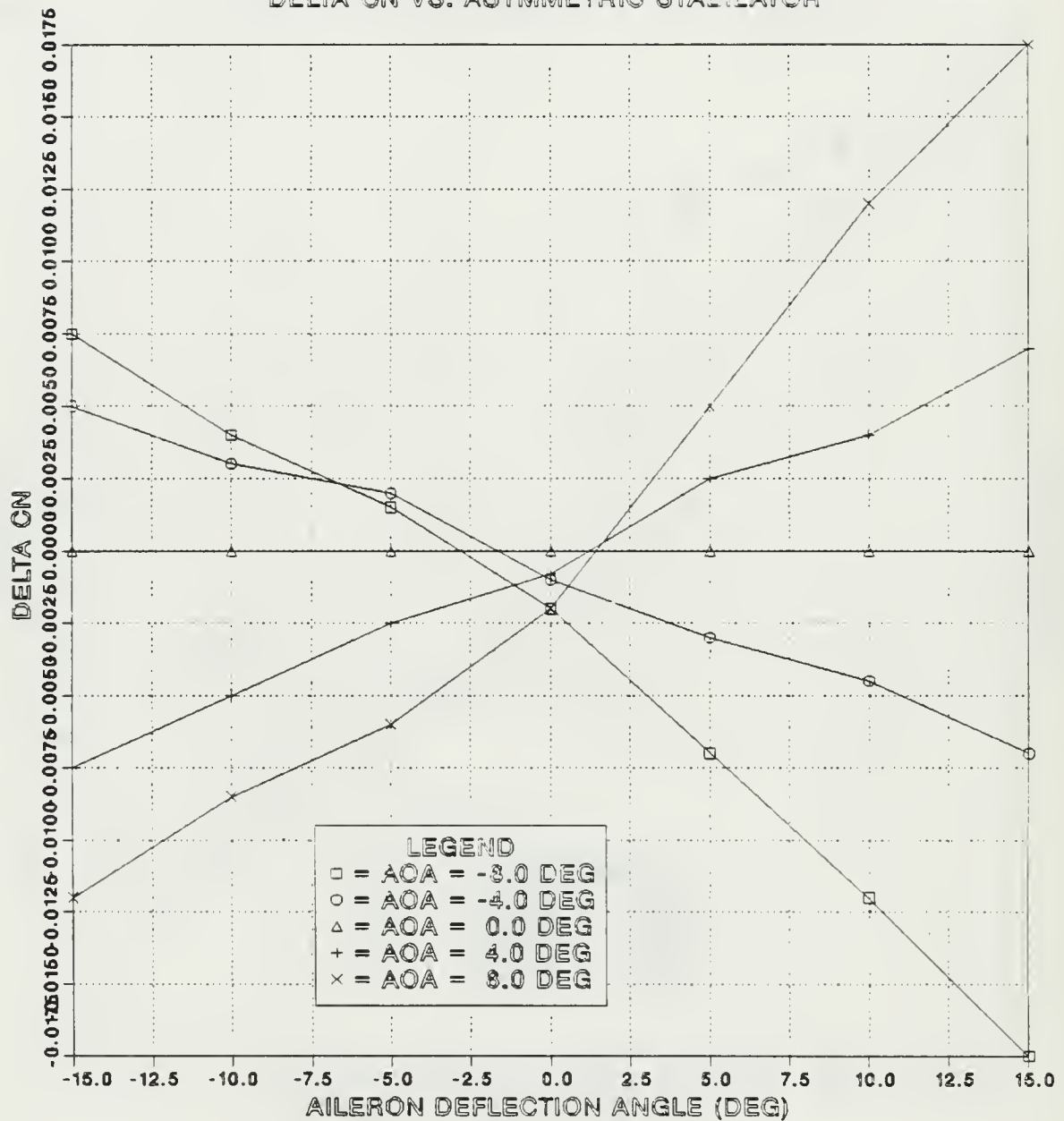


Figure A.17 Data Array LTFL2.

STATIC AERODYNAMIC COEFFICIENTS  
**LATERAL COEFFICIENT DATA**  
 DELTA CROLL VS. ASYMMETRIC STABILATOR

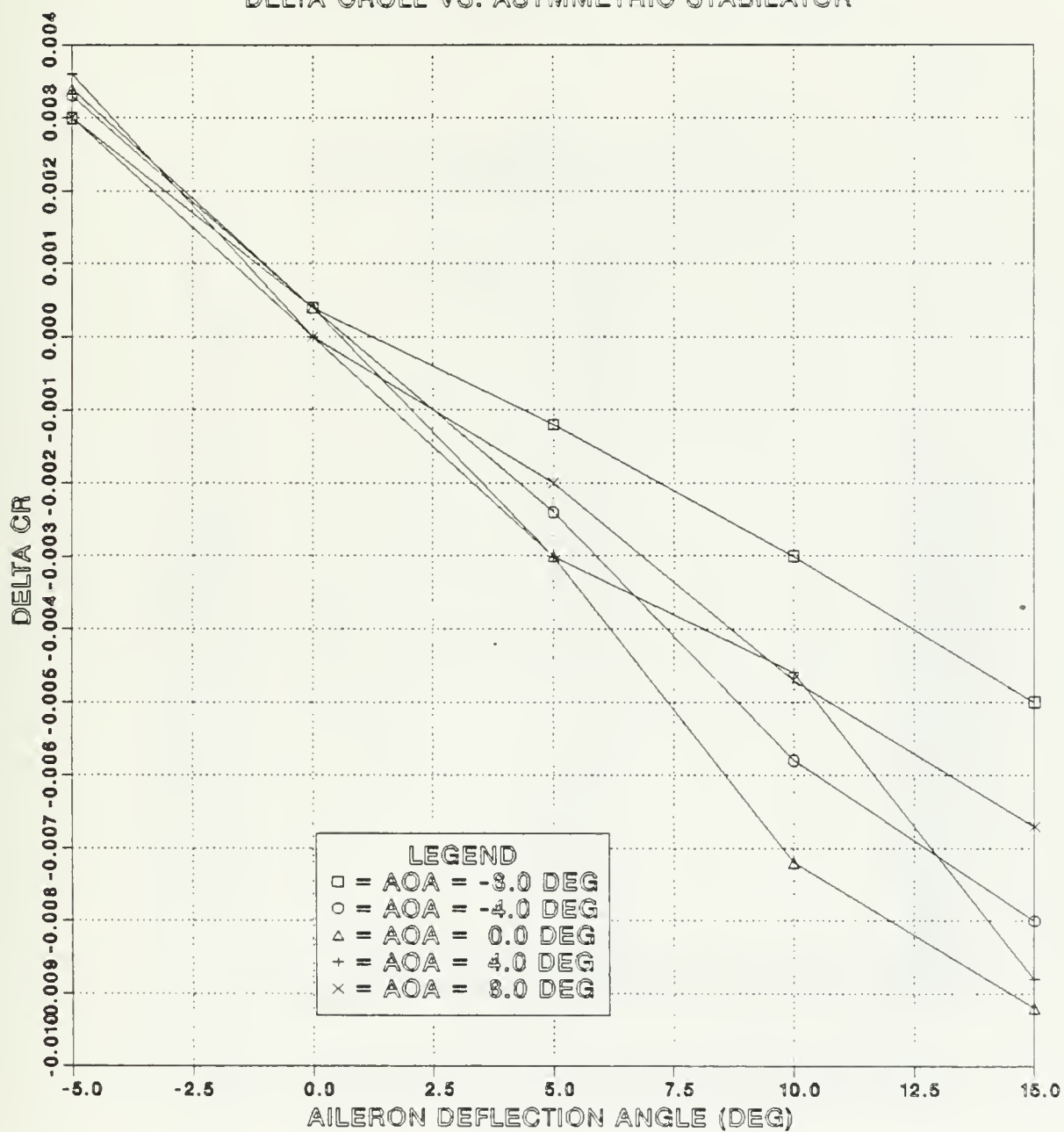


Figure A.18 Data Array LTRL3.



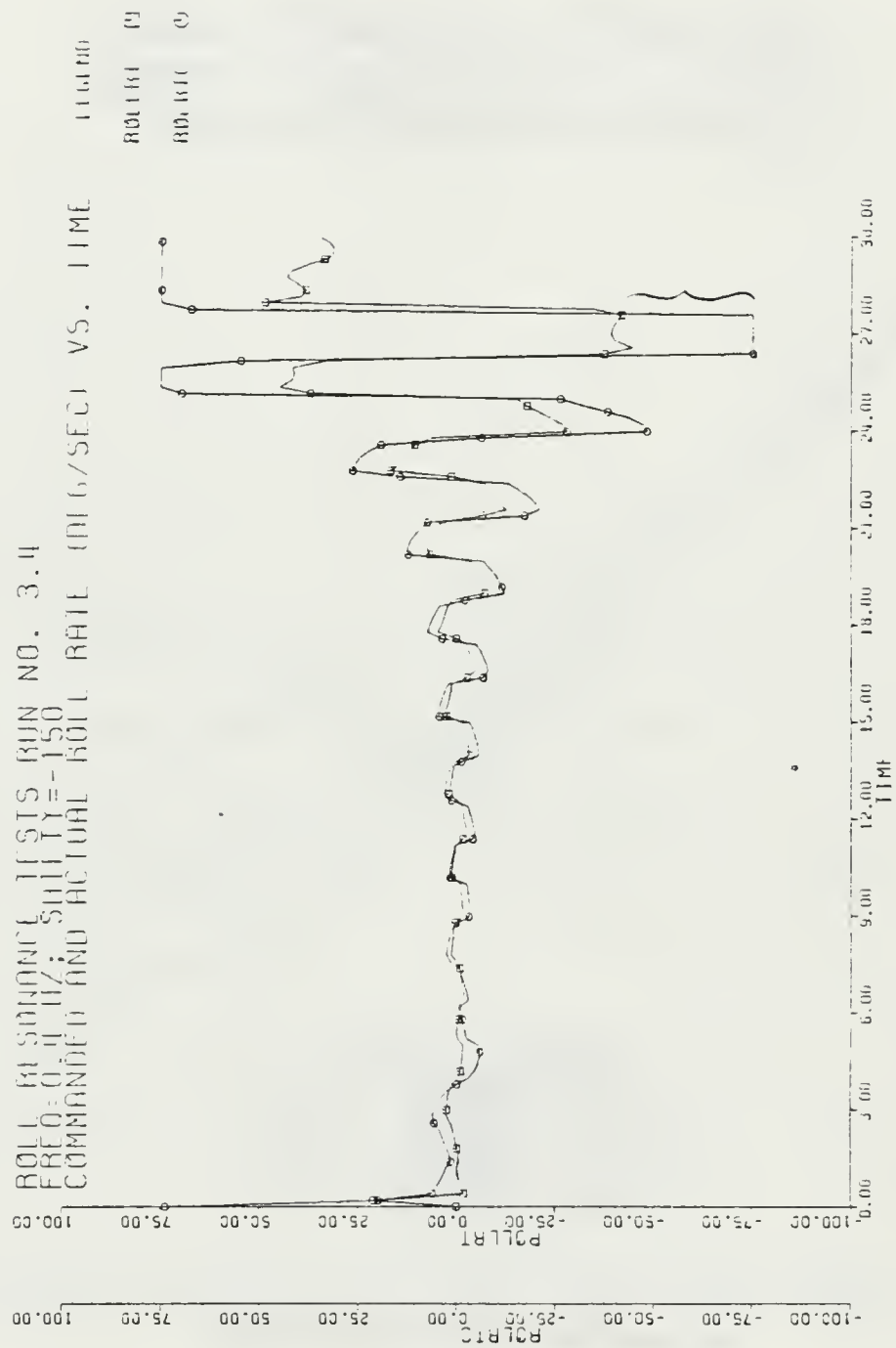


Figure A.19 CSMP Data (Roll Rate) - KROLLR = 0.1.

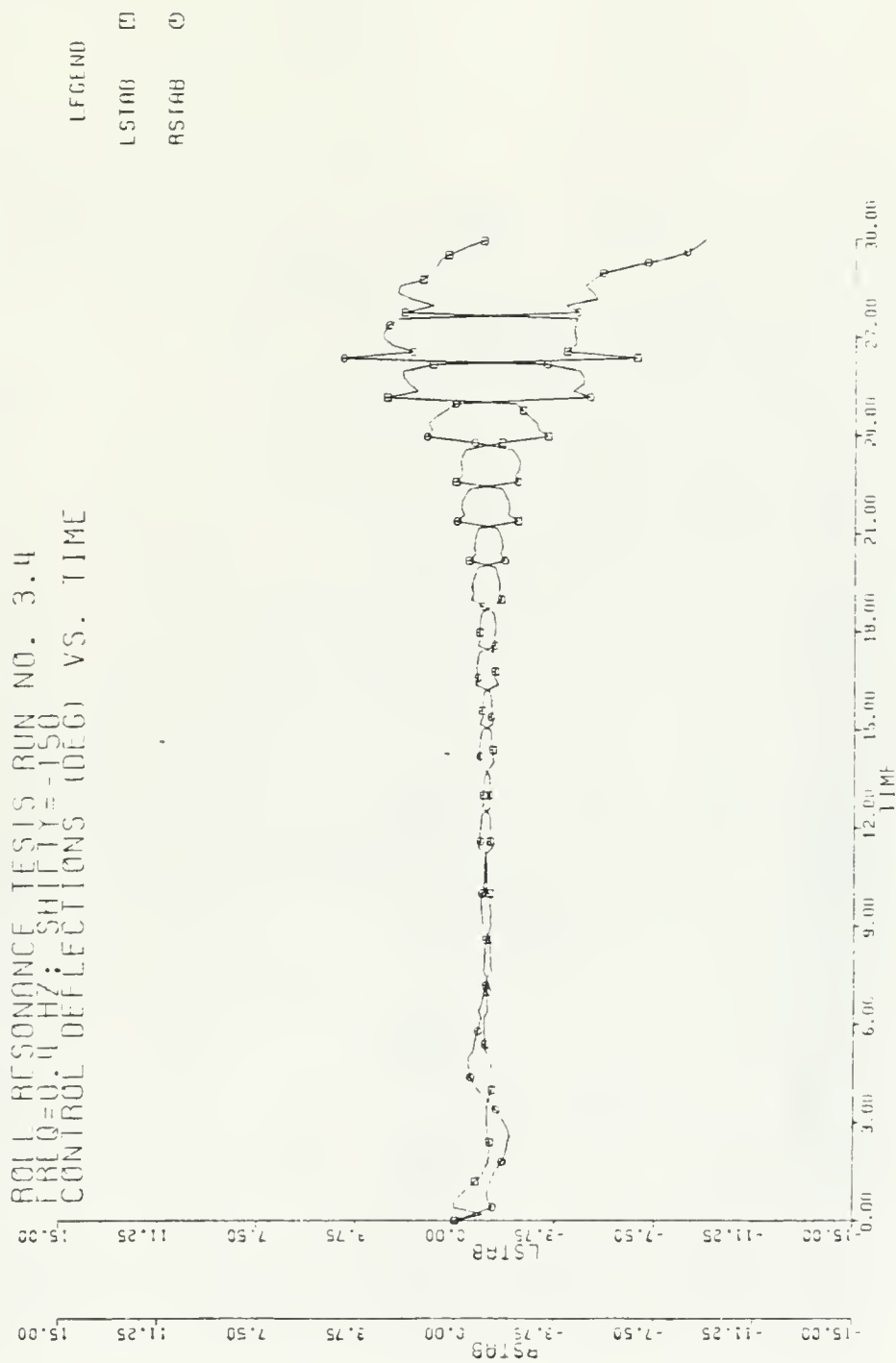


Figure A.20 CSMP Data (Controls) - KROLLP = 0.1.

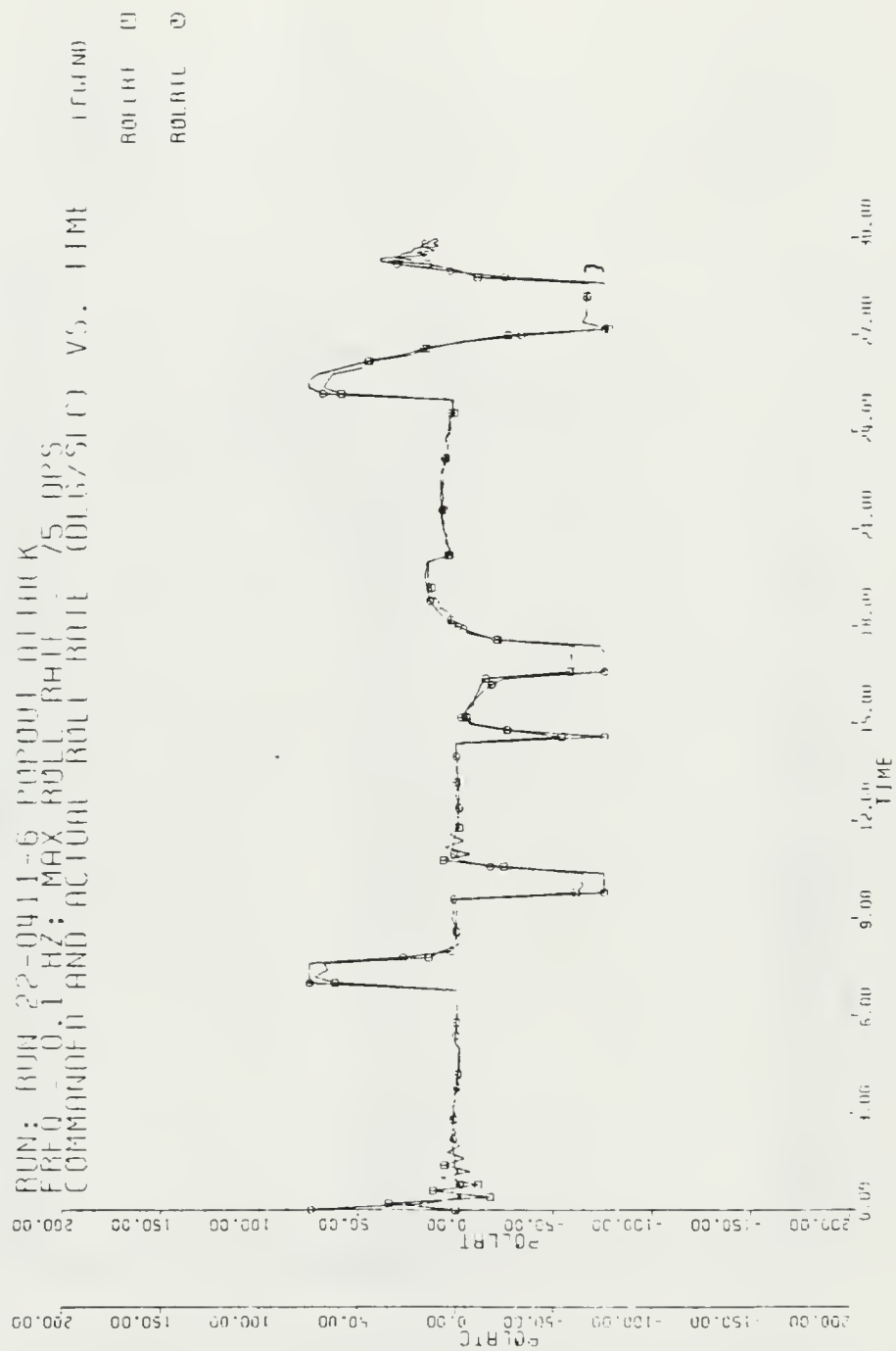


Figure A.21 CSMP Data (Roll Rate) - KROLLR = 0.5.

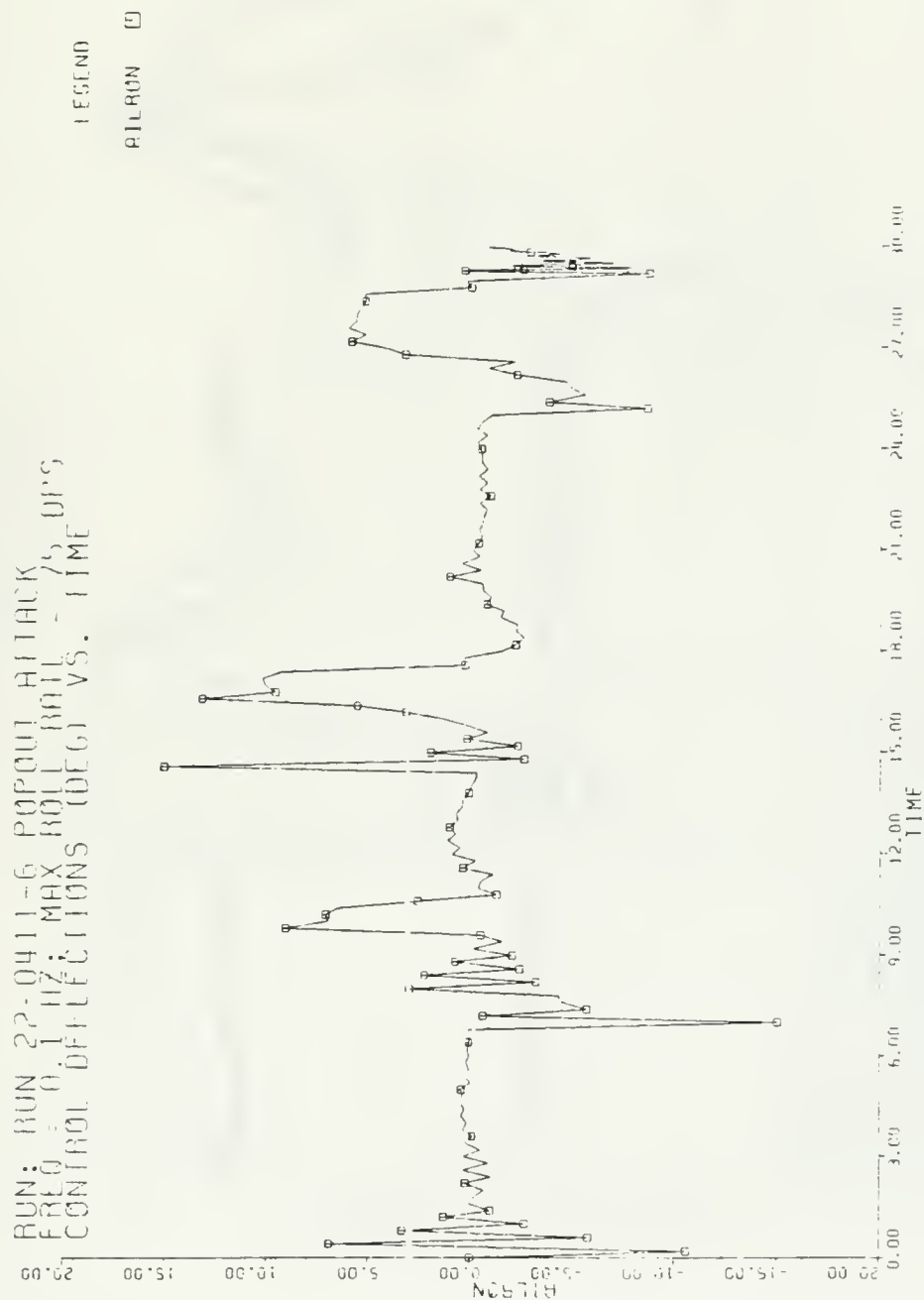


Figure A.22 CSMP Data (Controls) - Krollr = 0.5.

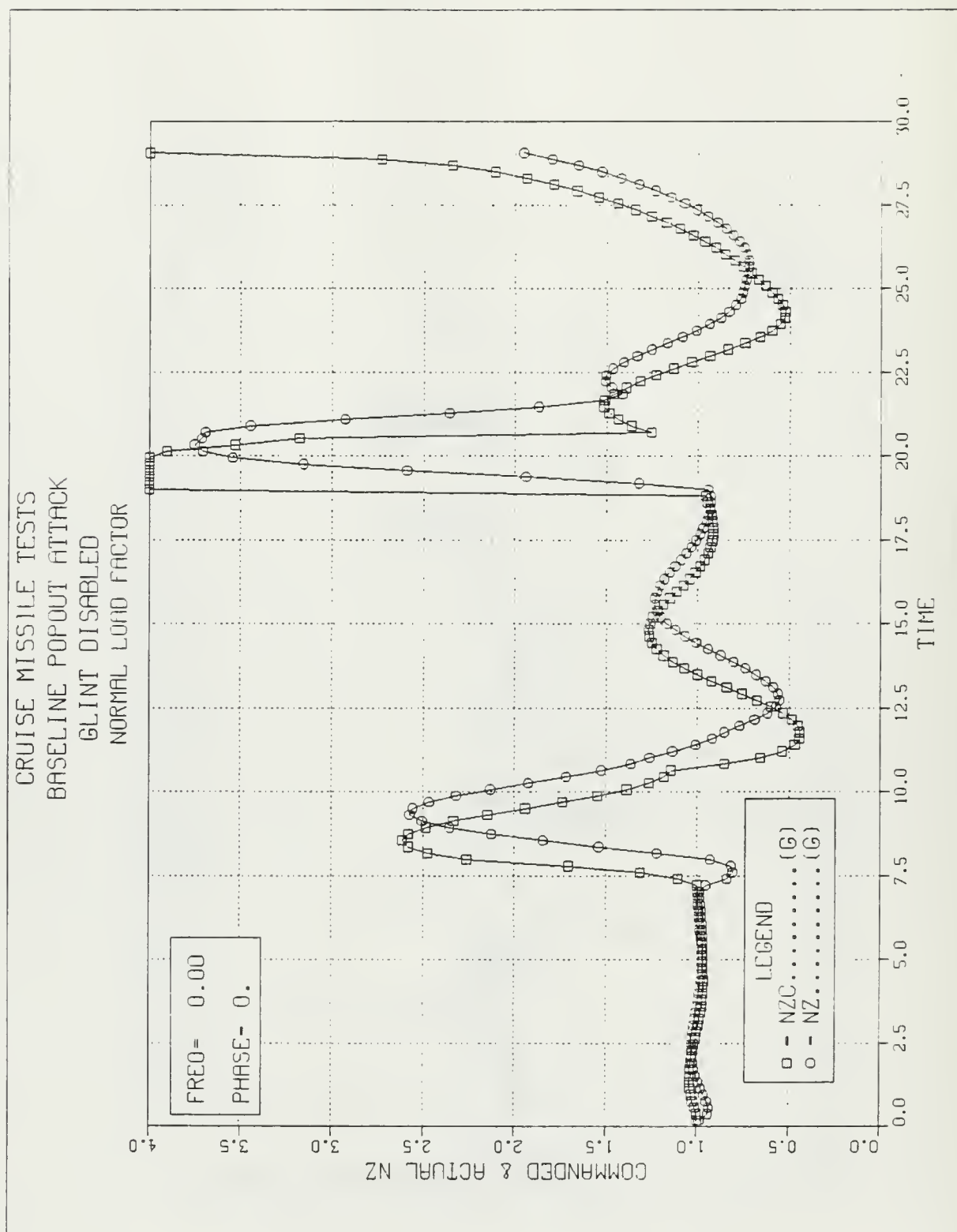


Figure A.23 Baseline - no ECM or GLINT - Load Factor.



CRUISE MISSILE TESTS  
 BASELINE POPOUT ATTACK  
 GLINT DISABLED  
 ROLL RATE CONTROL

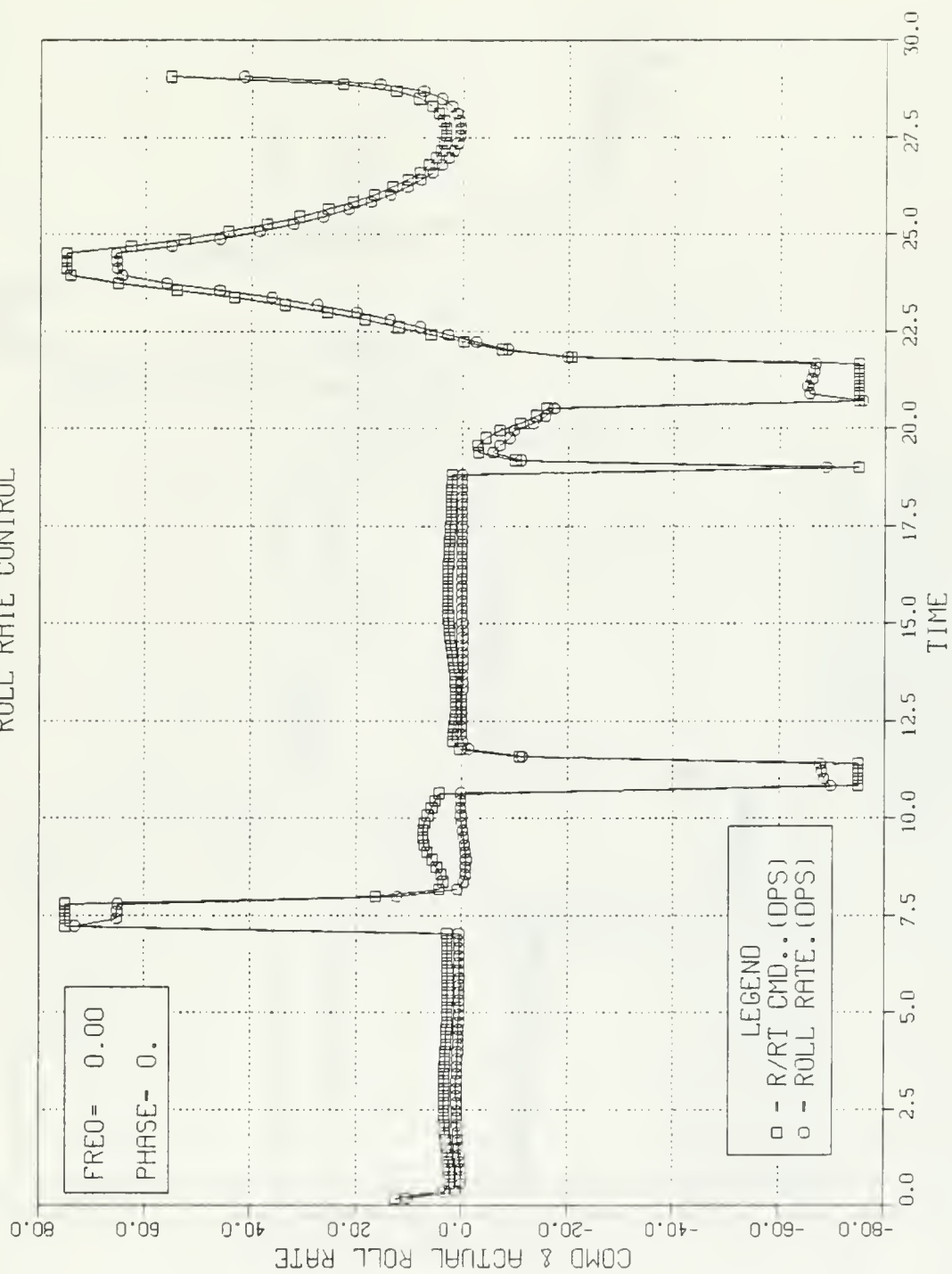


Figure A.24 Baseline - no ECM or GLINT - Roll Rate.

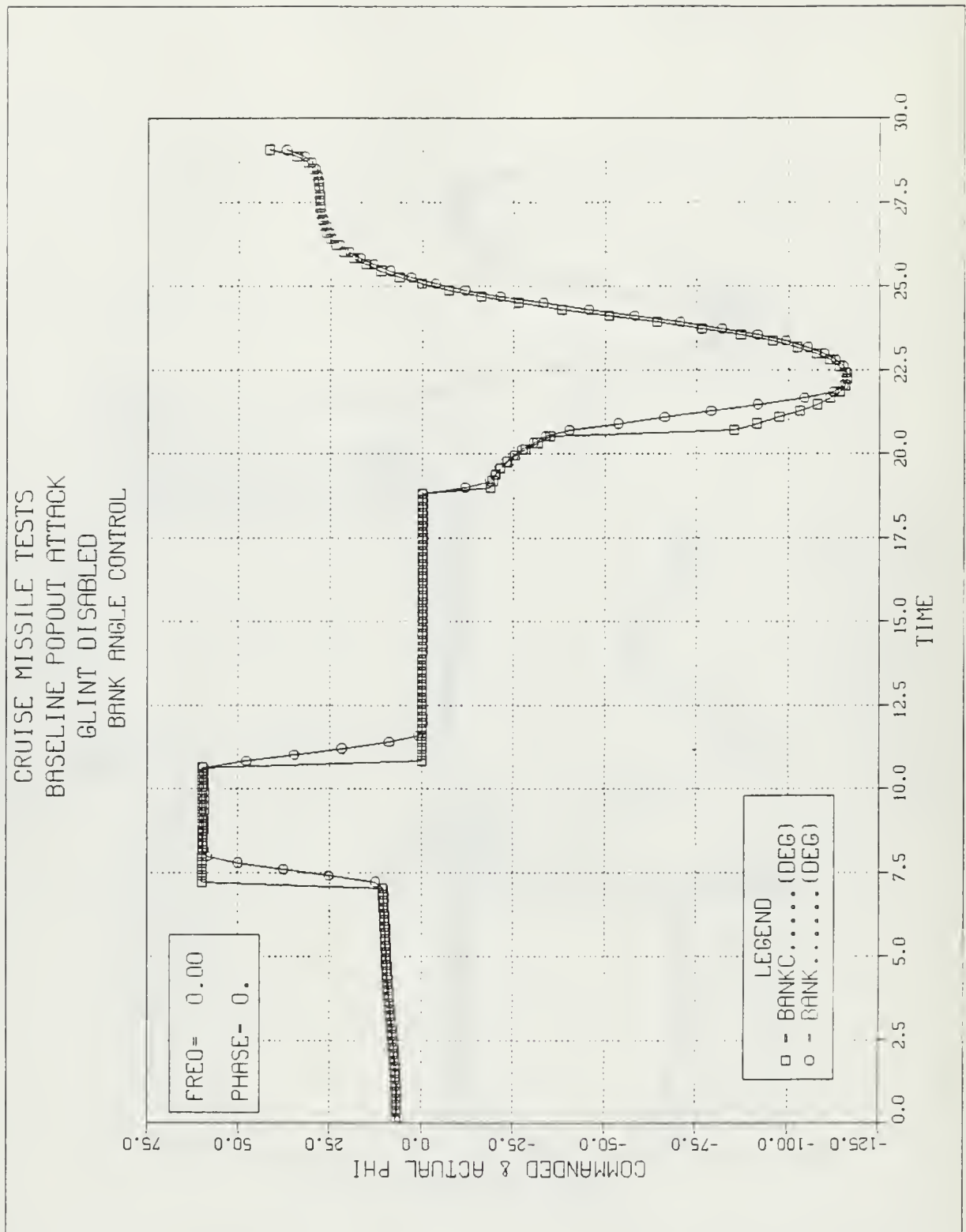


Figure A.25 Baseline - no ECM or GLINT - Bank.

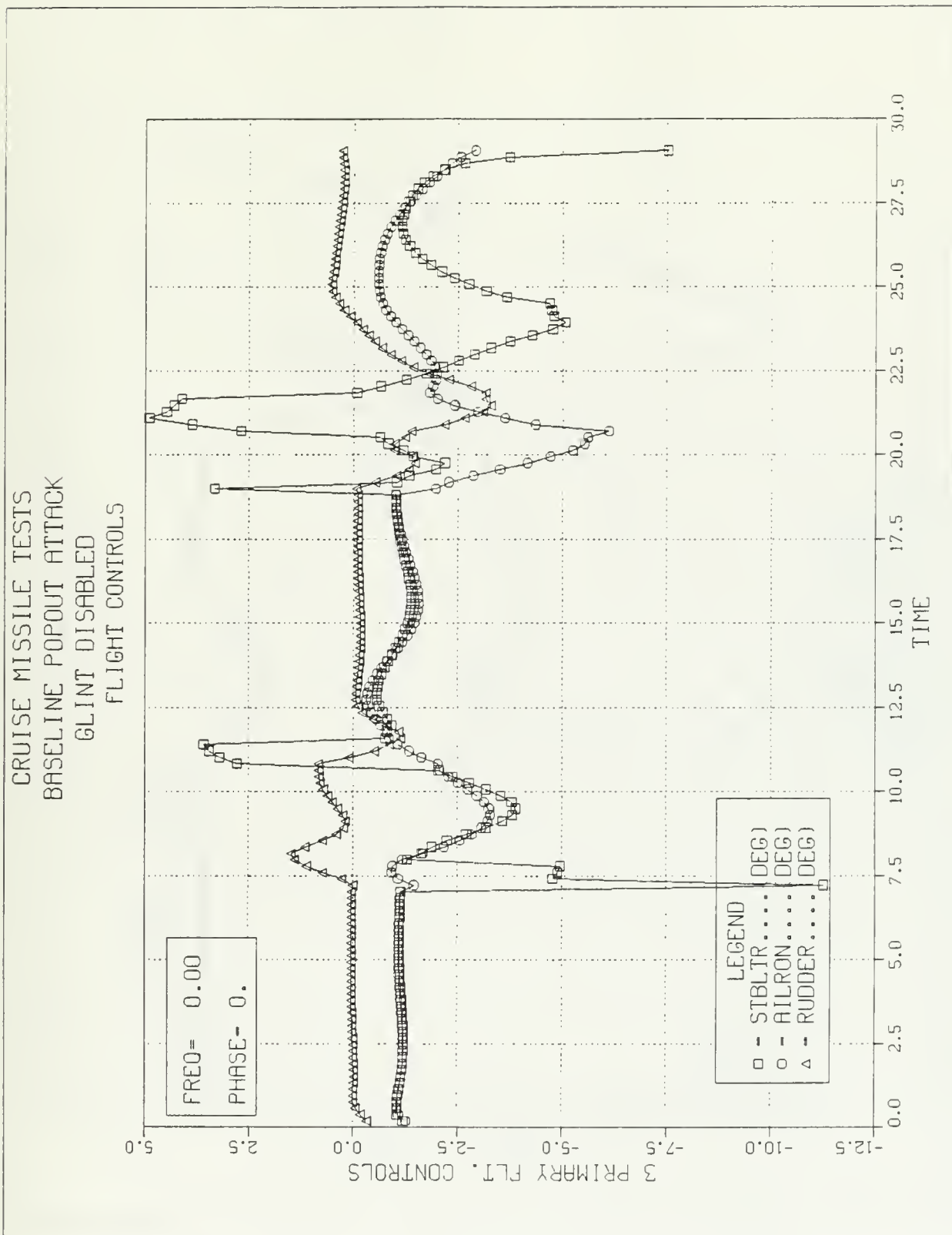


Figure A.26 Baseline - no ECM or GLINT - Controls.

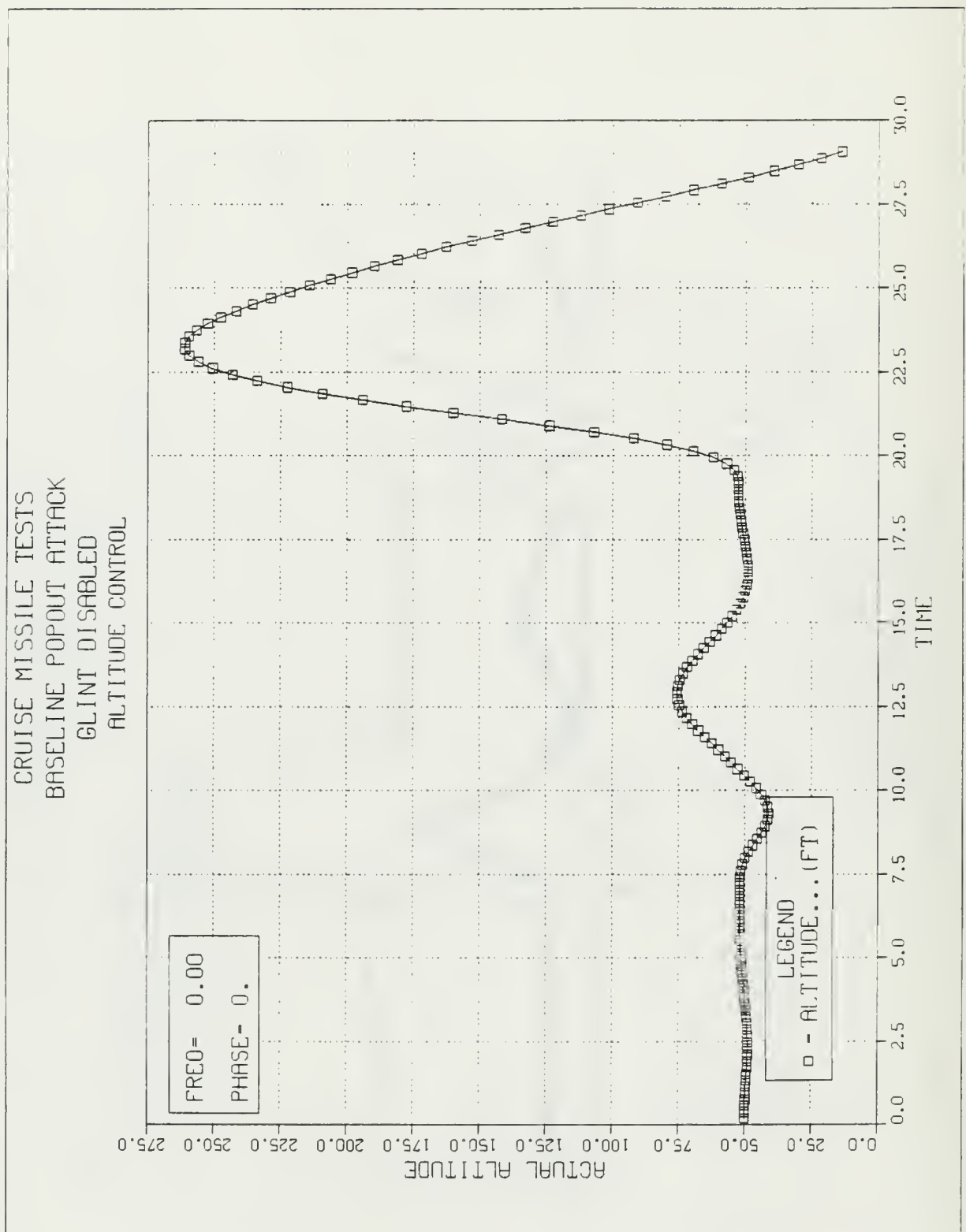


Figure A.27 Baseline - no ECM or GLINT - Altitude.

CRUISE MISSILE TESTS  
 BASELINE POPOUT ATTACK  
 GLINT DISABLED

FREQ= 0.  
 PHASE= 0.

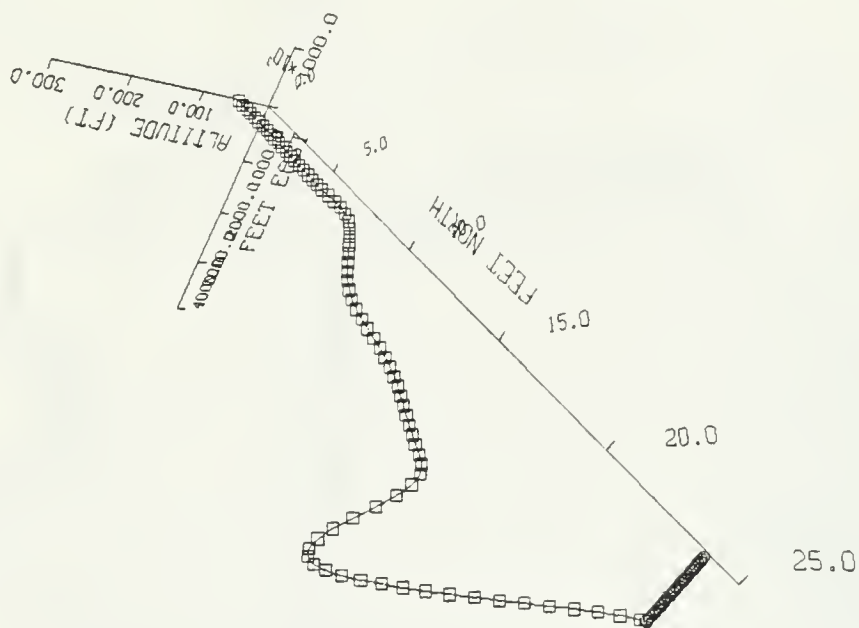


Figure A.28 Baseline - no ECM or GLINT - Geo Plot.



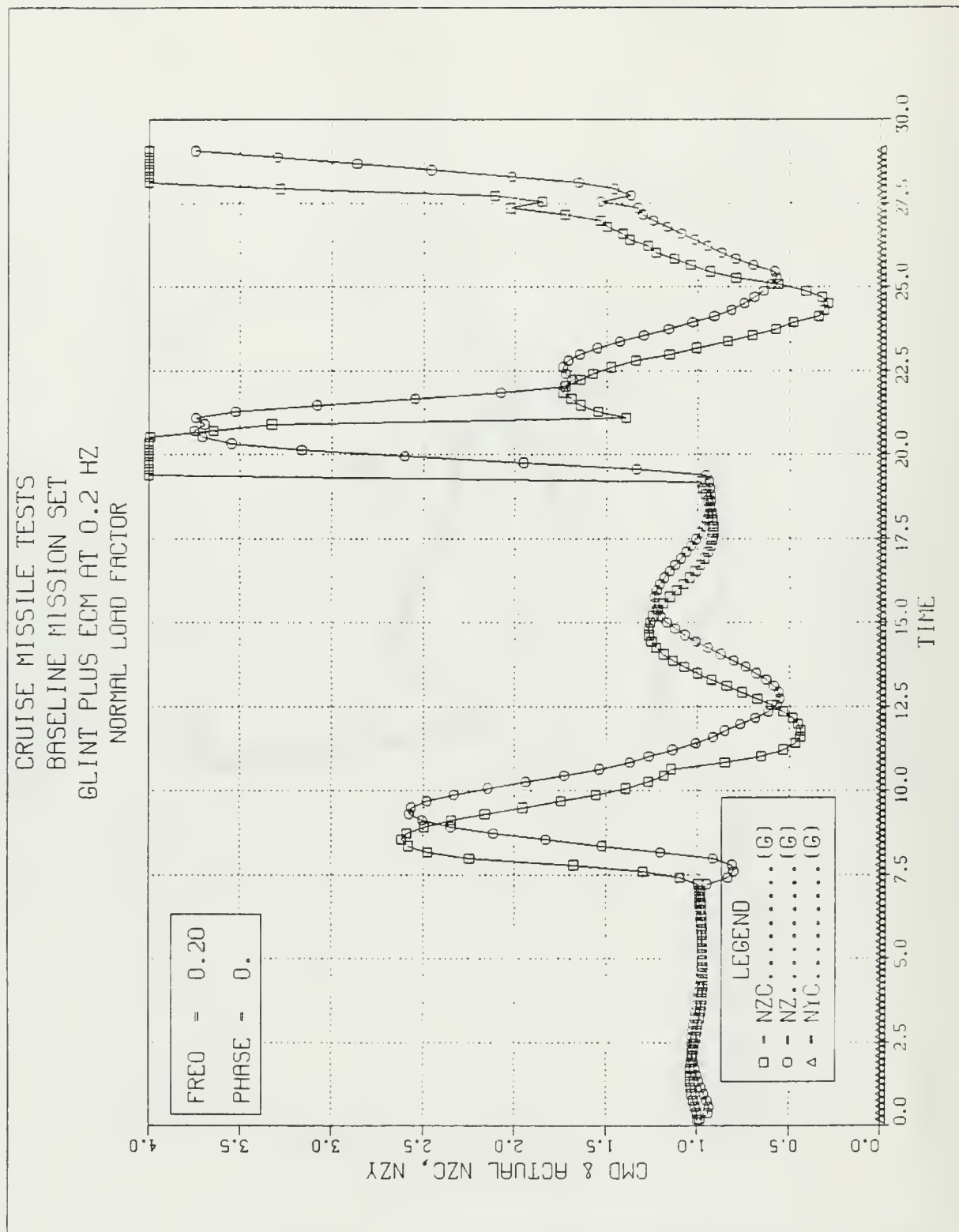


Figure A.29 Baseline with GLINT & ECM - Load Factor.

CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 BANK ANGLE CONTROL

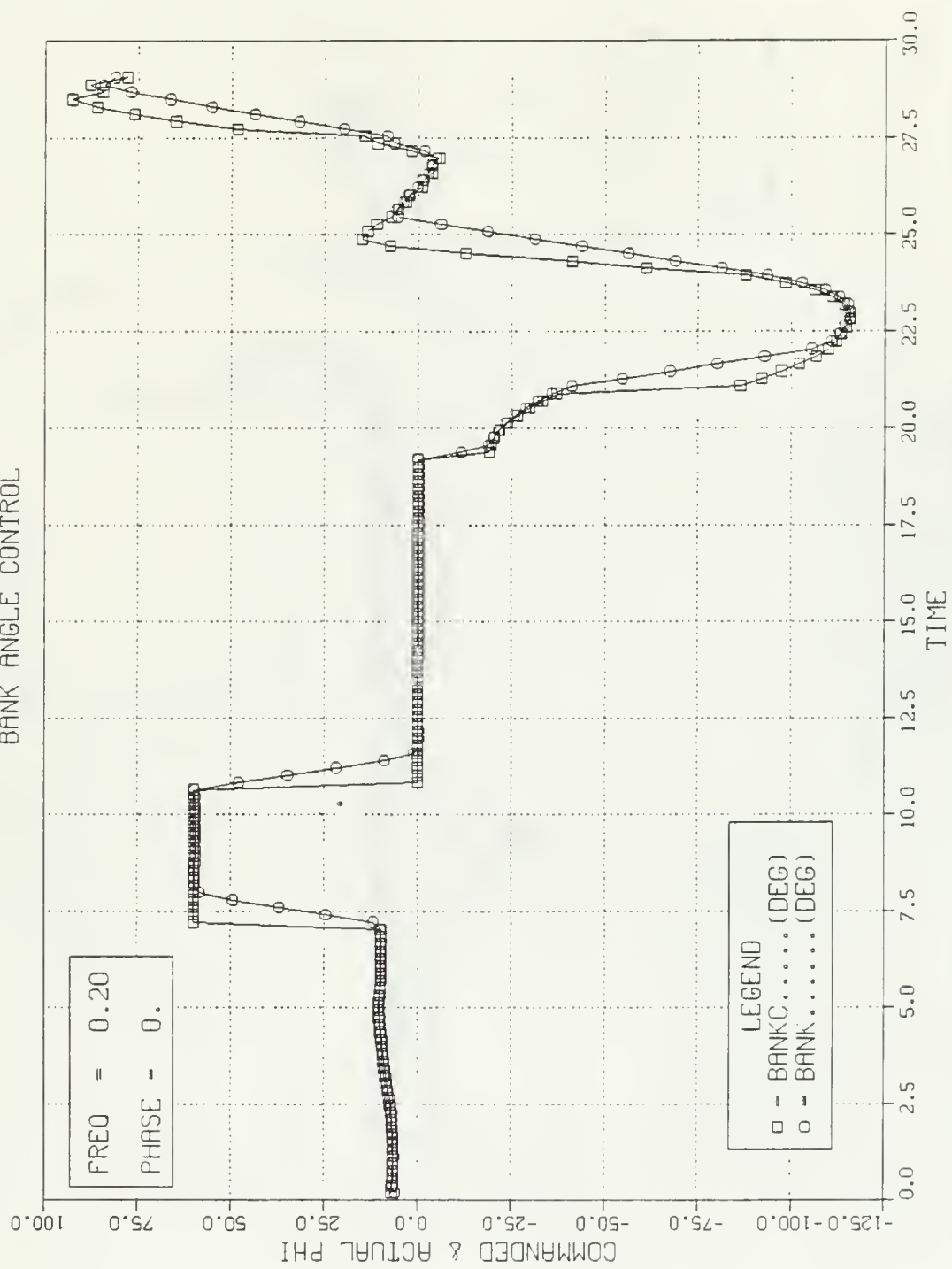


Figure A.30 Baseline with GLINT & ECM - Bank.

CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 ROLL RATE CONTROL

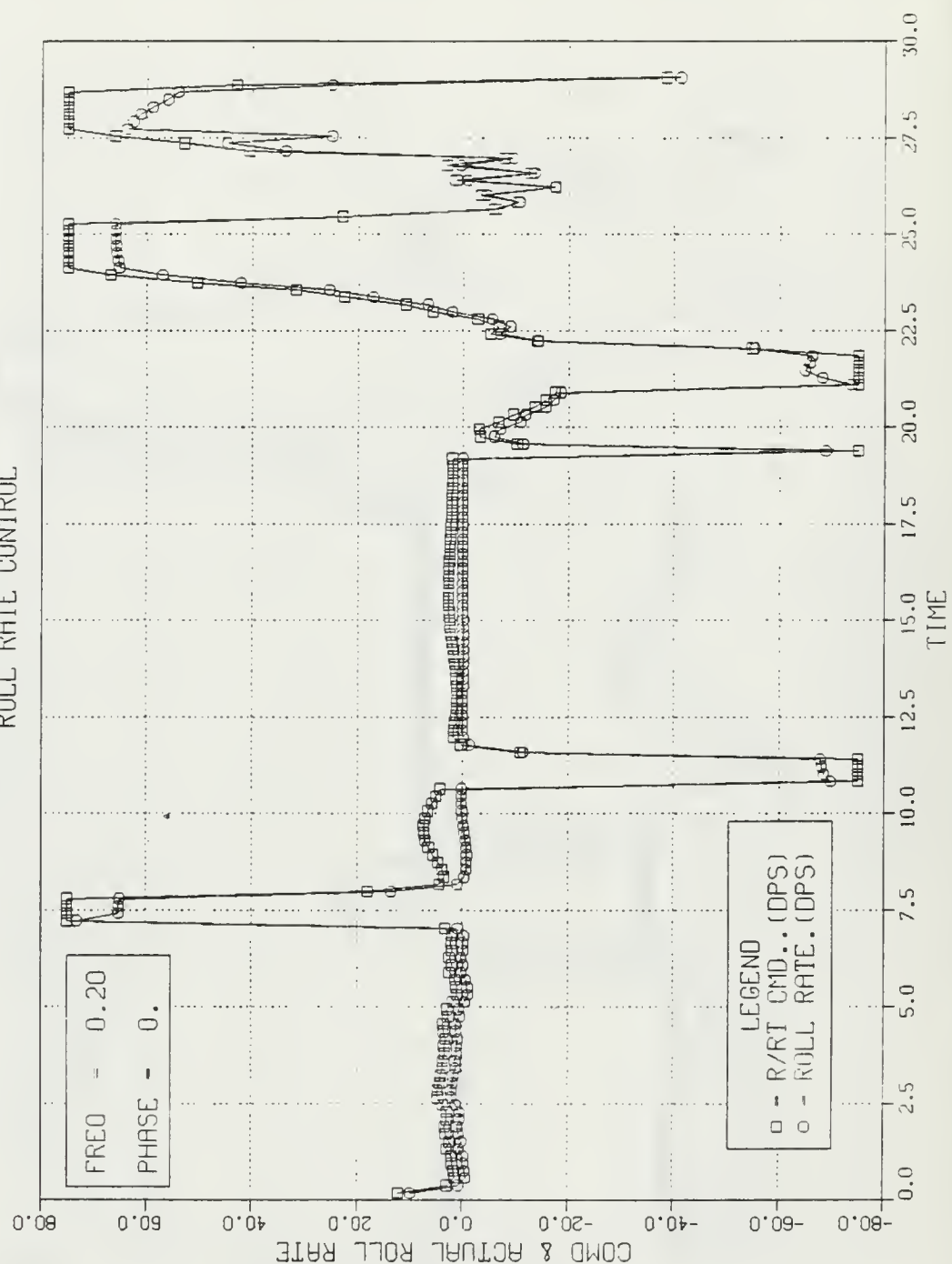


Figure A.31 Baseline with GLINT & ECM - Roll Rate.

CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 FLIGHT CONTROLS

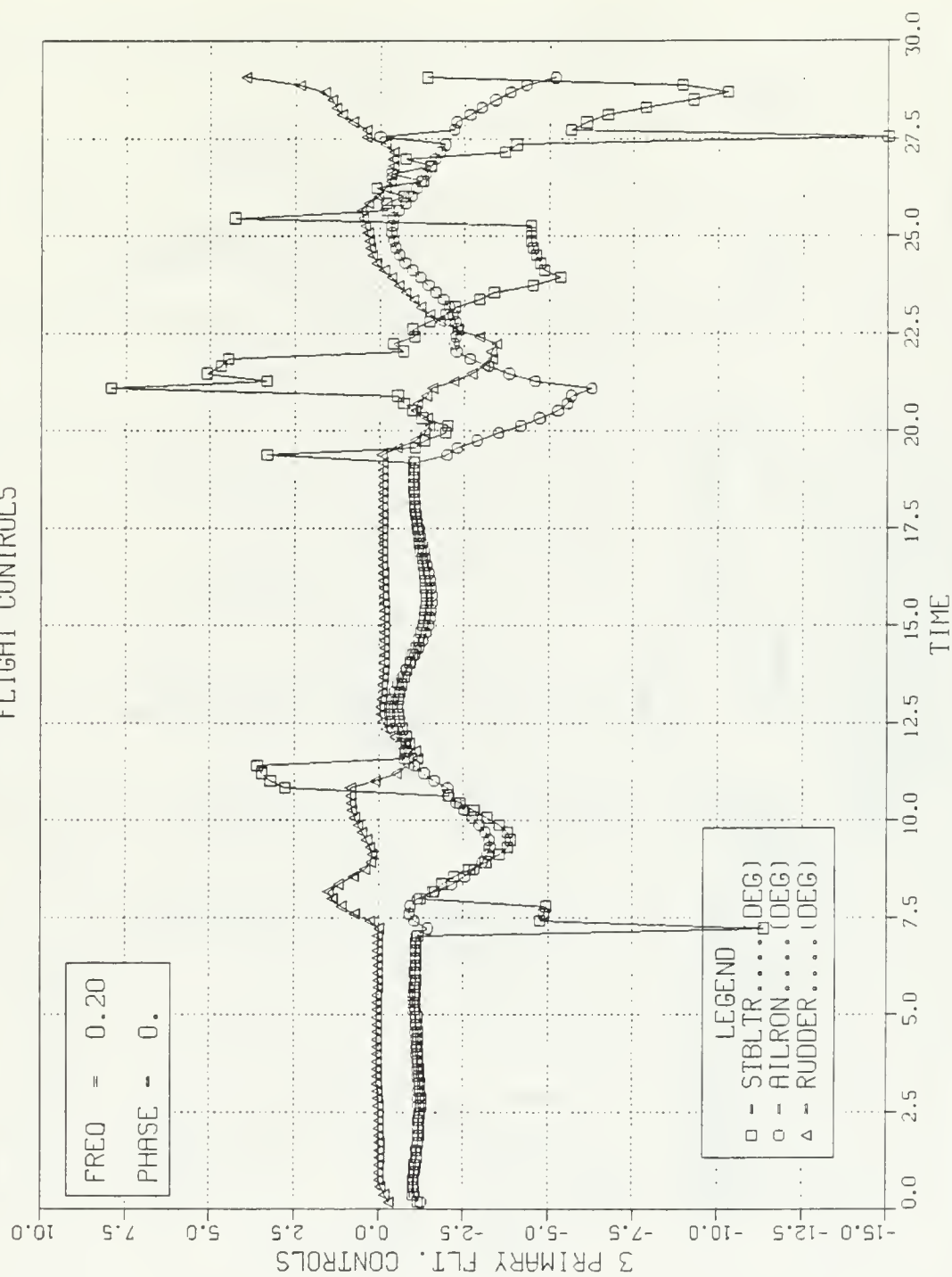


Figure A.32 Baseline with GLINT & ECM - Controls.

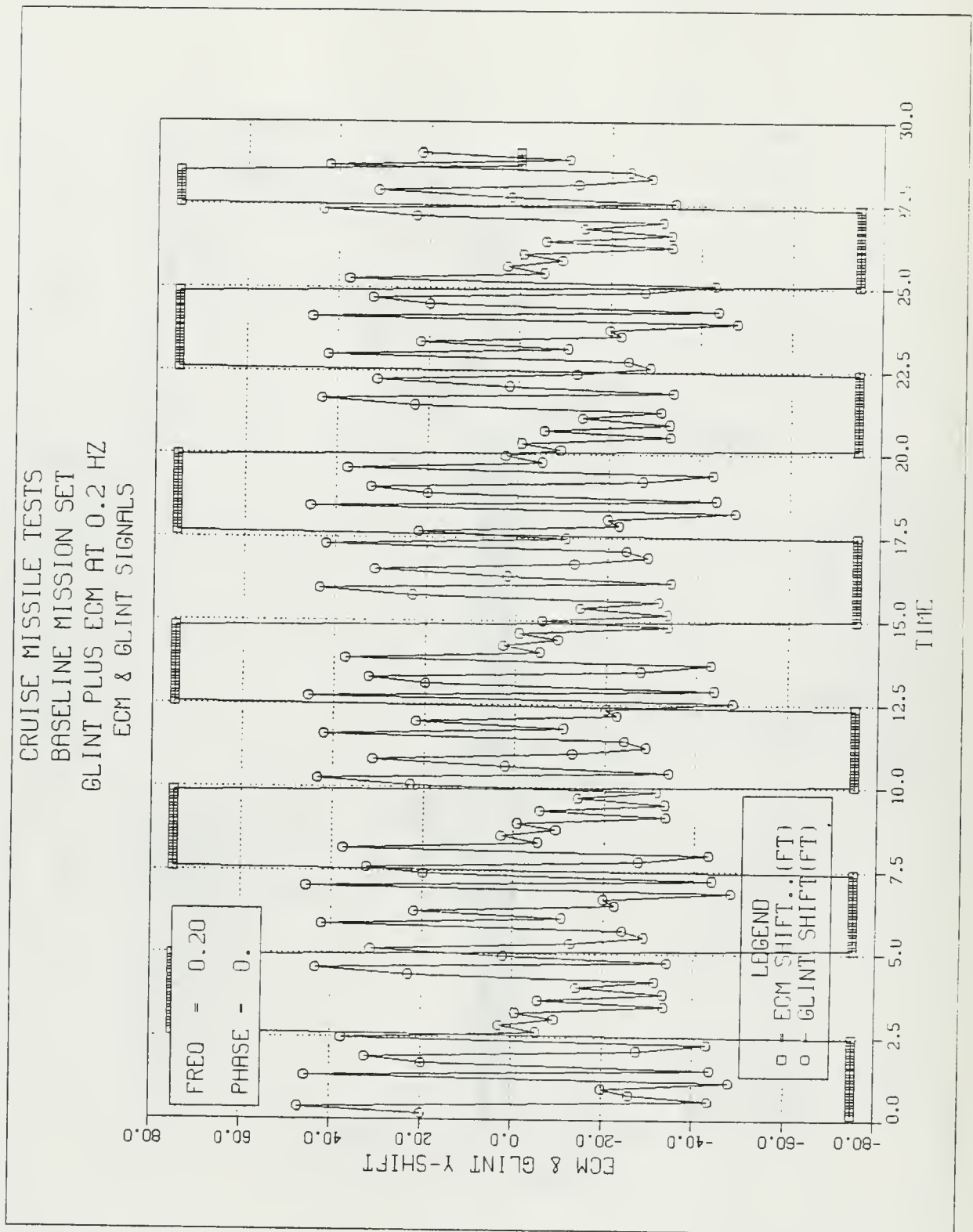


Figure A.33 Baseline with GLINT & ECM - ECM & GLINT.



CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 ALTITUDE CONTROL

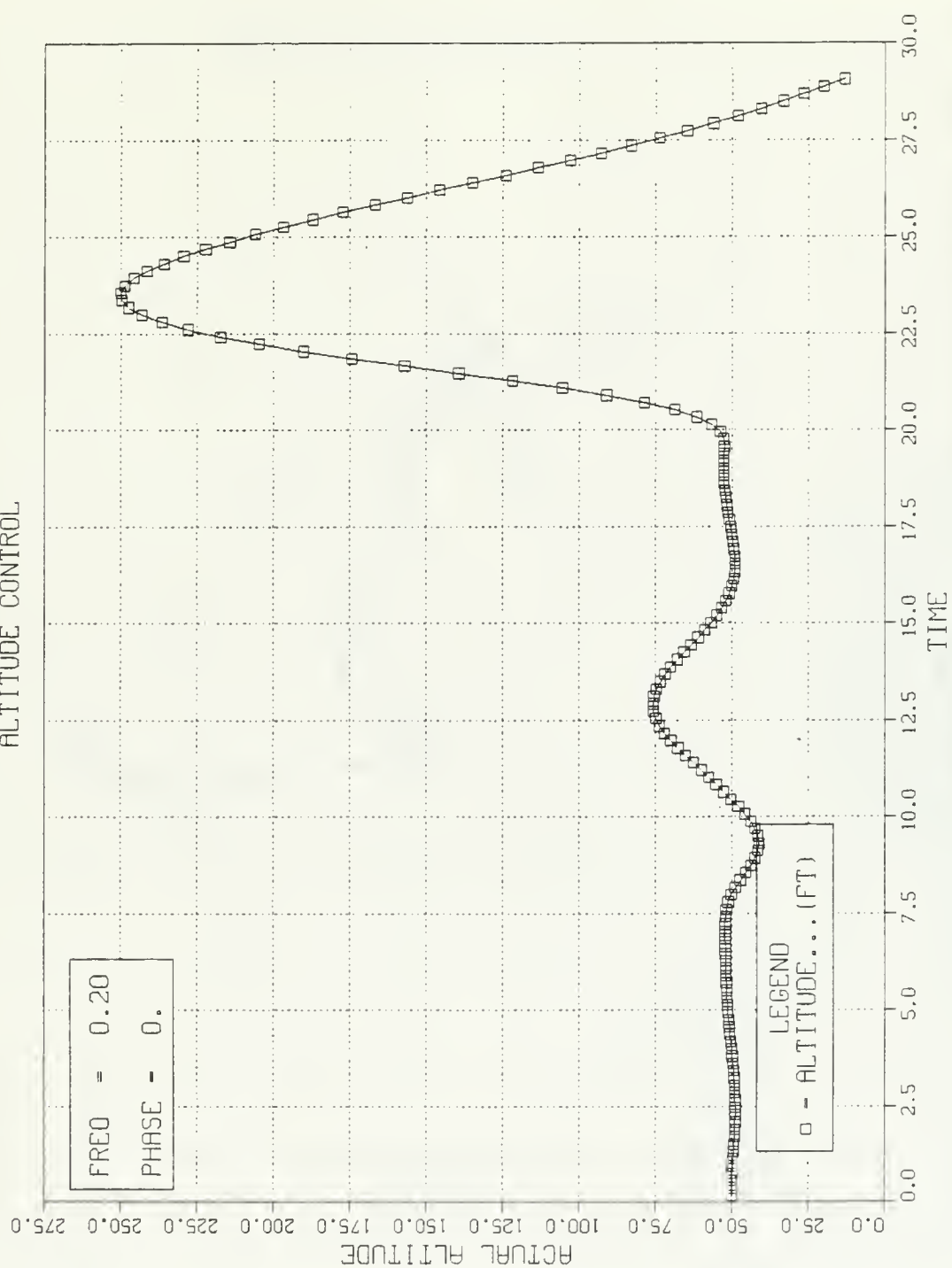


Figure A.34 Baseline with GLINT & ECM - Altitude.

CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 GEOGRAPHICAL TRACKS

FREQ	=	0.20
PHASE	=	0.



Figure A.35 Baseline with GLINT & ECM - Geo Plot.

# BASELINE SCAN RESULTS

## MISS DISTANCES

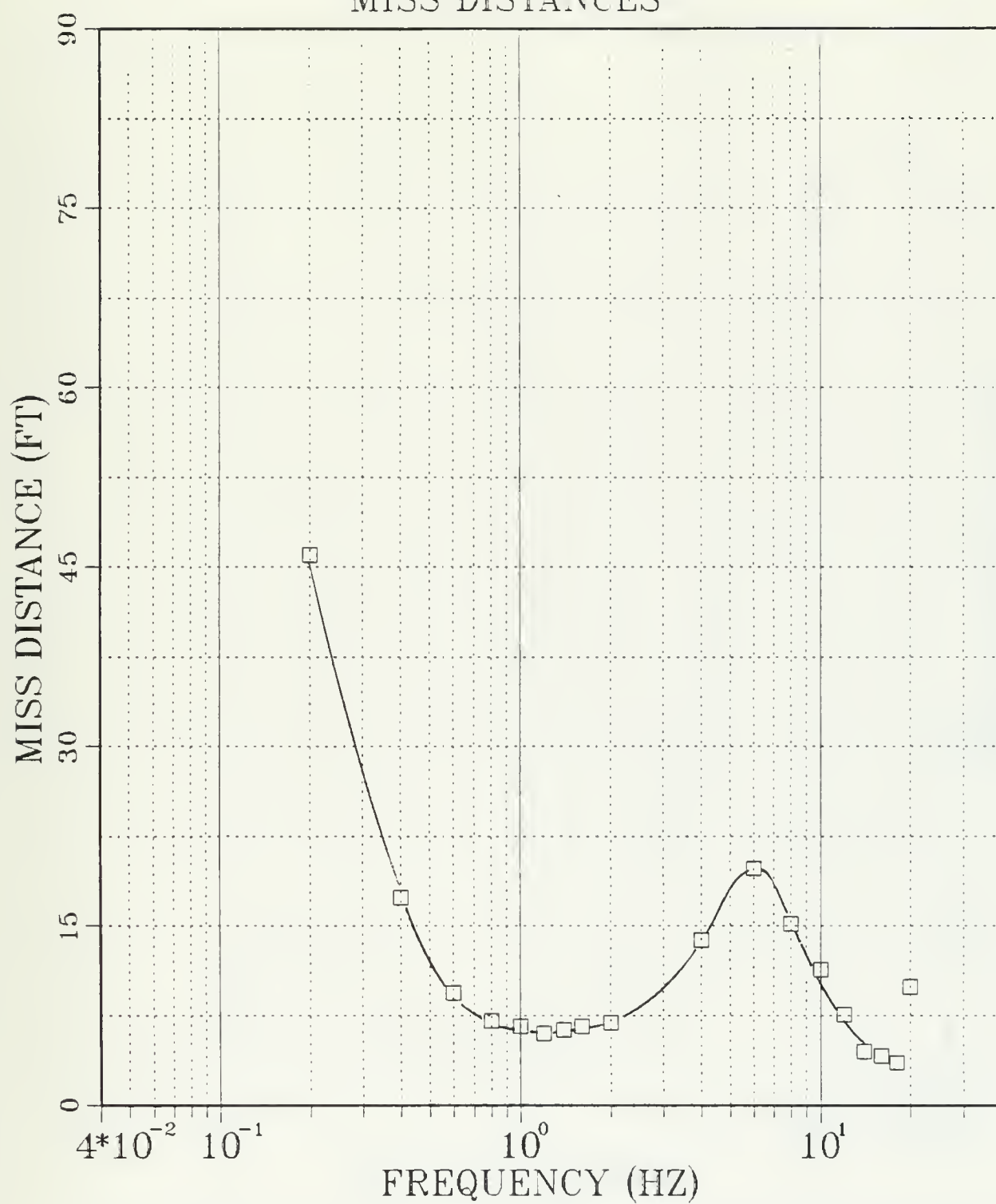


Figure A.36 Mean Miss Distances - Baseline.

# CONFIGURATION II SCANS

## MISS DISTANCES

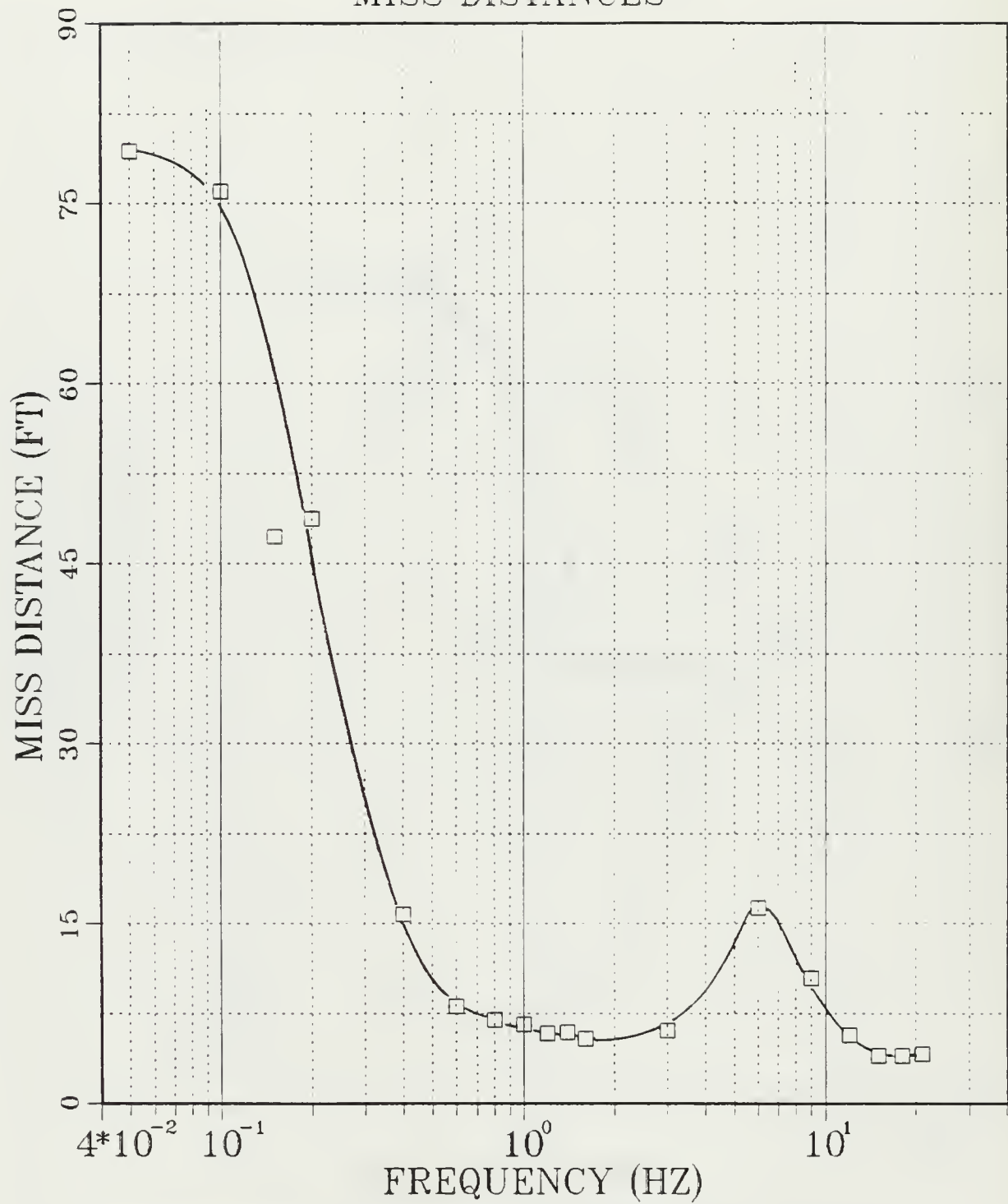


Figure A.37 Mean Miss Distances - Configuration II.

# CONFIGURATION III SCANS

## MISS DISTANCES

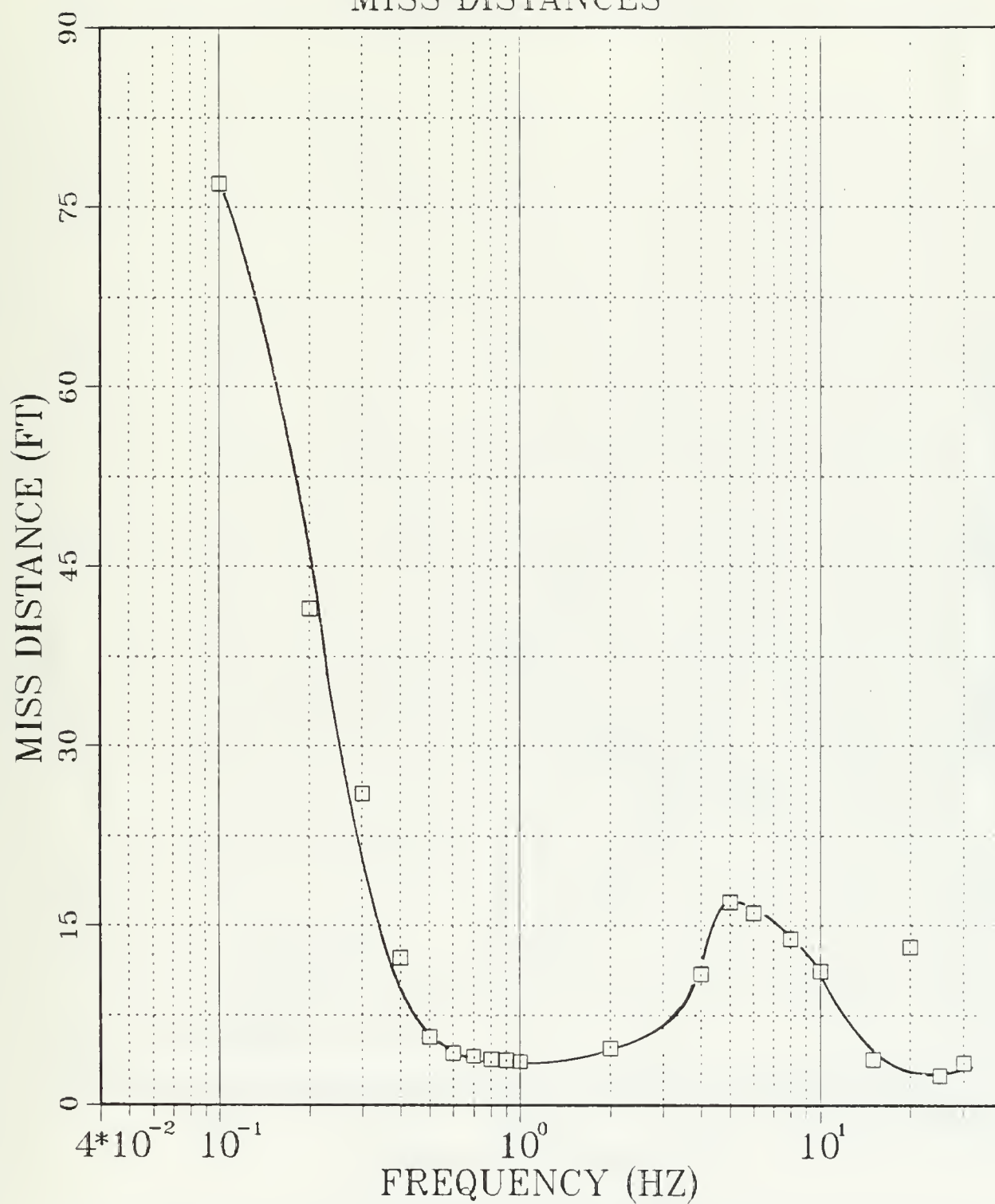


Figure A.38 Mean Miss Distances - Configuration III.



# CONFIGURATION IV SCANS

## MISS DISTANCES

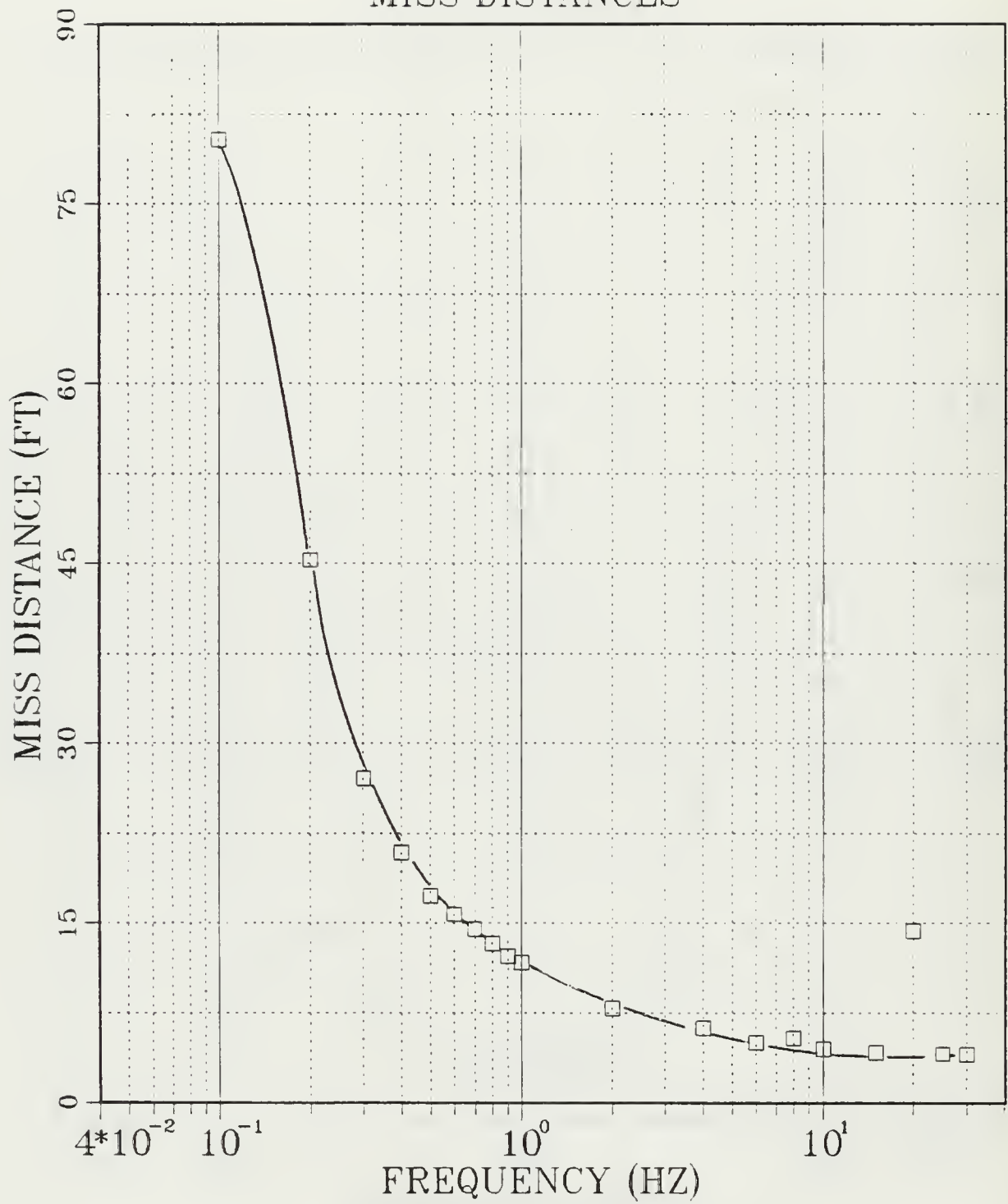


Figure A.39 Mean Miss Distances - Configuration IV.

# BASELINE SCAN RESULTS

## AUTOPILOT ERRORS

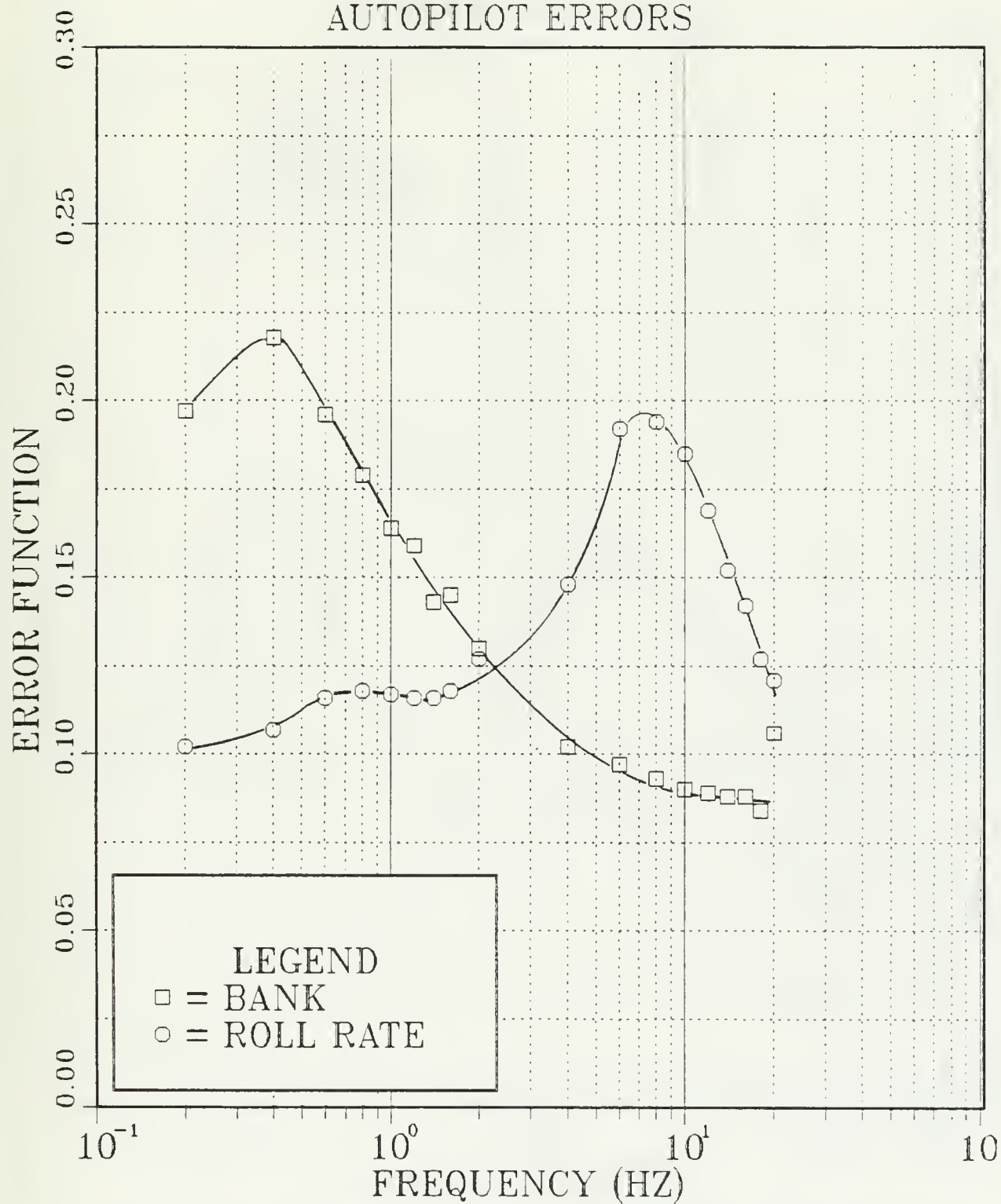


Figure A.40 Autopilot Errors - Baseline.

# CONFIGURATION II SCANS

## AUTOPILOT ERRORS

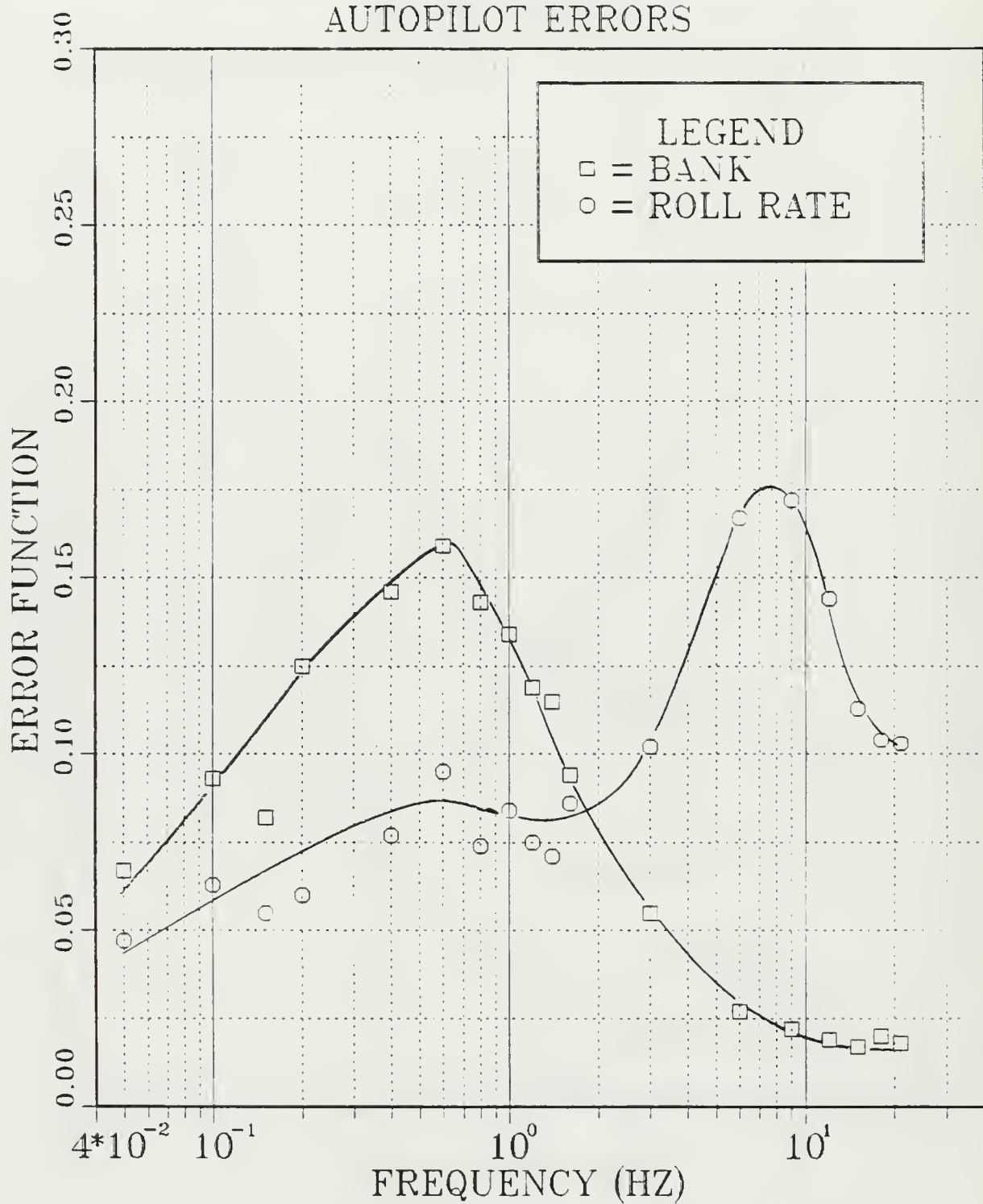


Figure A.41 Autopilot Errors - Configuration II.

# CONFIGURATION III SCANS

## AUTOPILOT ERRORS

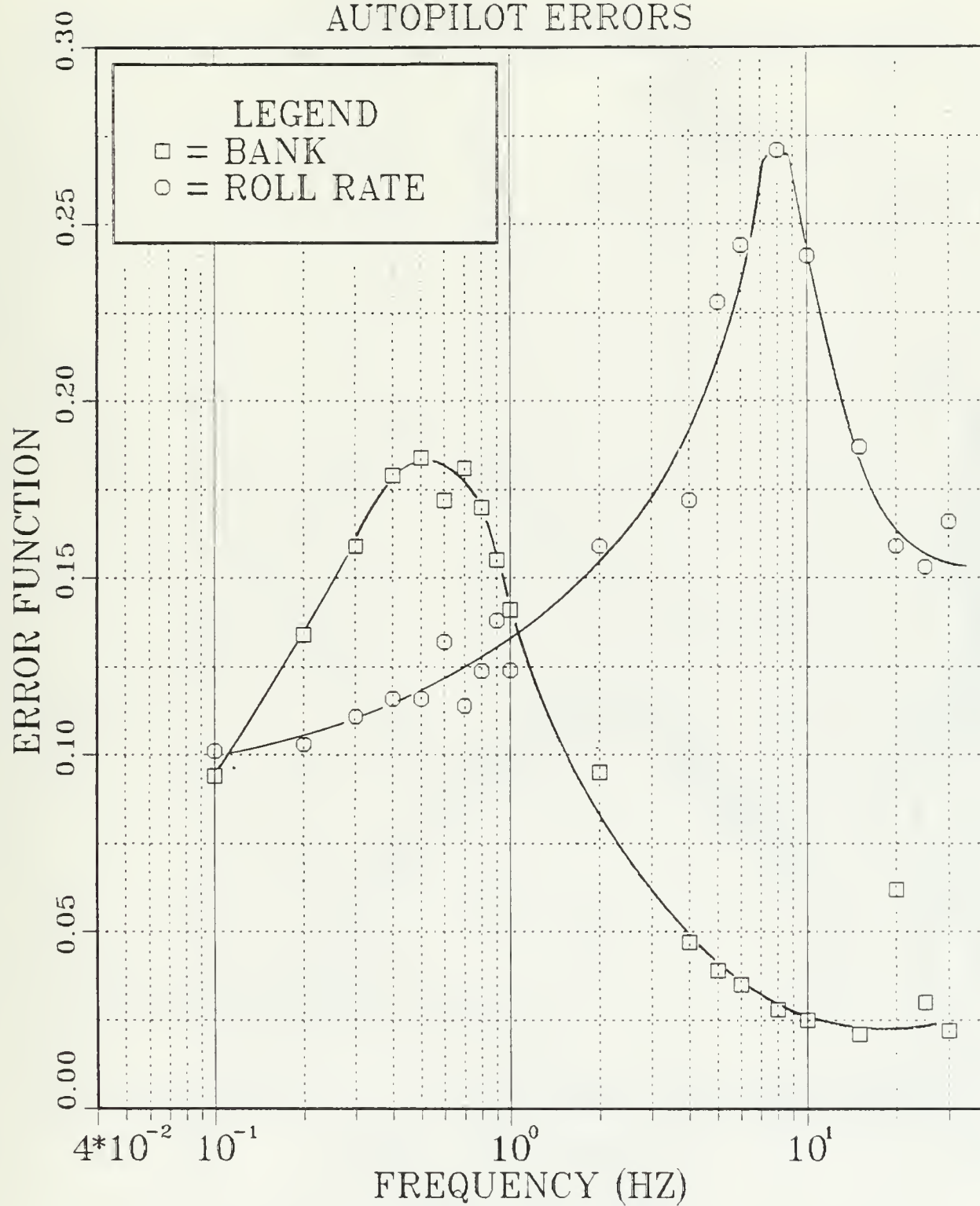


Figure A.42 Autopilot Errors - Configuration III.

# CONFIGURATION IV SCANS

## AUTOPILOT ERRORS

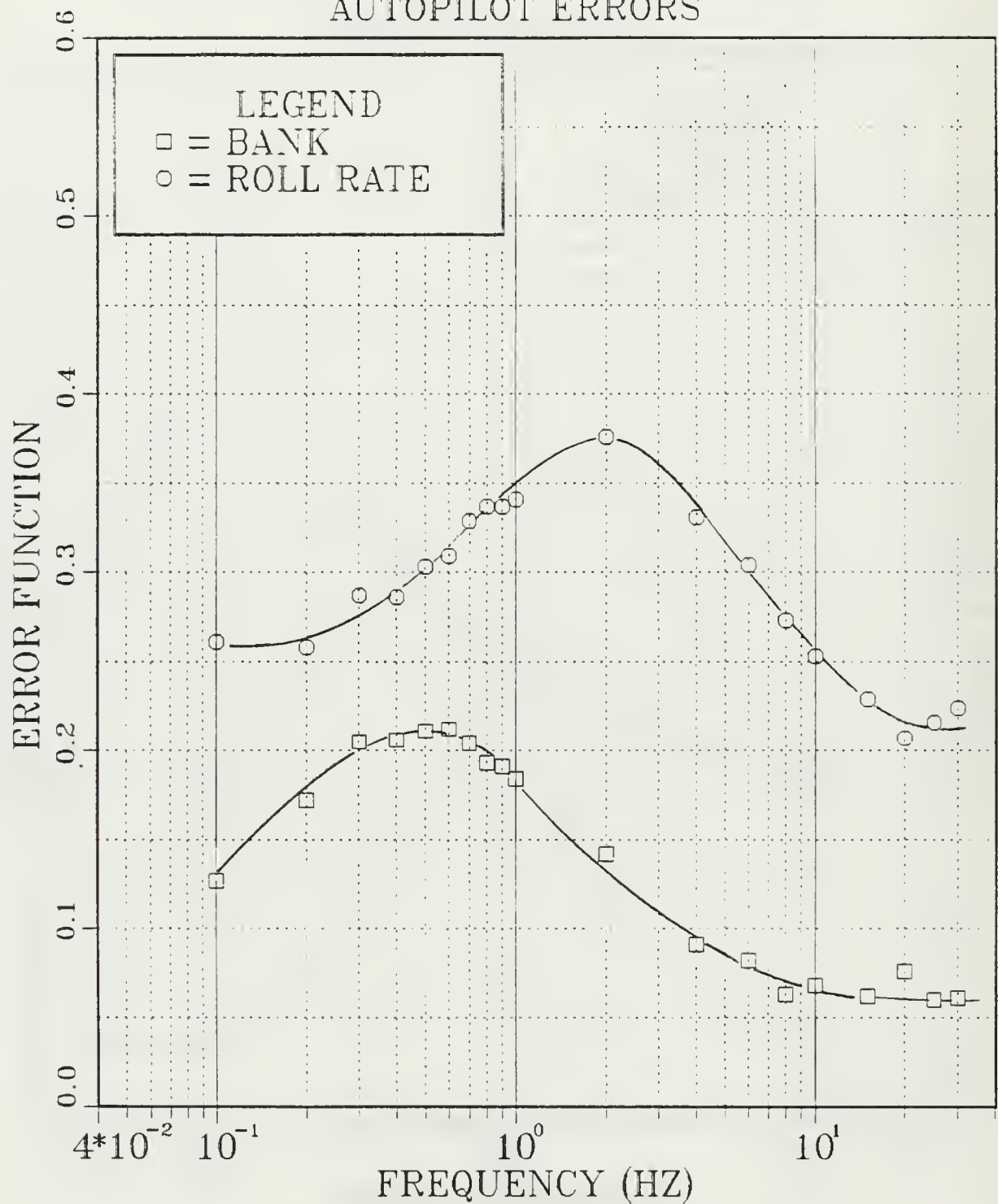


Figure A.43 Autopilot Errors - Configuration IV.

# BASELINE SCAN RESULTS

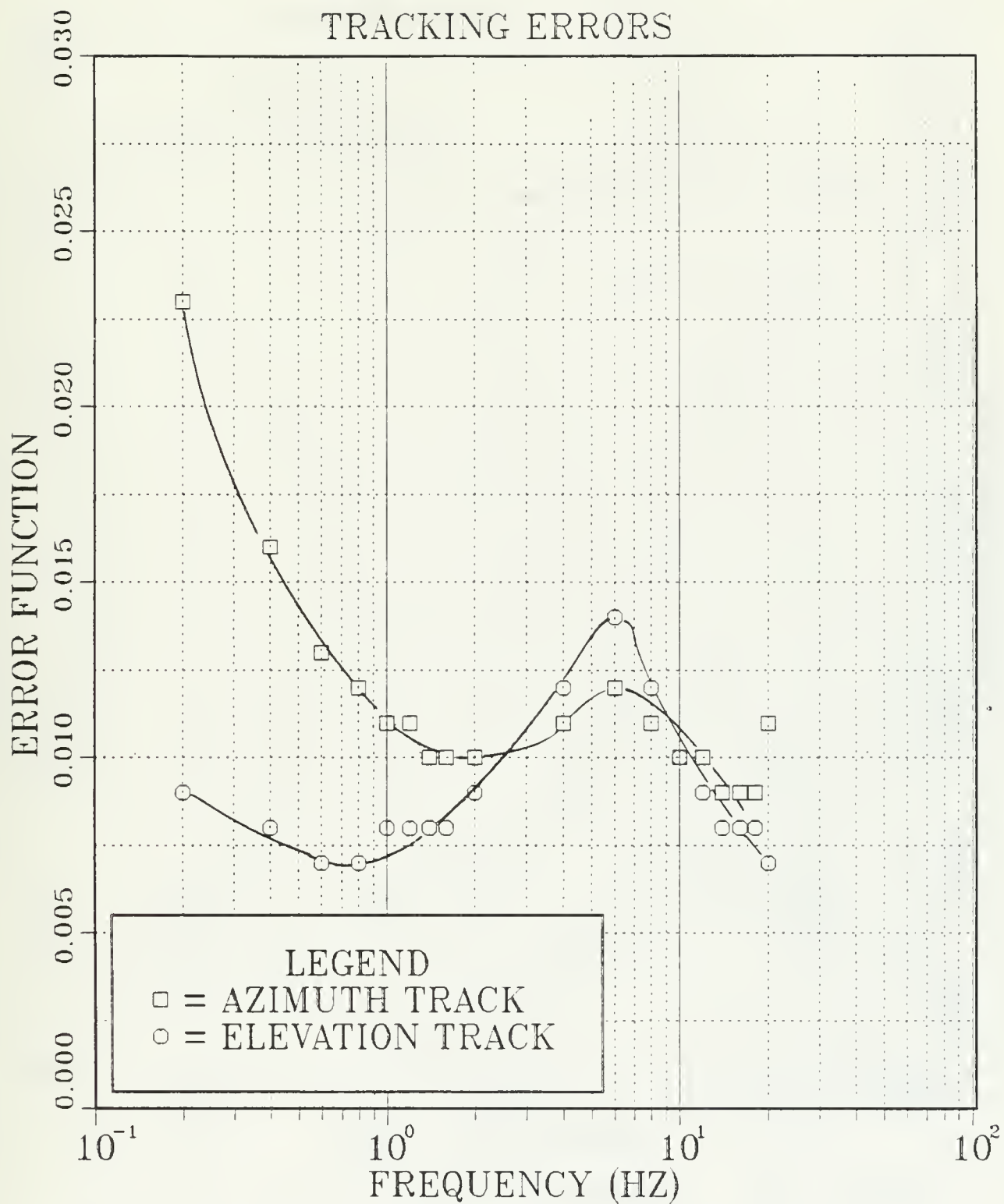


Figure A.44 Tracking Errors - Baseline.



# CONFIGURATION II SCANS

## TRACKING ERRORS

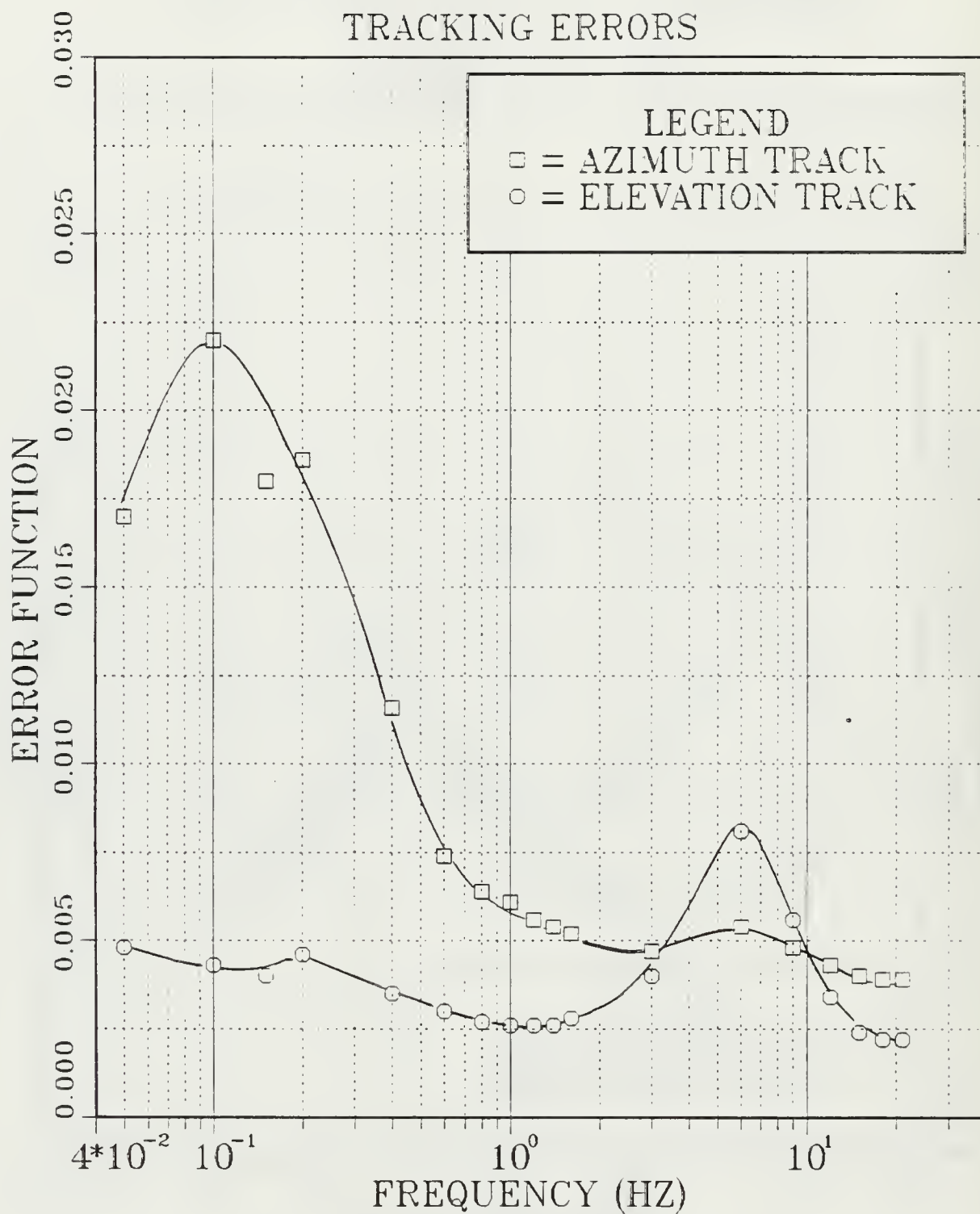


Figure A.45 Tracking Errors - Configuration II.

# CONFIGURATION III SCANS

## TRACKING ERRORS

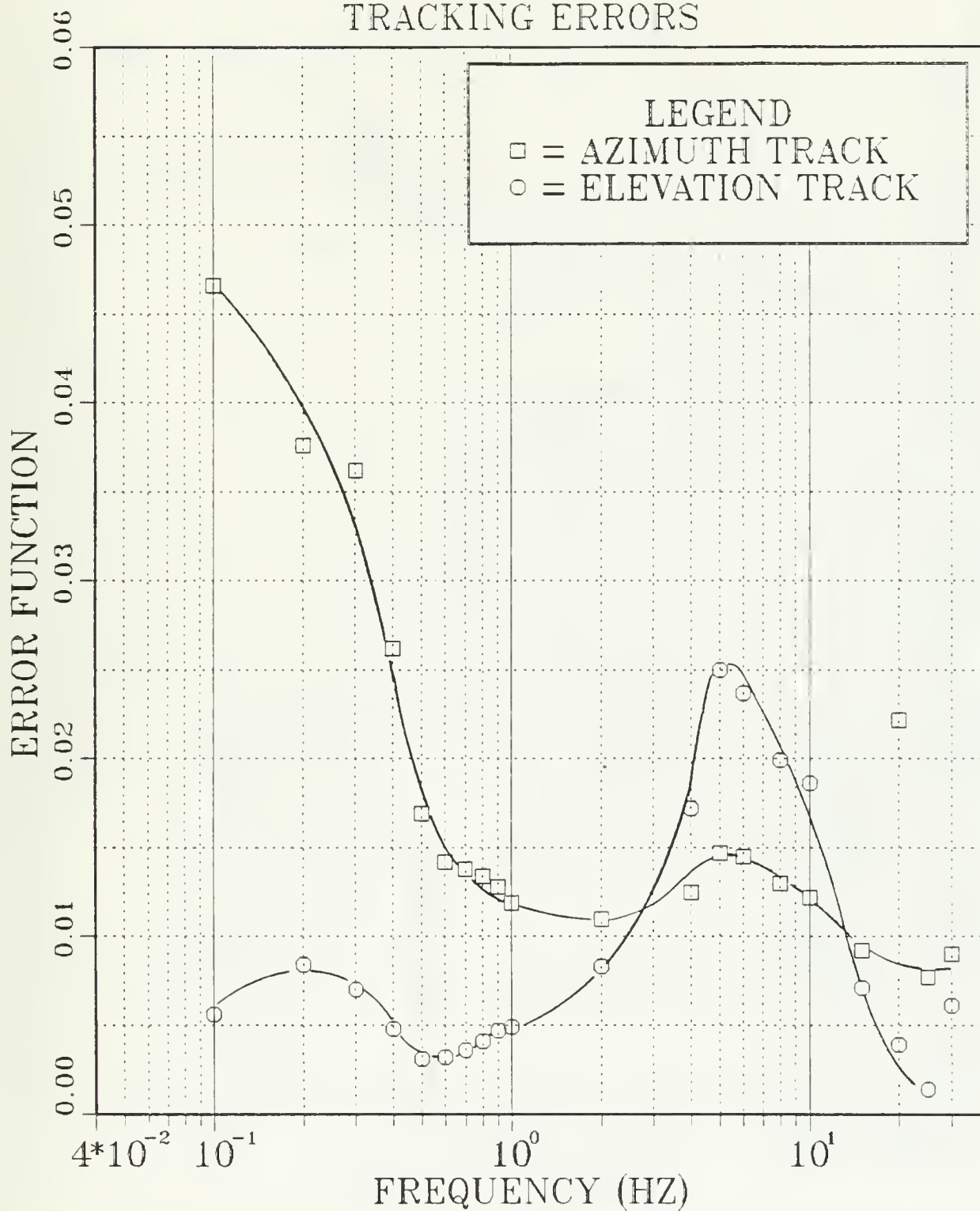


Figure A.46 Tracking Errors - Configuration III.

# CONFIGURATION IV SCANS

## TRACKING ERRORS

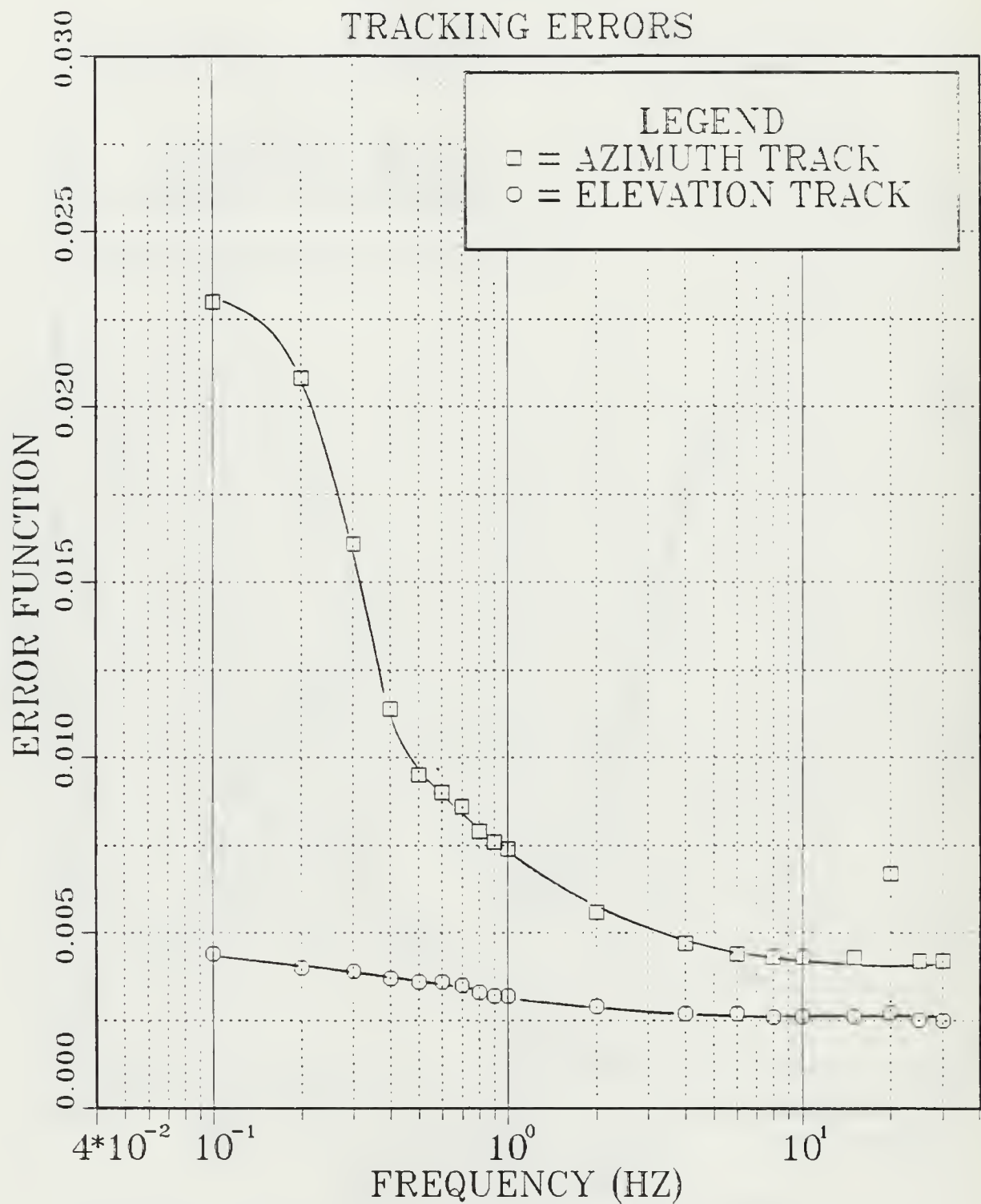


Figure A.47 Tracking Errors - Configuration IV.

CRUISE MISSILE TESTS  
 BASELINE POPOUT ATTACK-NO GLNT  
 LO-FREQUENCY SCAN 0.2-1.6 HZ  
 BANK ANGLE CONTROL

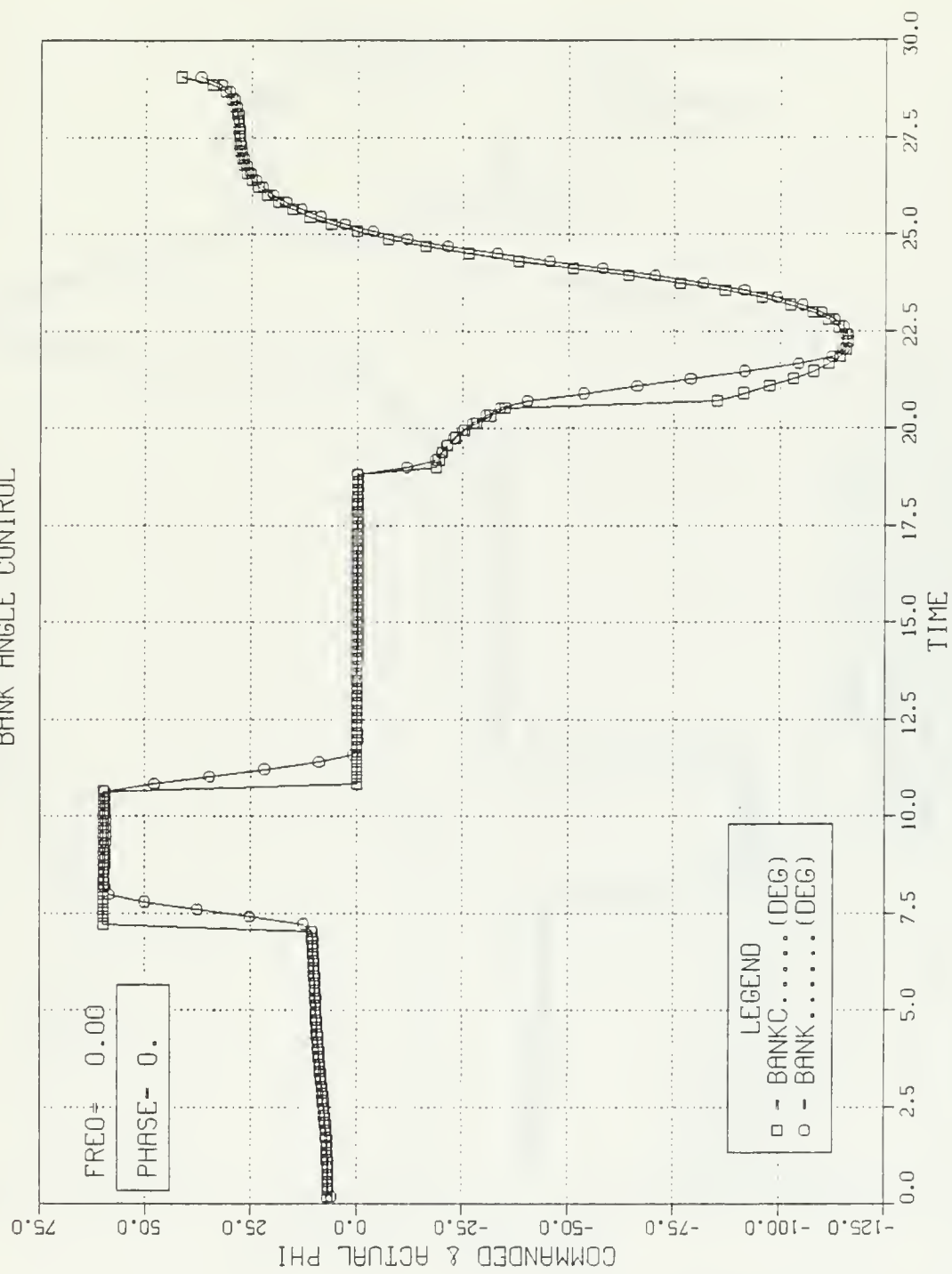


Figure A.48 Baseline/ECM Freq = 0.0 Hz - Bank.

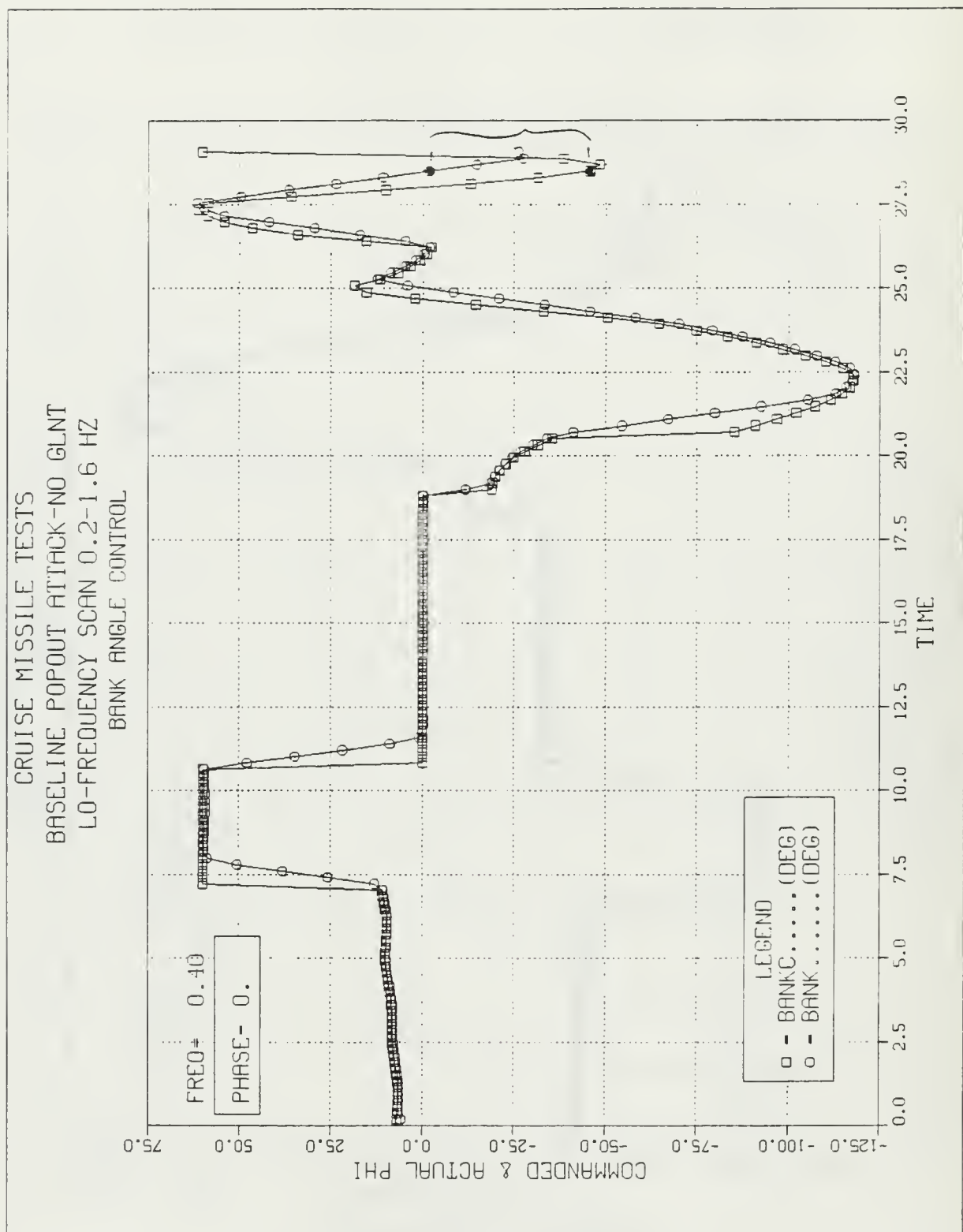


Figure A.49 Baseline/ECM Freq = 0.4 Hz - Bank.

CRUISE MISSILE TESTS  
 BASELINE POPOUT ATTACK-NO GLNT  
 HI-FREQUENCY SCAN 0.0-20. HZ  
 BANK ANGLE CONTROL

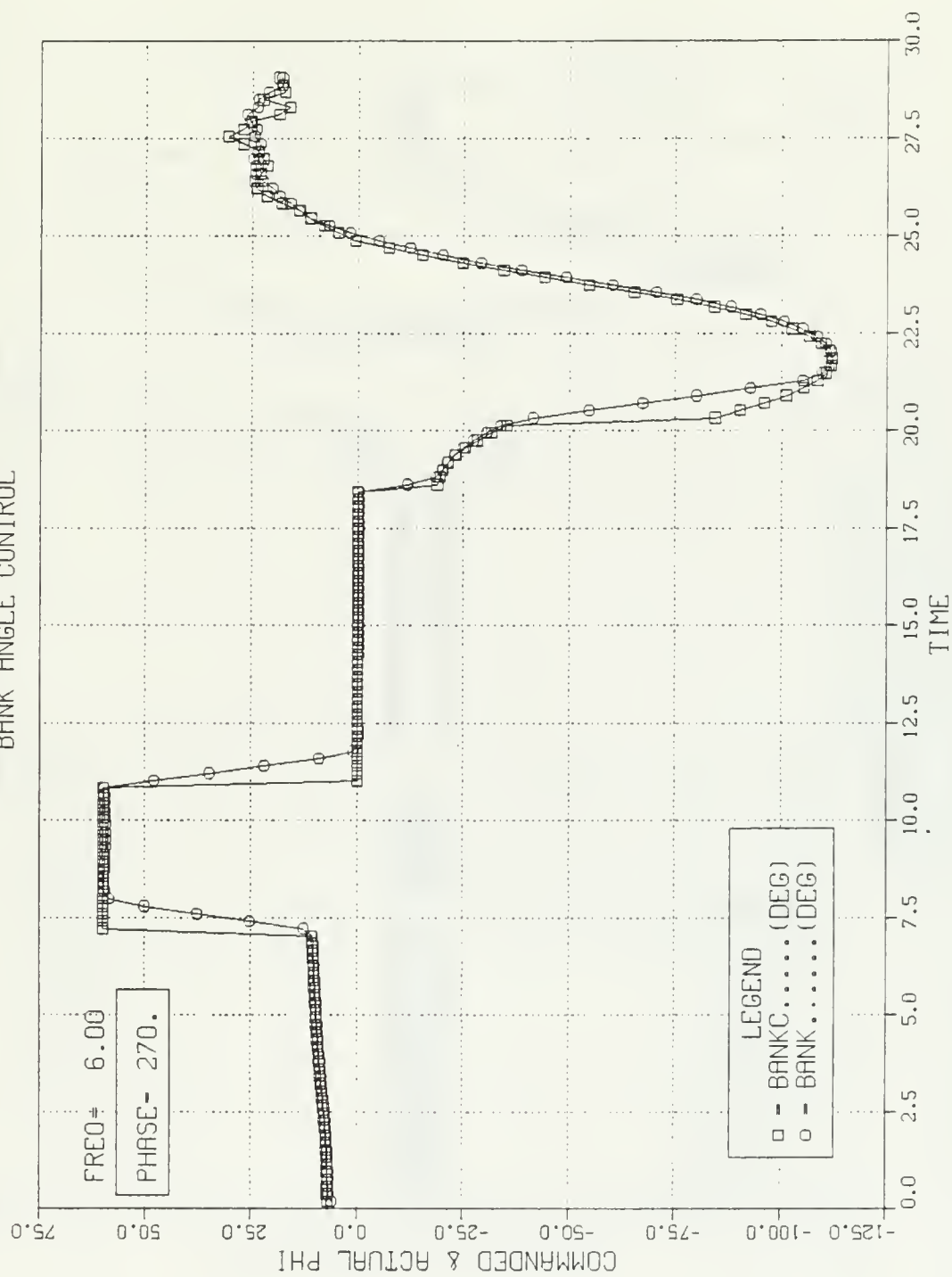


Figure A.50 Baseline/ECM Freq = 6.0 Hz - Bank.



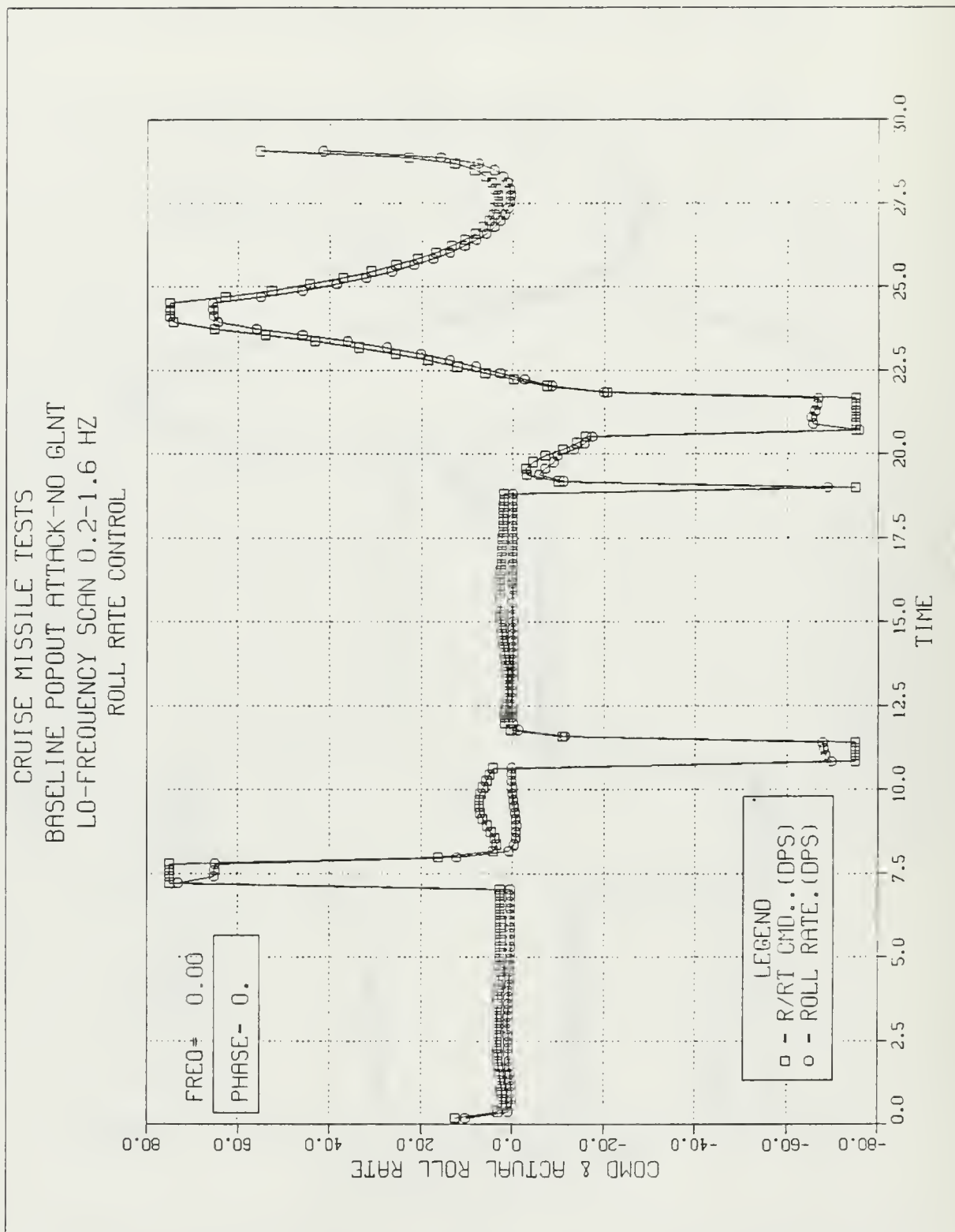


Figure A.51 Baseline/ECM Freq = 0.0 Hz - Roll Fate.

CRUISE MISSILE TESTS  
 BASELINE POPOUT ATTACK-NO GLNT  
 LO-FREQUENCY SCAN 0.2-1.6 HZ  
 ROLL RATE CONTROL

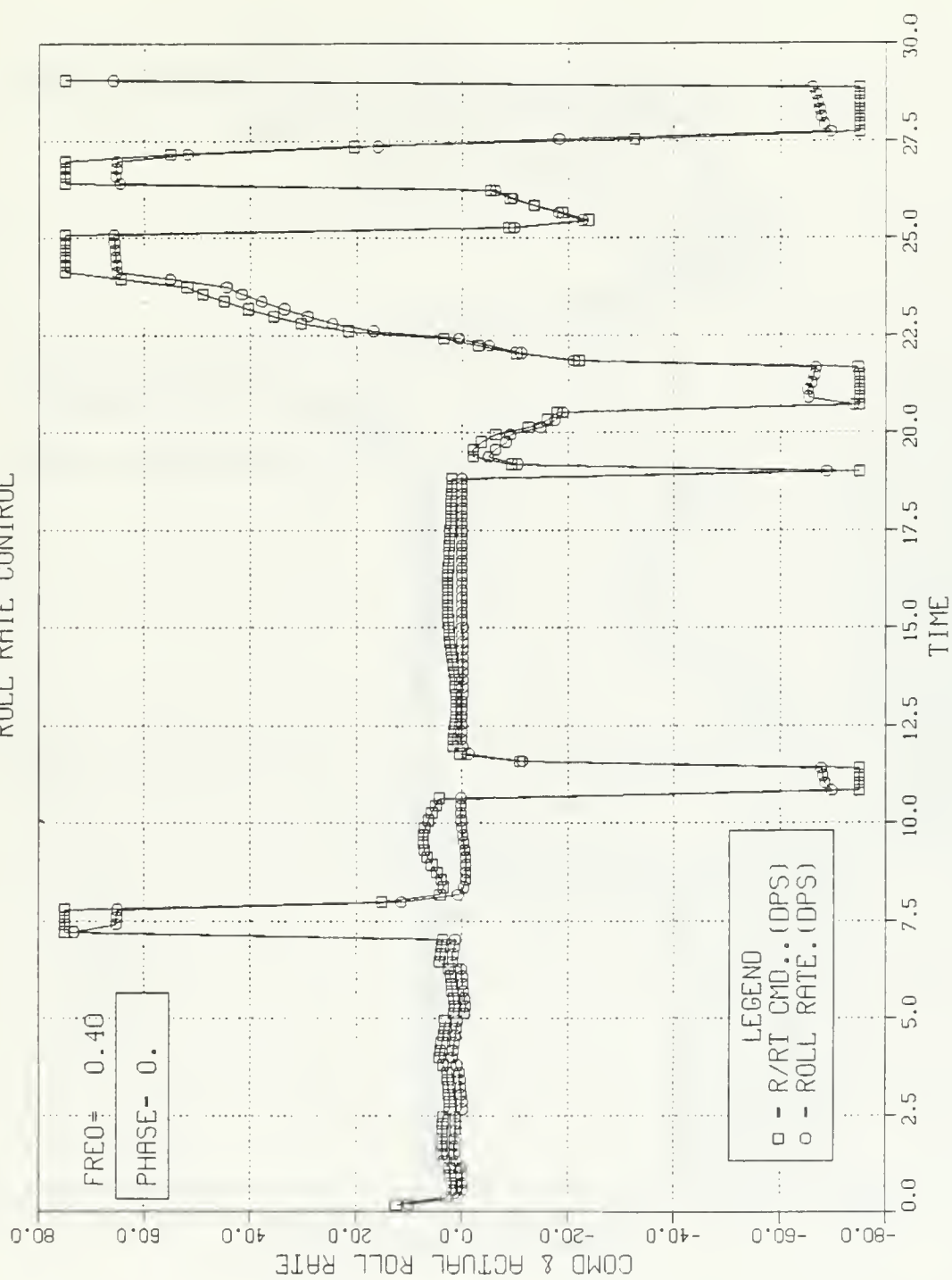


Figure A.52 Baseline/ECM Freq = 0.4 Hz - Roll Rate.

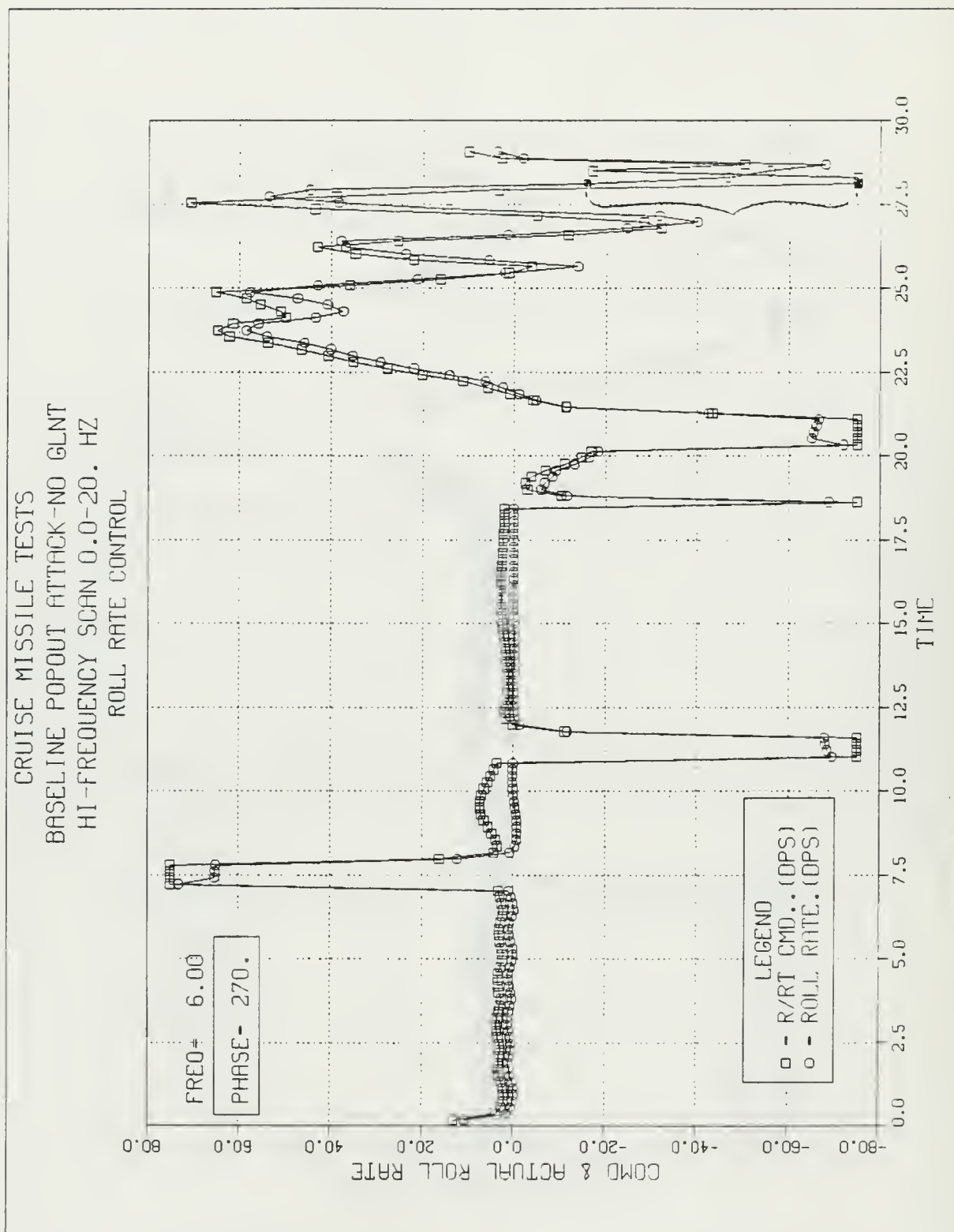


Figure A.53 Baseline/ECM Freq = 6.0 Hz - Roll Rate.

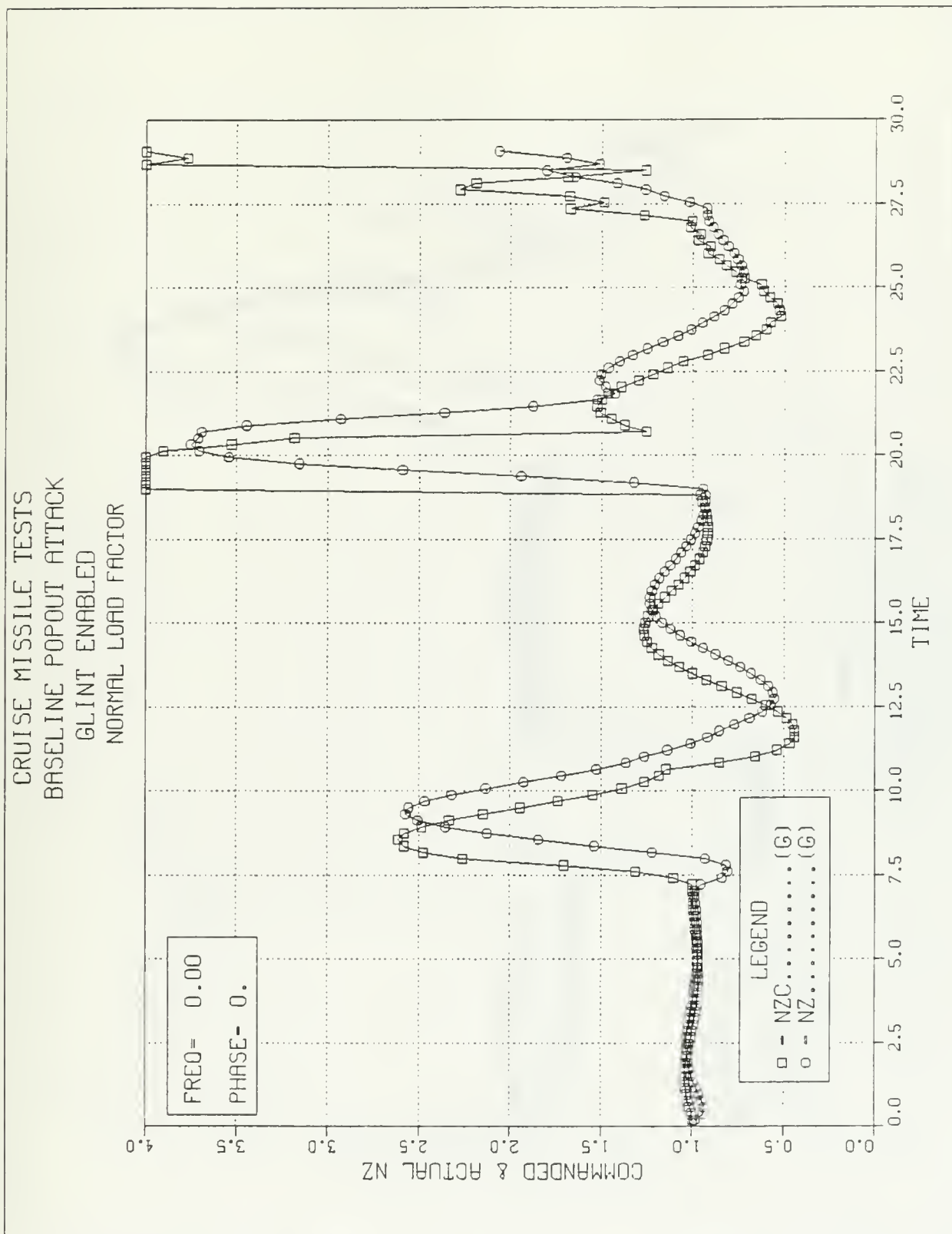


Figure A.54 Baseline with GLINT only - Load Factor.

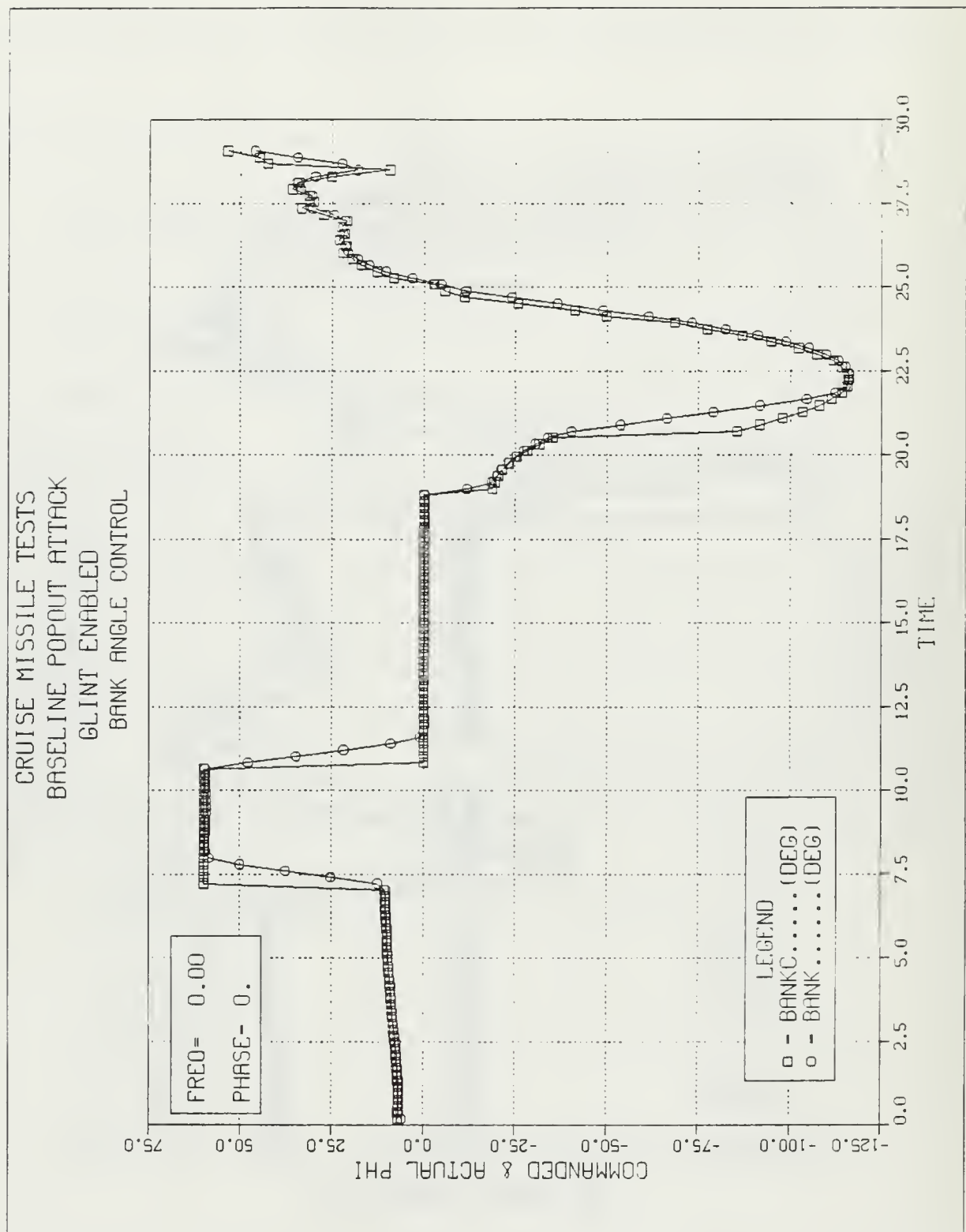


Figure A.55 Baseline with GLINT only - Bank.

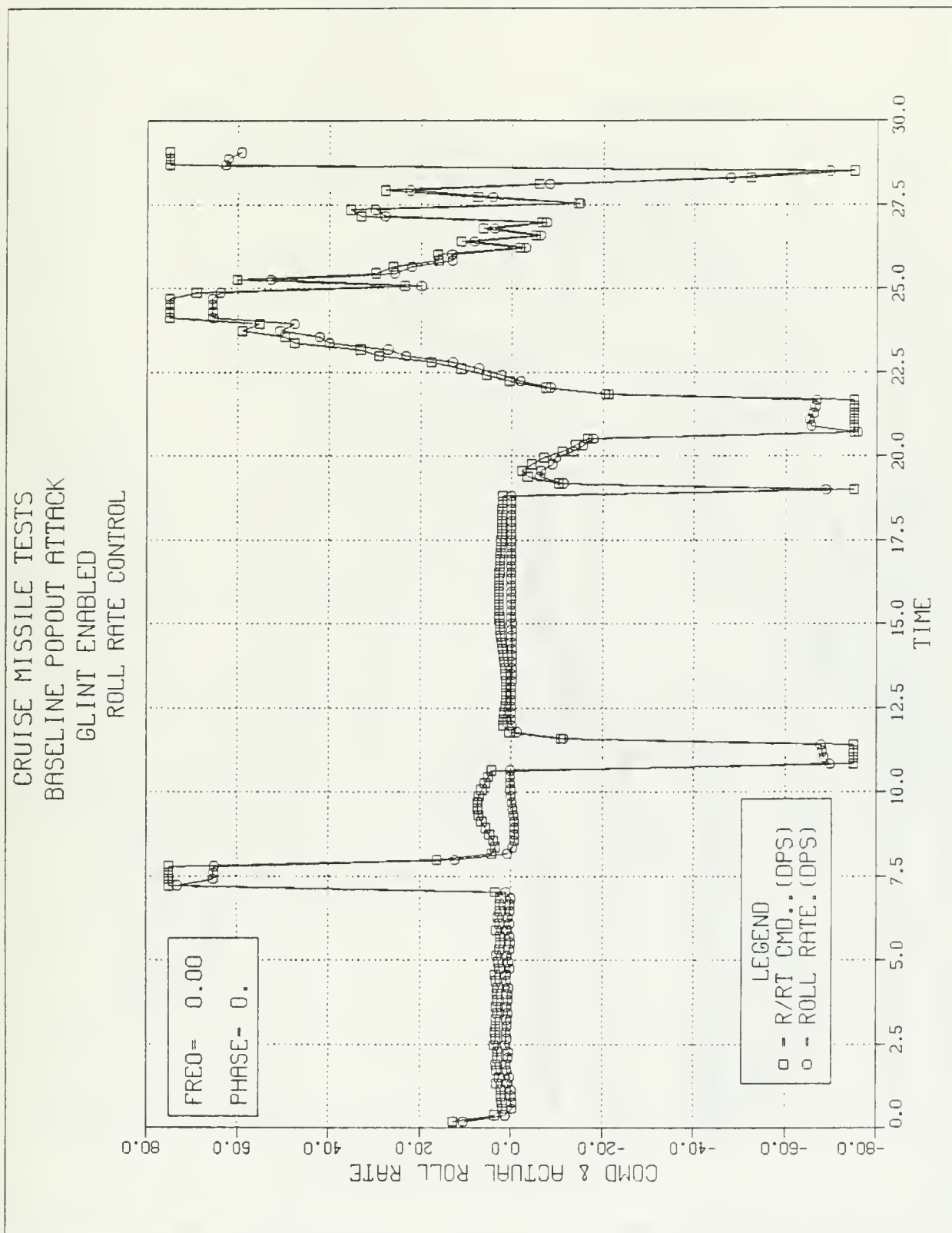


Figure A.56 Baseline with GLINT only - Roll Rate.



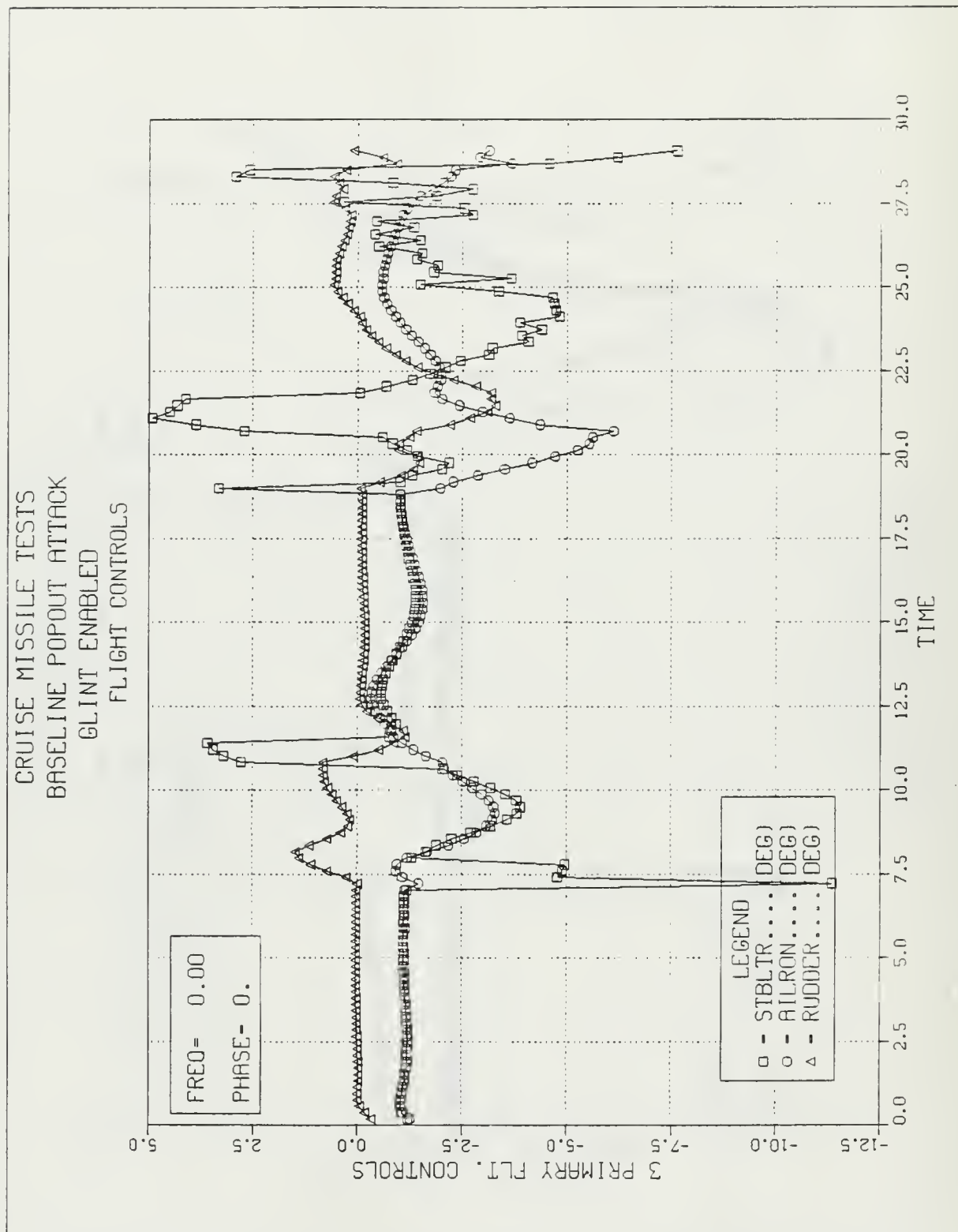


Figure A.57 Baseline with GLINT only - Controls.

CRUISE MISSILE TESTS  
 CONFIGURATION II MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 NORMAL LOAD FACTOR

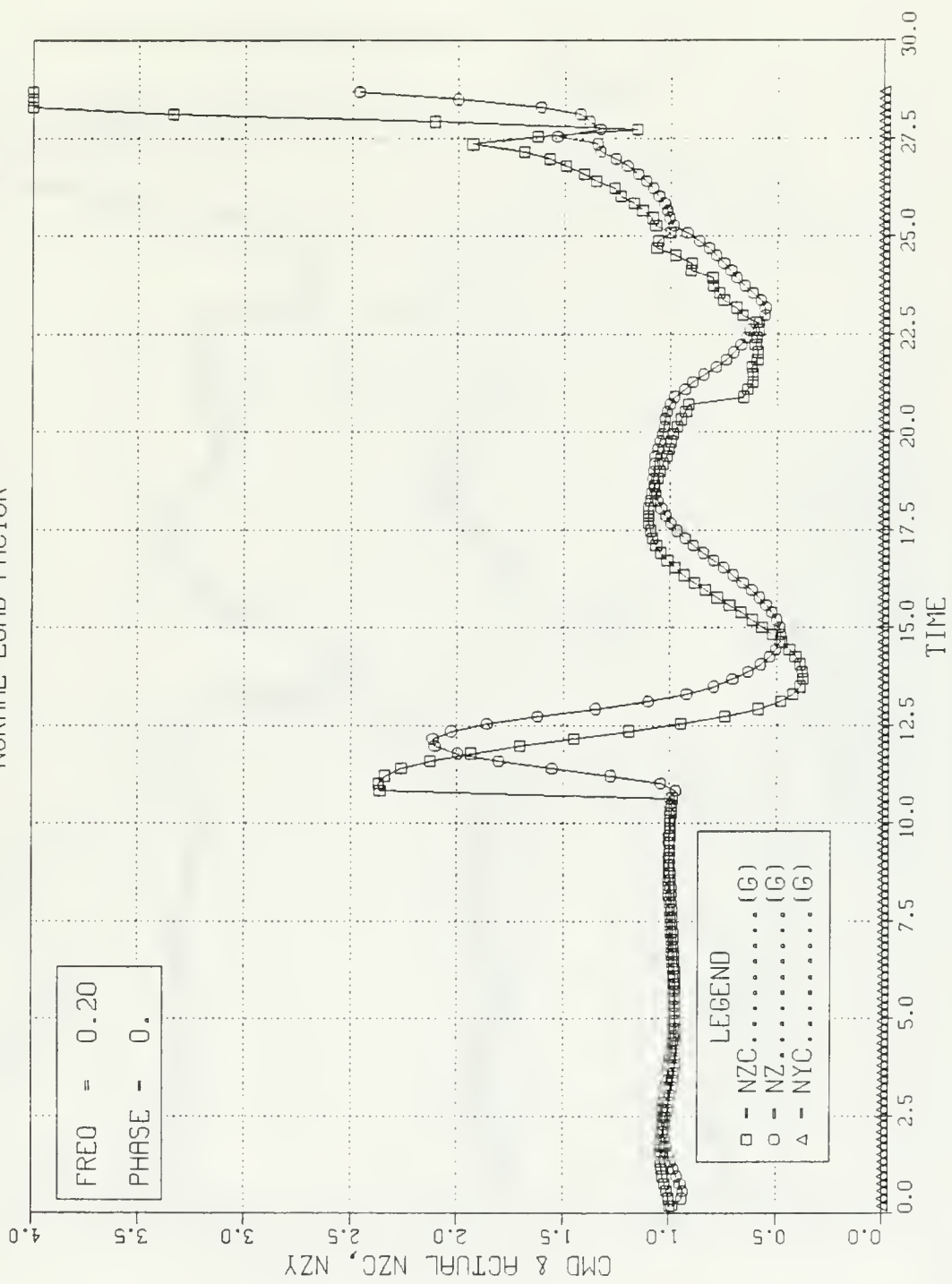


Figure A.58 Conf. II Mission Set - Load Factor.

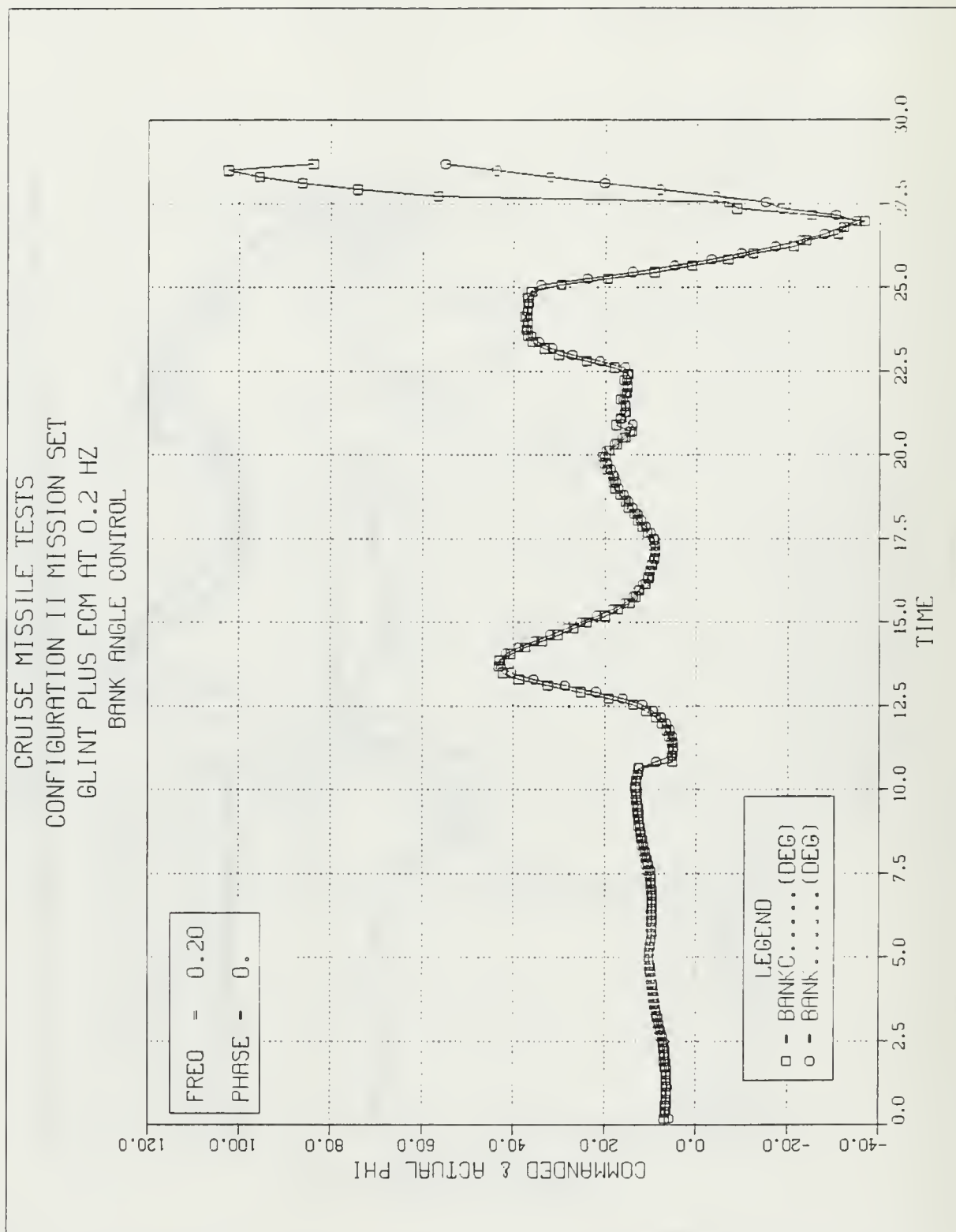


Figure A.59 Conf. II Mission Set - Bank.

CRUISE MISSILE TESTS  
 CONFIGURATION II MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 ROLL RATE CONTROL

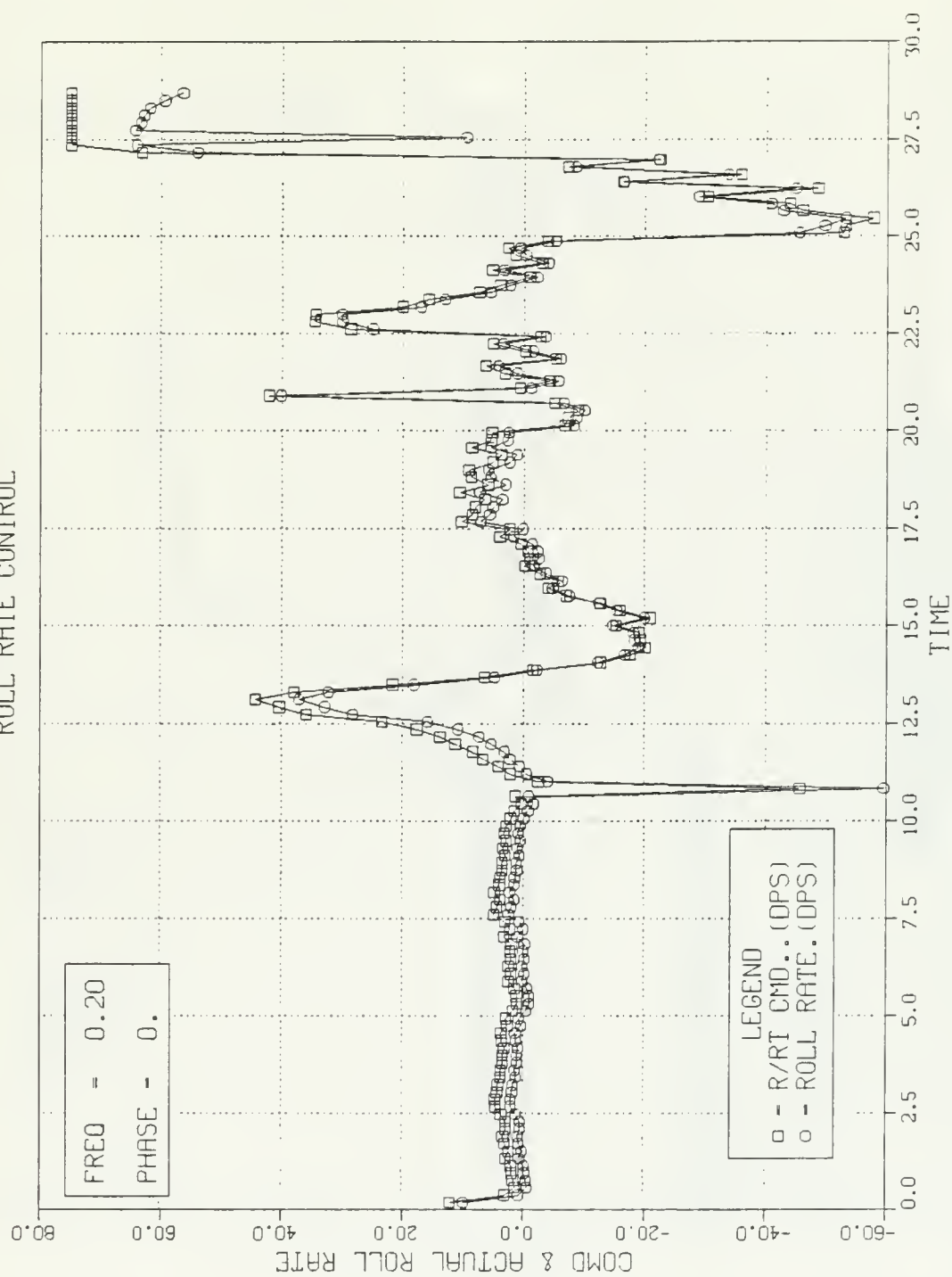


Figure A.60 Conf. II Mission Set - Roll Rate.

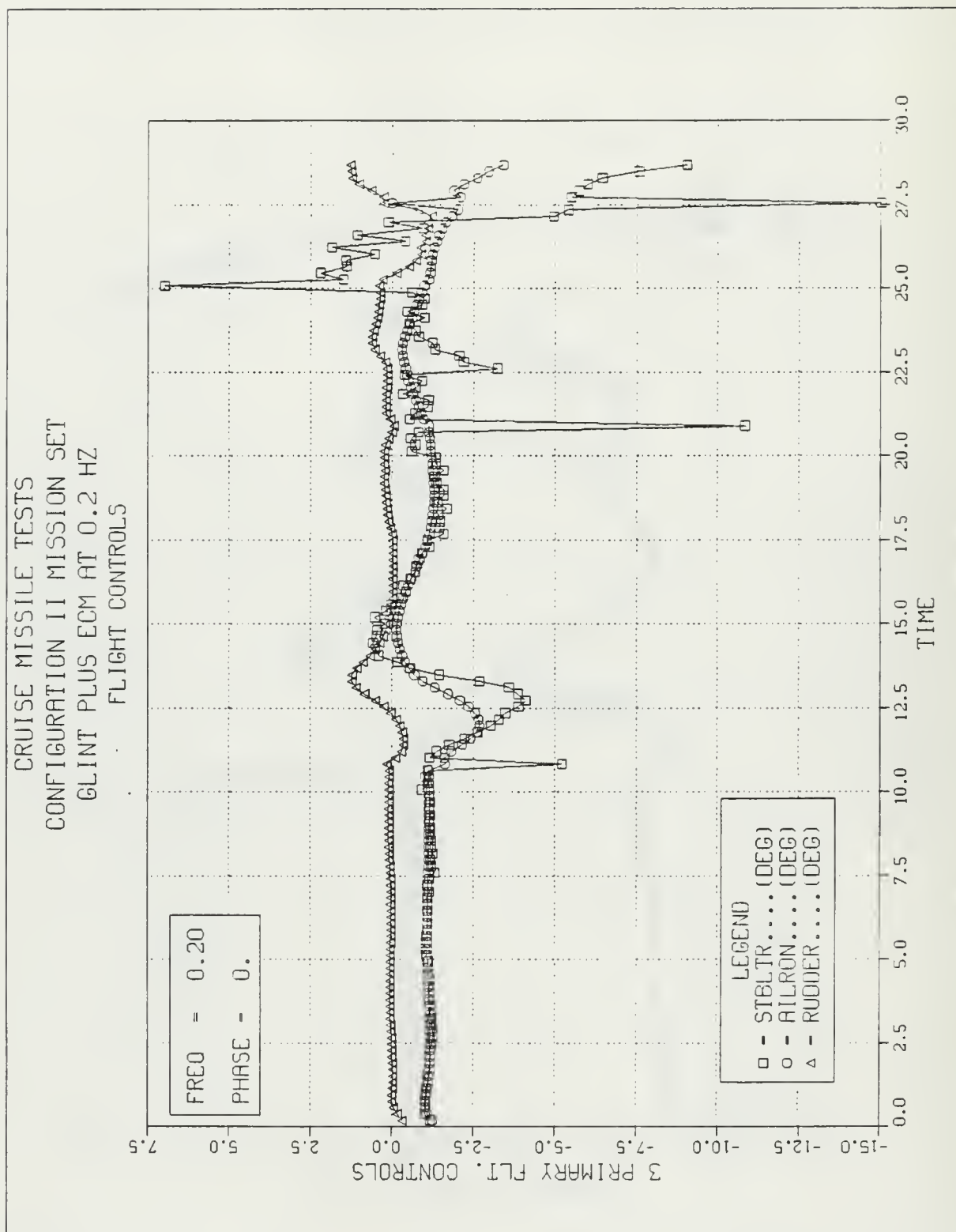


Figure A.61 Conf. II Mission Set - Controls.

CRUISE MISSILE TESTS  
 CONFIGURATION II MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 ALTITUDE CONTROL

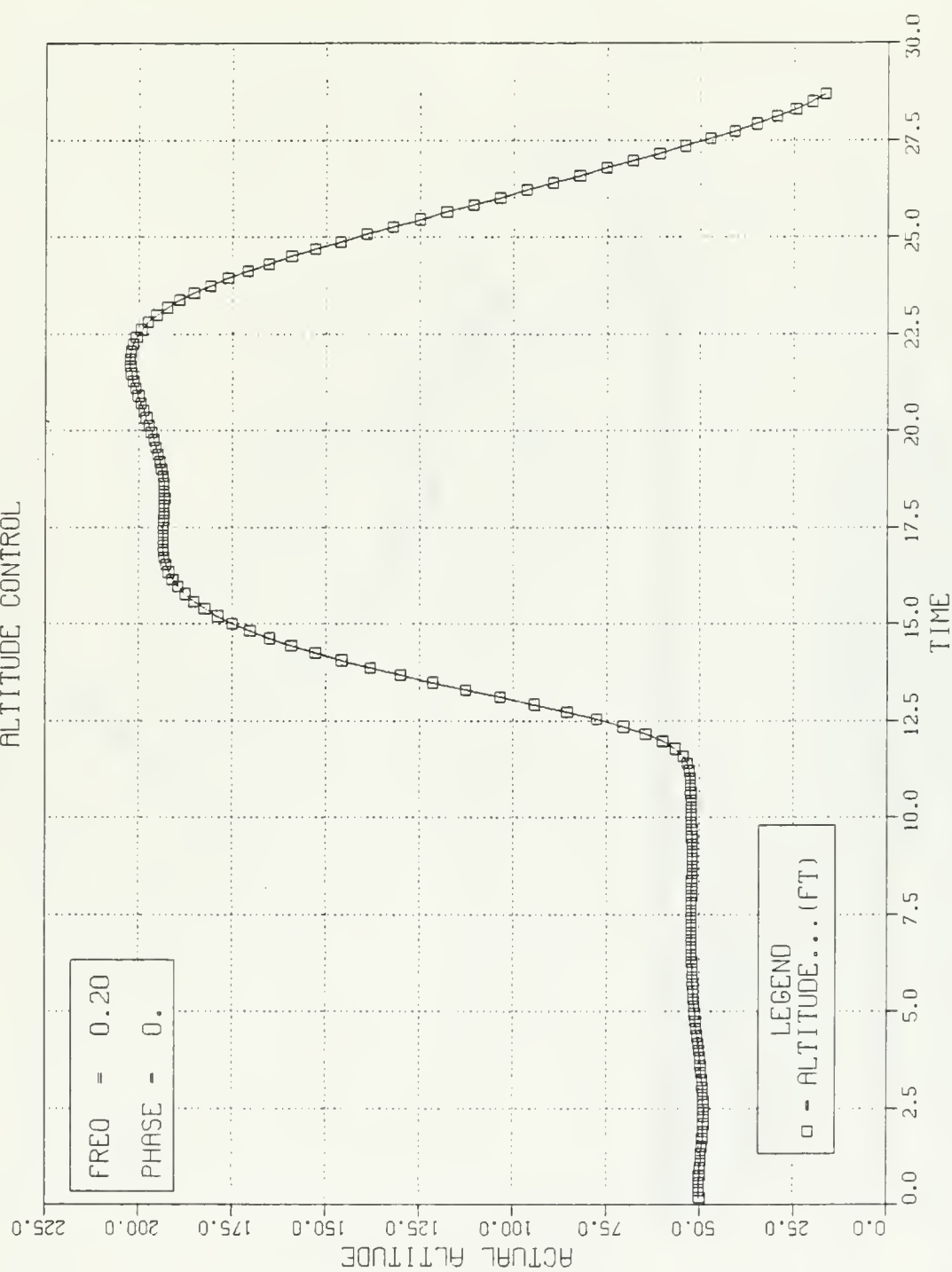
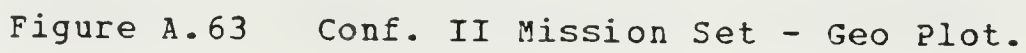


Figure A.62 Conf. II Mission Set - Altitude.



```
FREQ = 0.20
PHASE = 0.
```



CRUISE MISSILE TESTS  
 CONFIGURATION III MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 NORMAL LOAD FACTOR

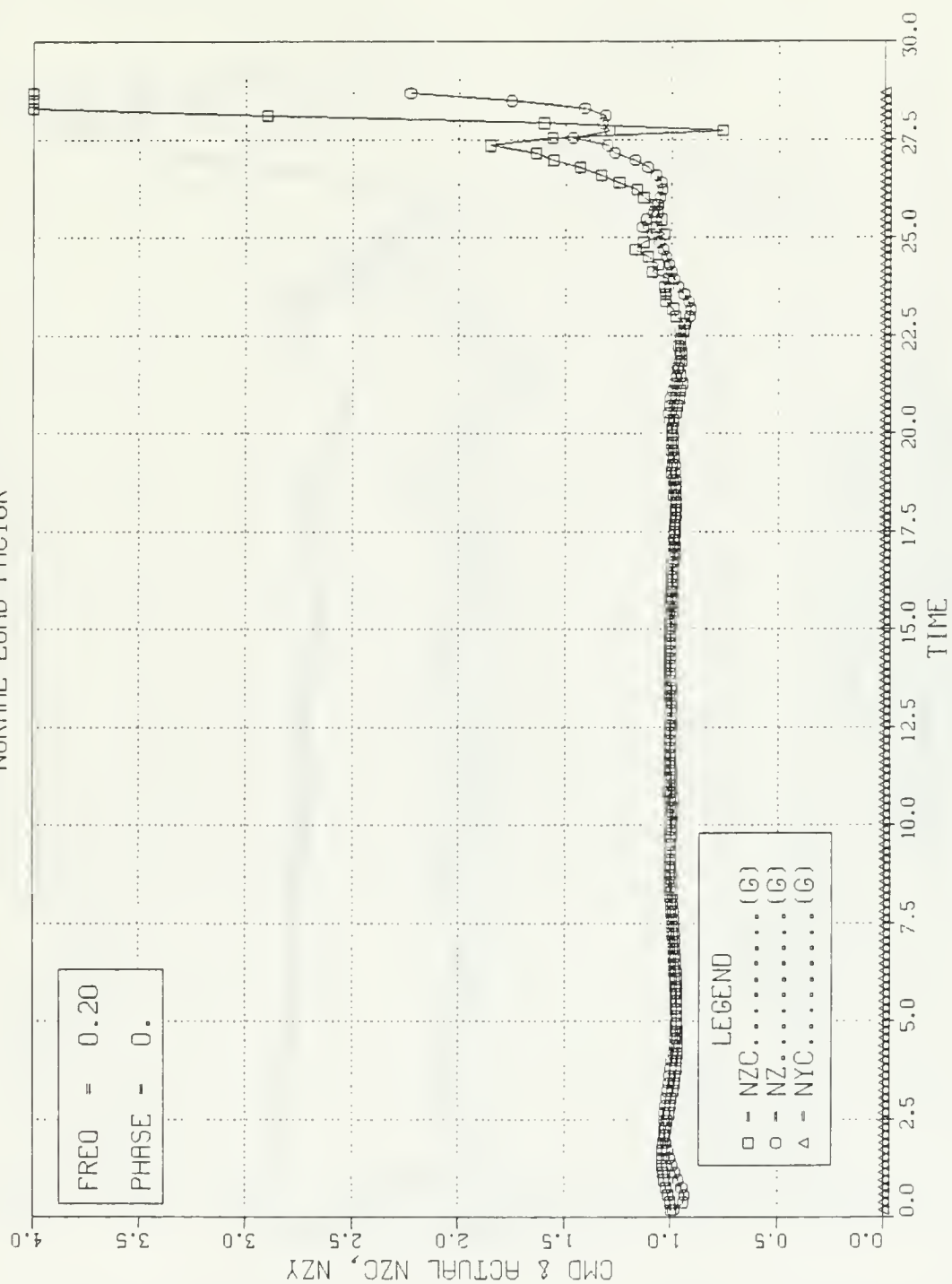


Figure A.64 Conf. III Mission Set - Load Factor.

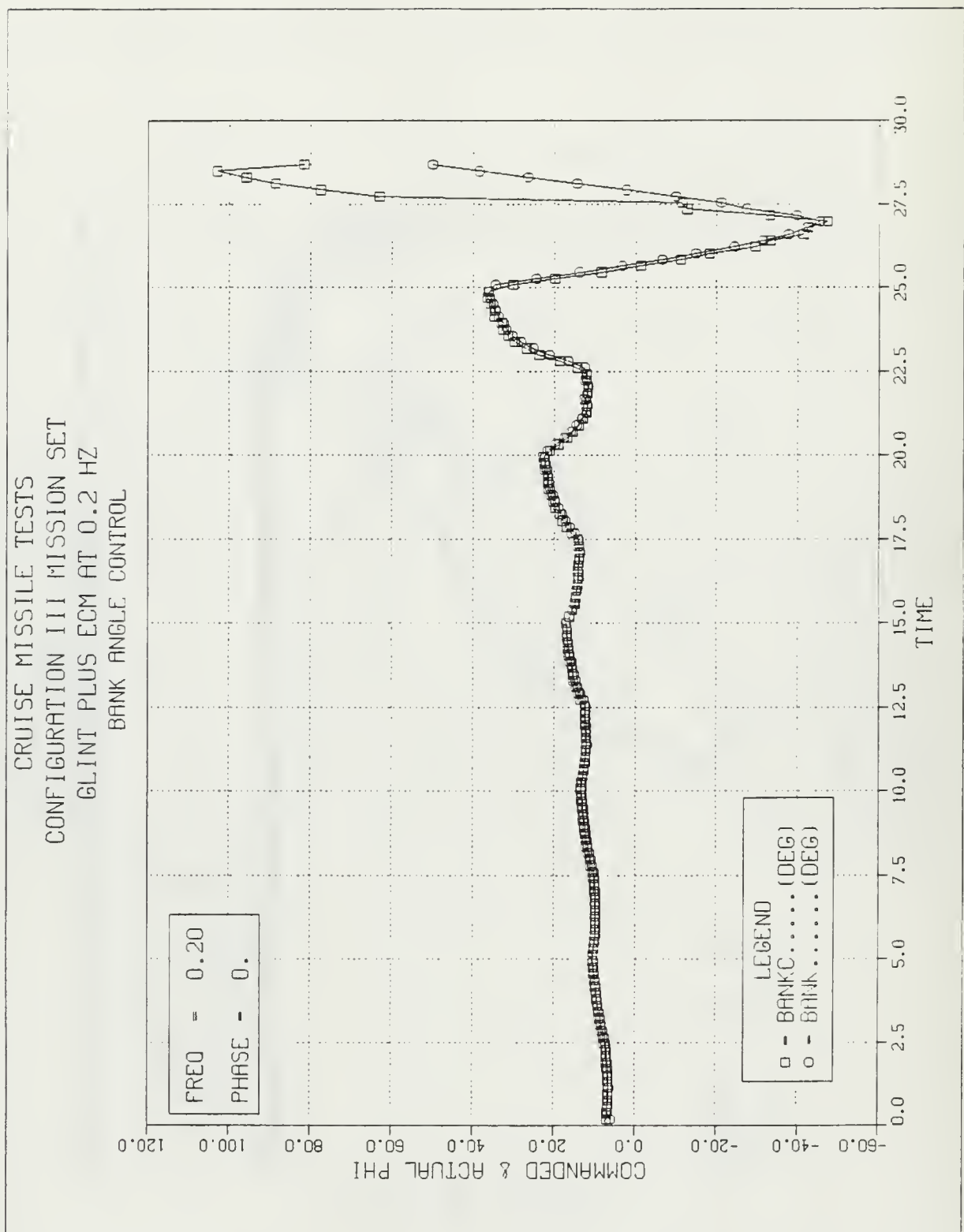


Figure A.65 Conf. III Mission Set - Bank.

CRUISE MISSILE TESTS  
 CONFIGURATION III MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 ROLL RATE CONTROL

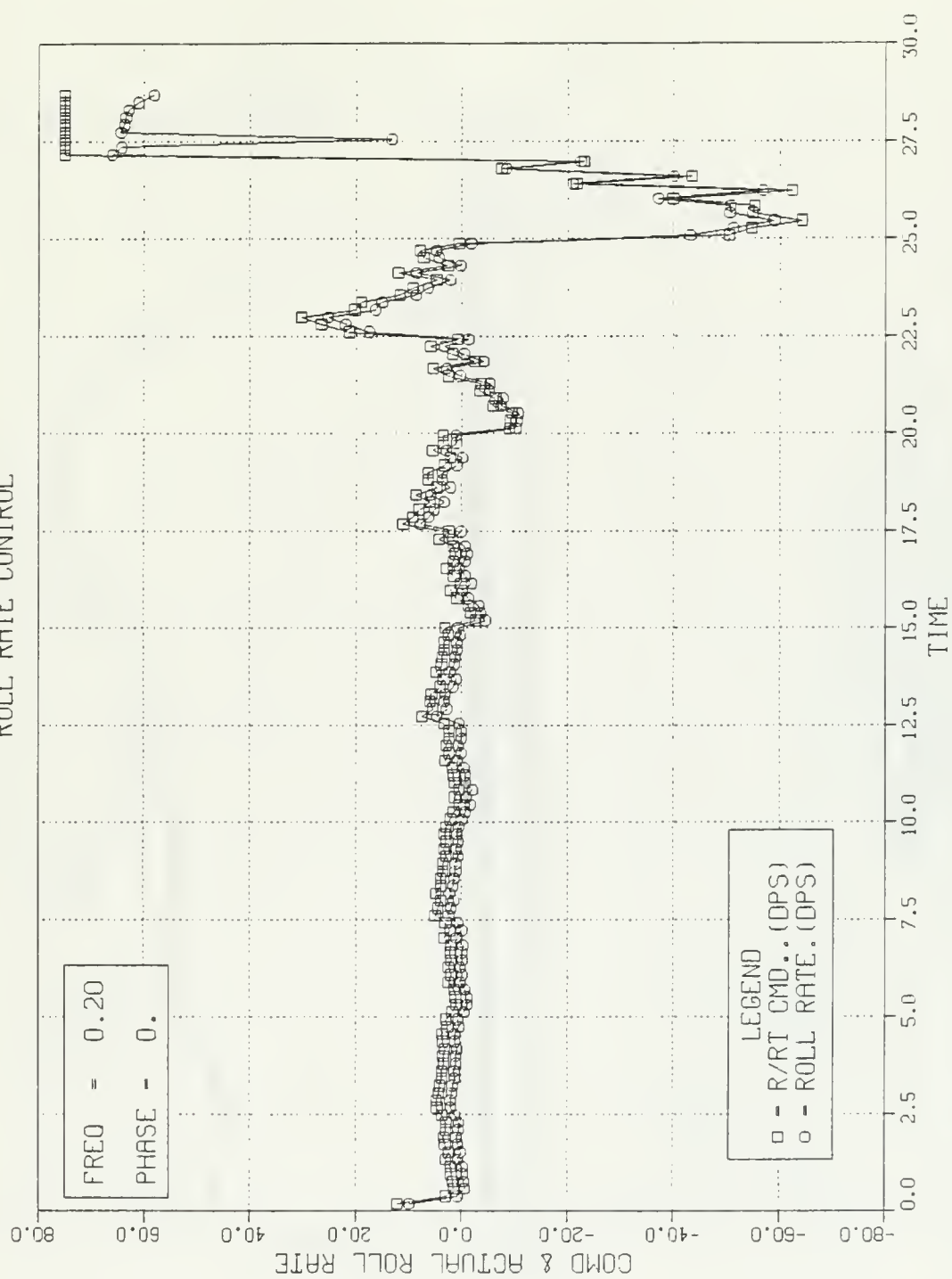


Figure A.66 Conf. III Mission Set - Roll Rate.

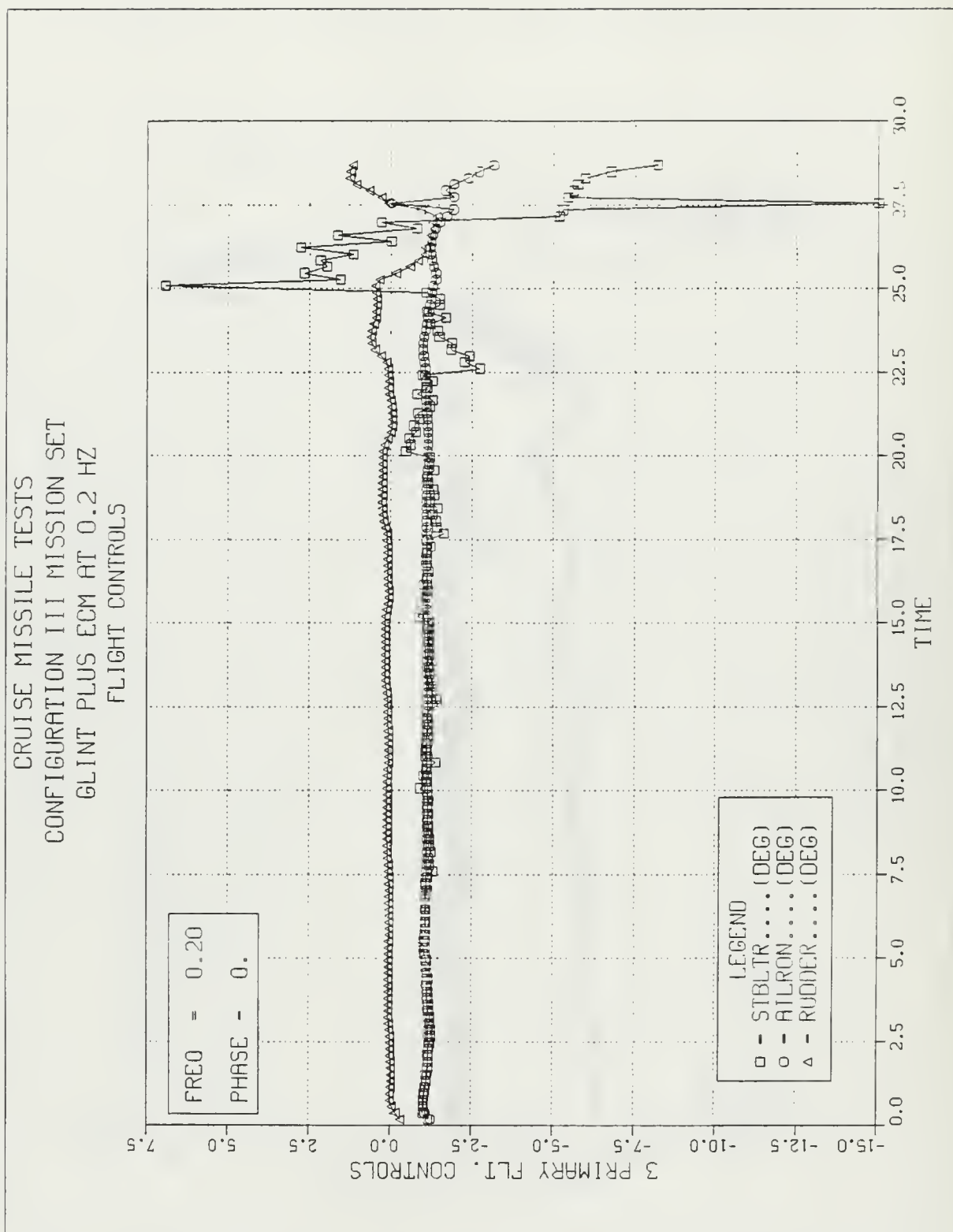


Figure A.67 Conf. III Mission Set - Controls.

CRUISE MISSILE TESTS  
 CONFIGURATION III MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 ALTITUDE CONTROL

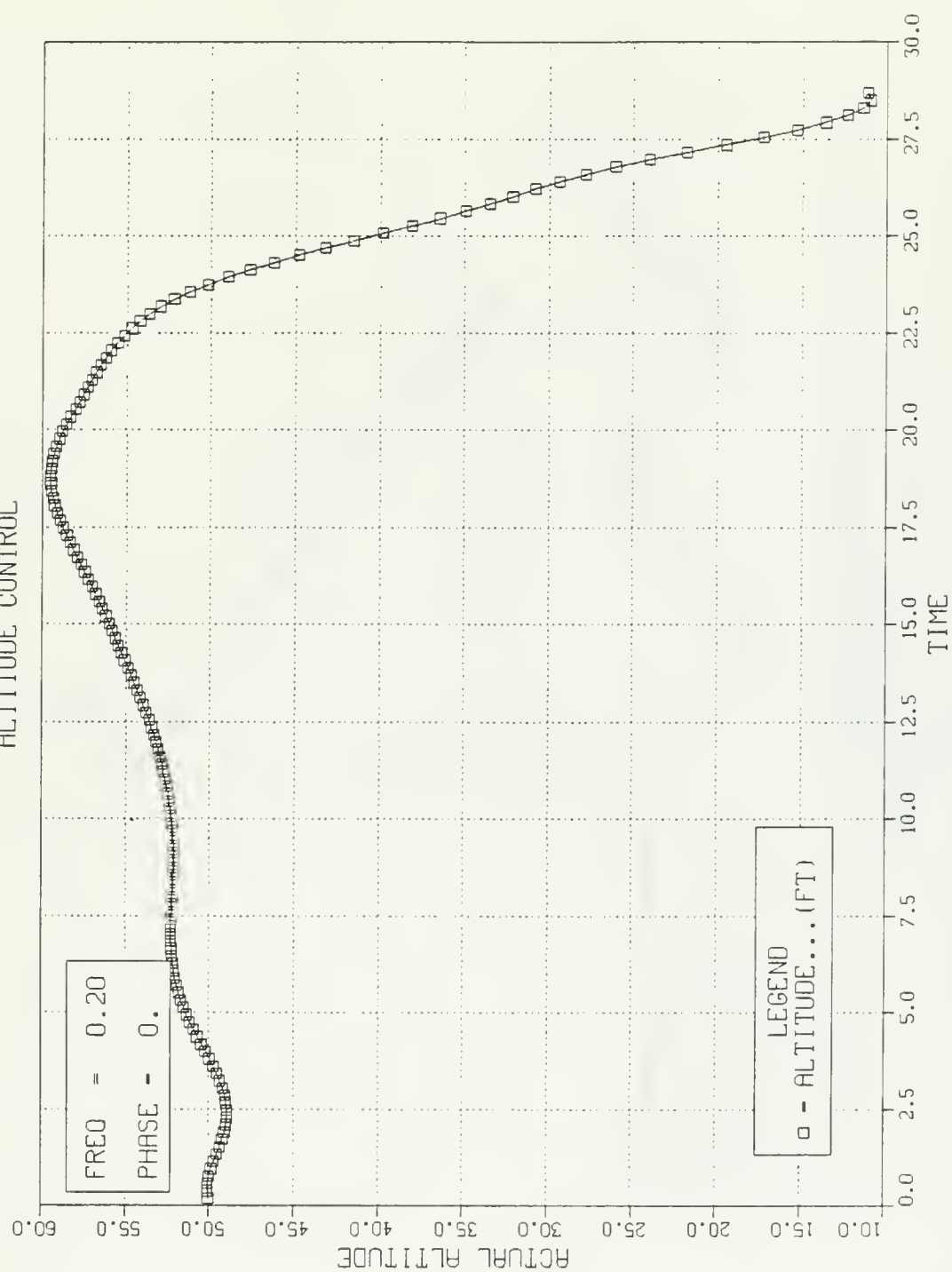


Figure A.68 Conf. III Mission Set - Altitude.



CRUISE MISSILE TESTS  
 CONFIGURATION III MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 GEOGRAPHICAL TRACKS

FREQ	=	0.20
PHASE	=	0.

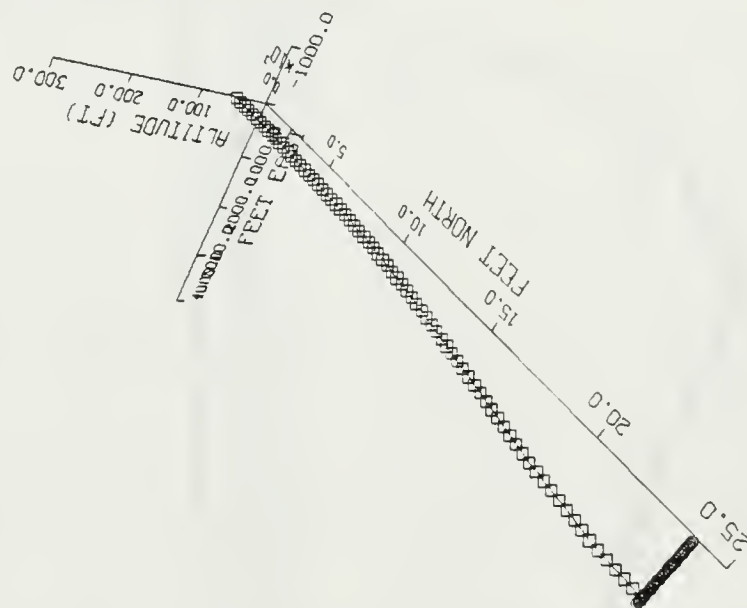


Figure A.69 Conf. III Mission Set - Geo Plot.

CRUISE MISSILE TESTS  
 CONFIGURATION IV MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 NORMAL LOAD FACTOR

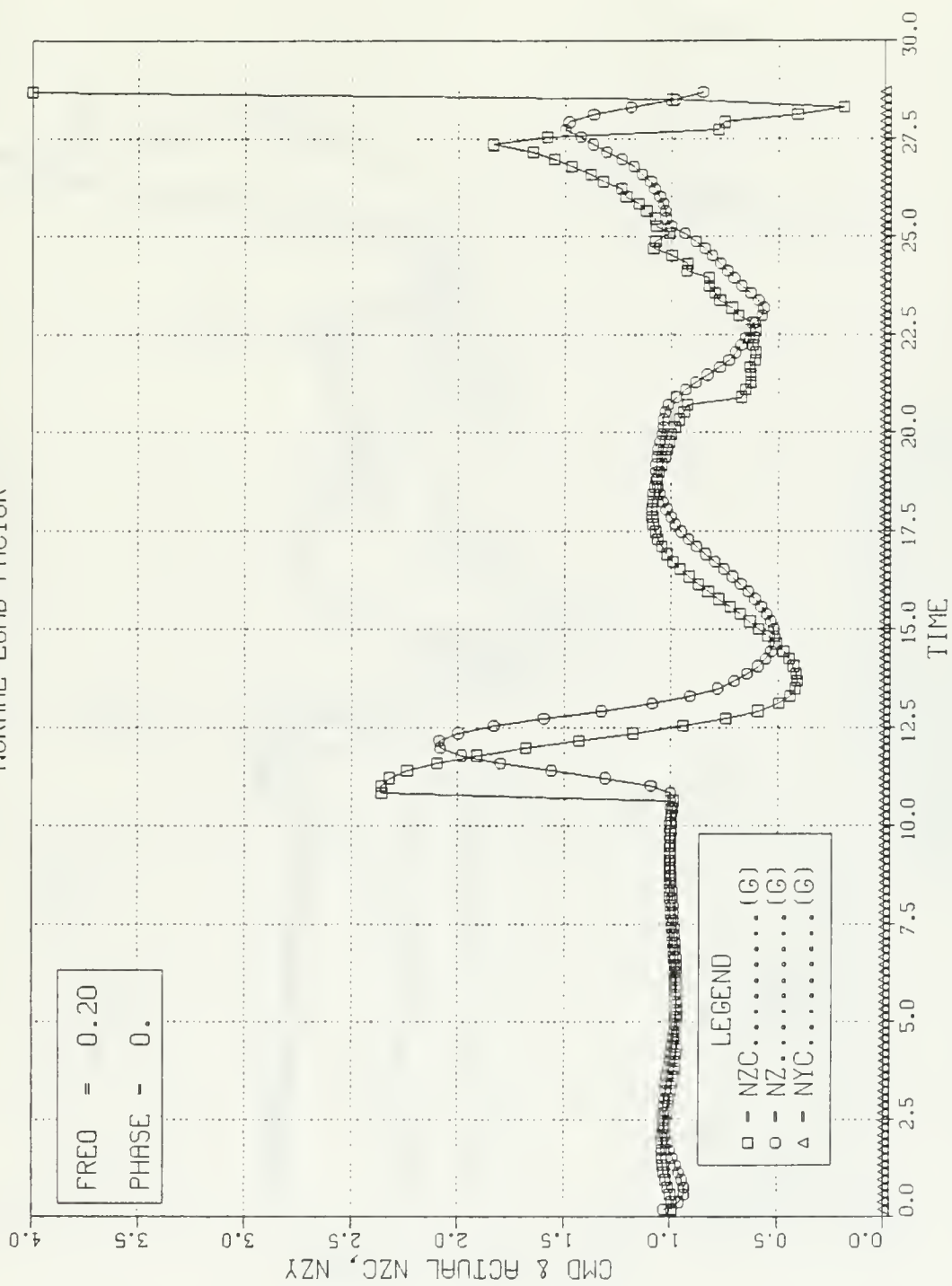


Figure A.70 Conf. IV Mission Set - Load Factor.

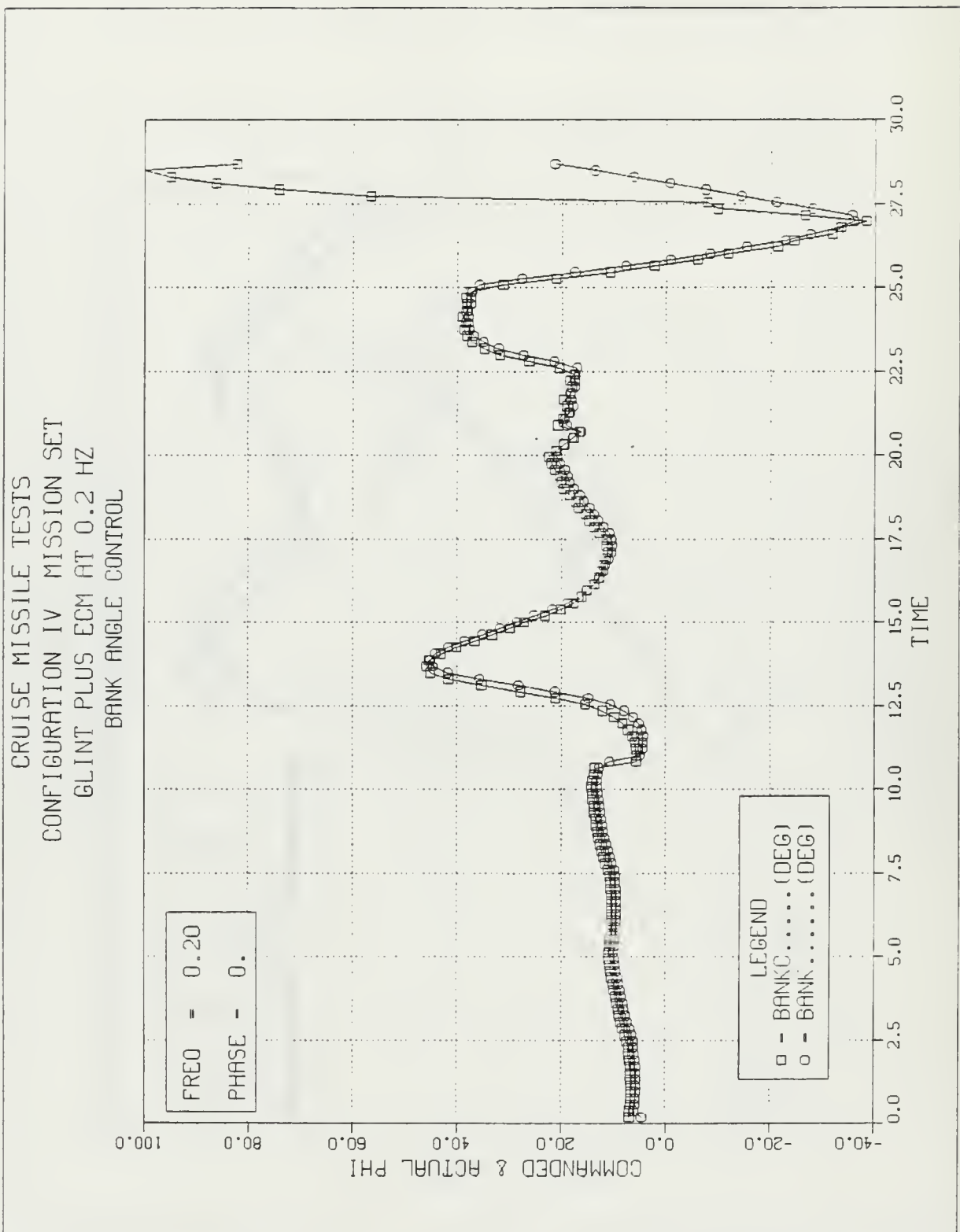


Figure A.71 Conf. IV Mission Set - Bank.

CRUISE MISSILE TESTS  
 CONFIGURATION IV MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 ROLL RATE CONTROL

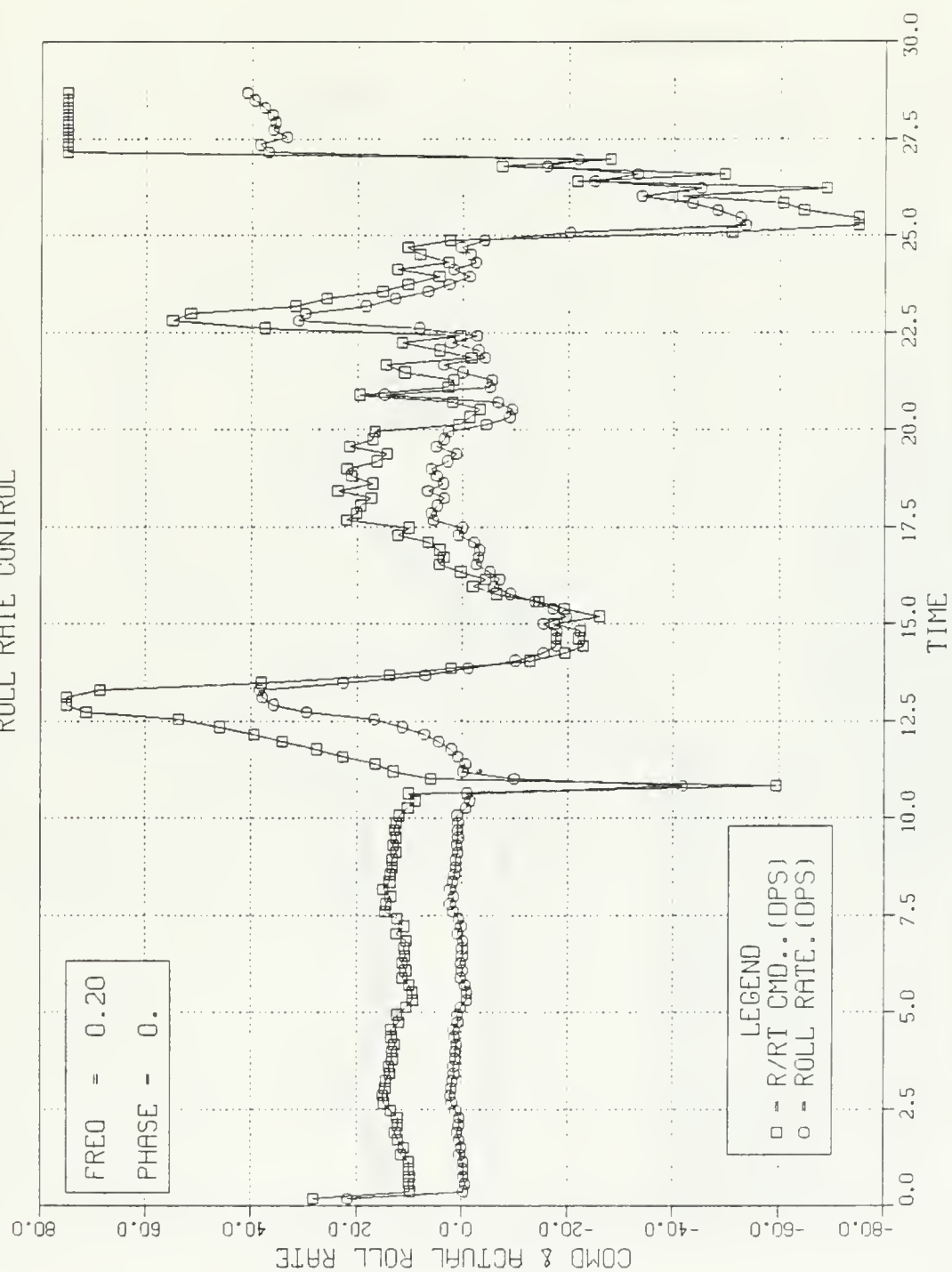


Figure A.72 Conf. IV Mission Set - Roll Rate.

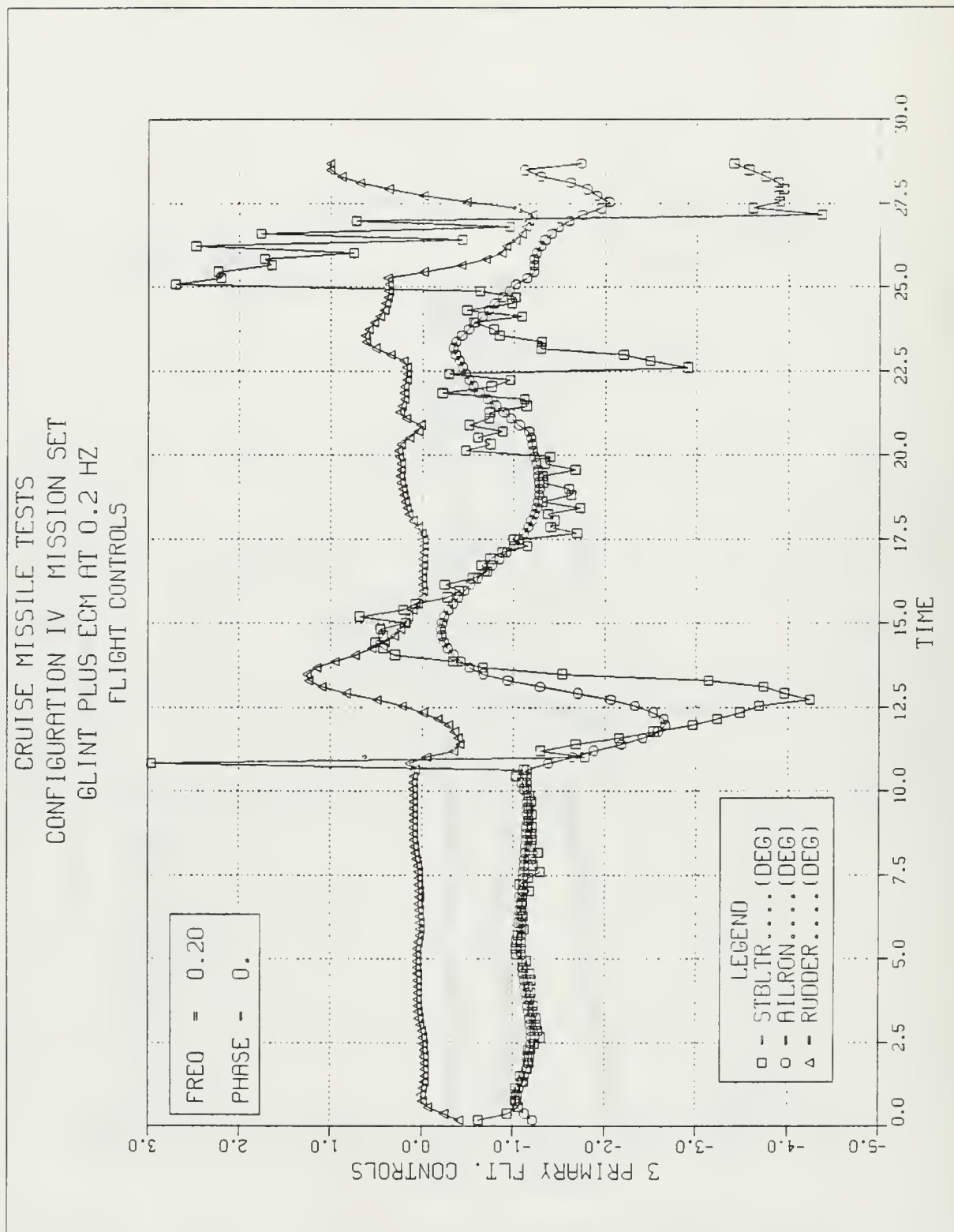


Figure A.73 Conf. IV Mission Set - Controls.

CRUISE MISSILE TESTS  
 CONFIGURATION IV MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 ALTITUDE CONTROL

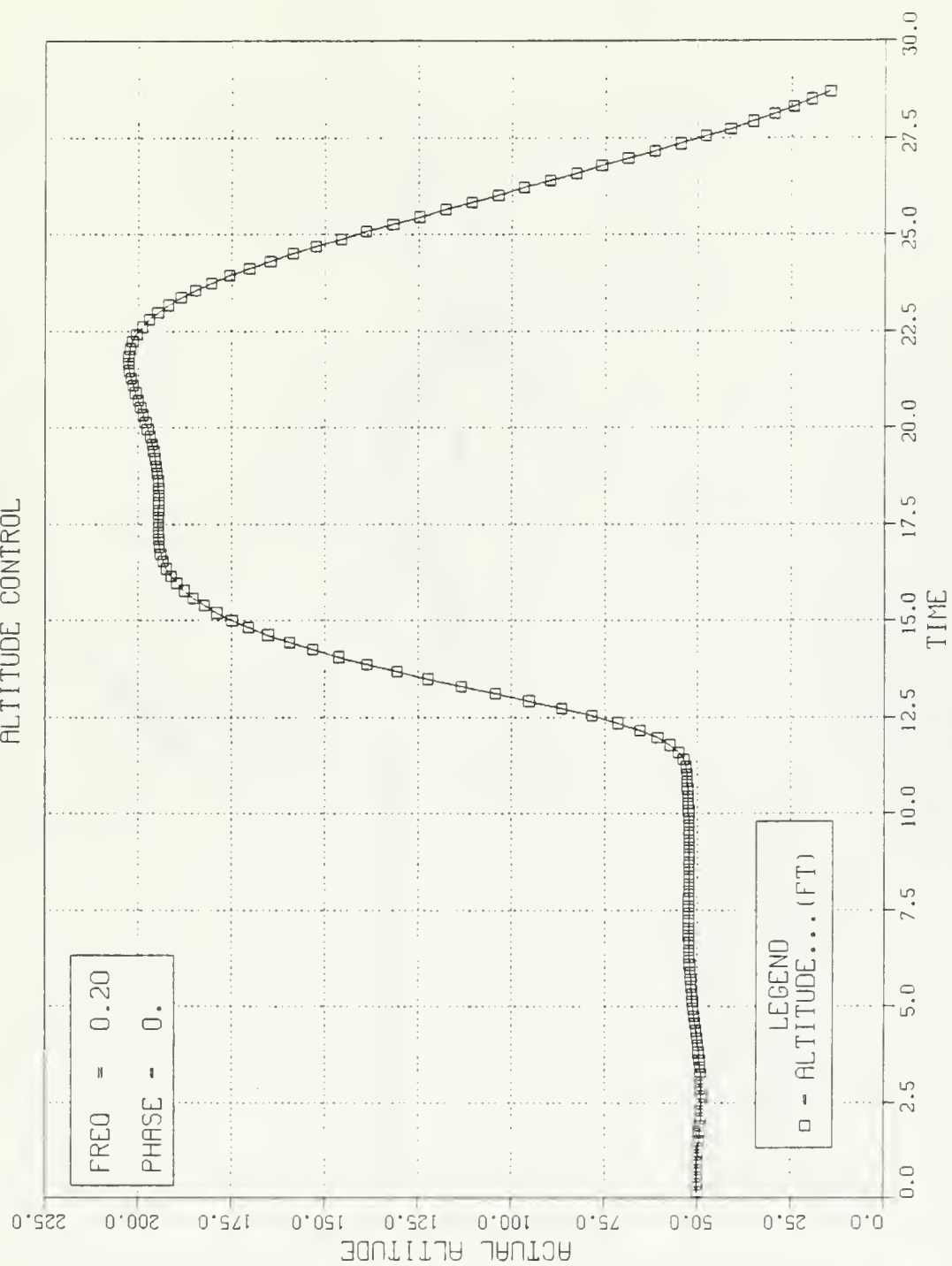


Figure A.74 Conf. IV Mission Set - Altitude.



CRUISE MISSILE TESTS  
 CONFIGURATION IV MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 GEOGRAPHICAL TRACKS

FREQ	=	0.20
PHASE	=	0.

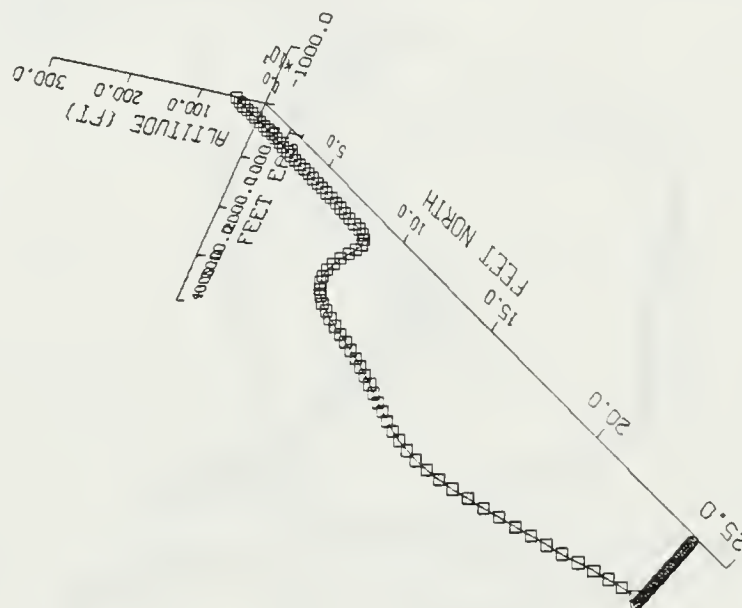


Figure A.75 Conf. IV Mission Set - Geo Plot.

CRUISE MISSILE TESTS  
SEA-SKIMMER (STT) - NO GLINT  
HI-FREQUENCY SCAN 0.0-21. HZ  
NORMAL LOAD FACTOR

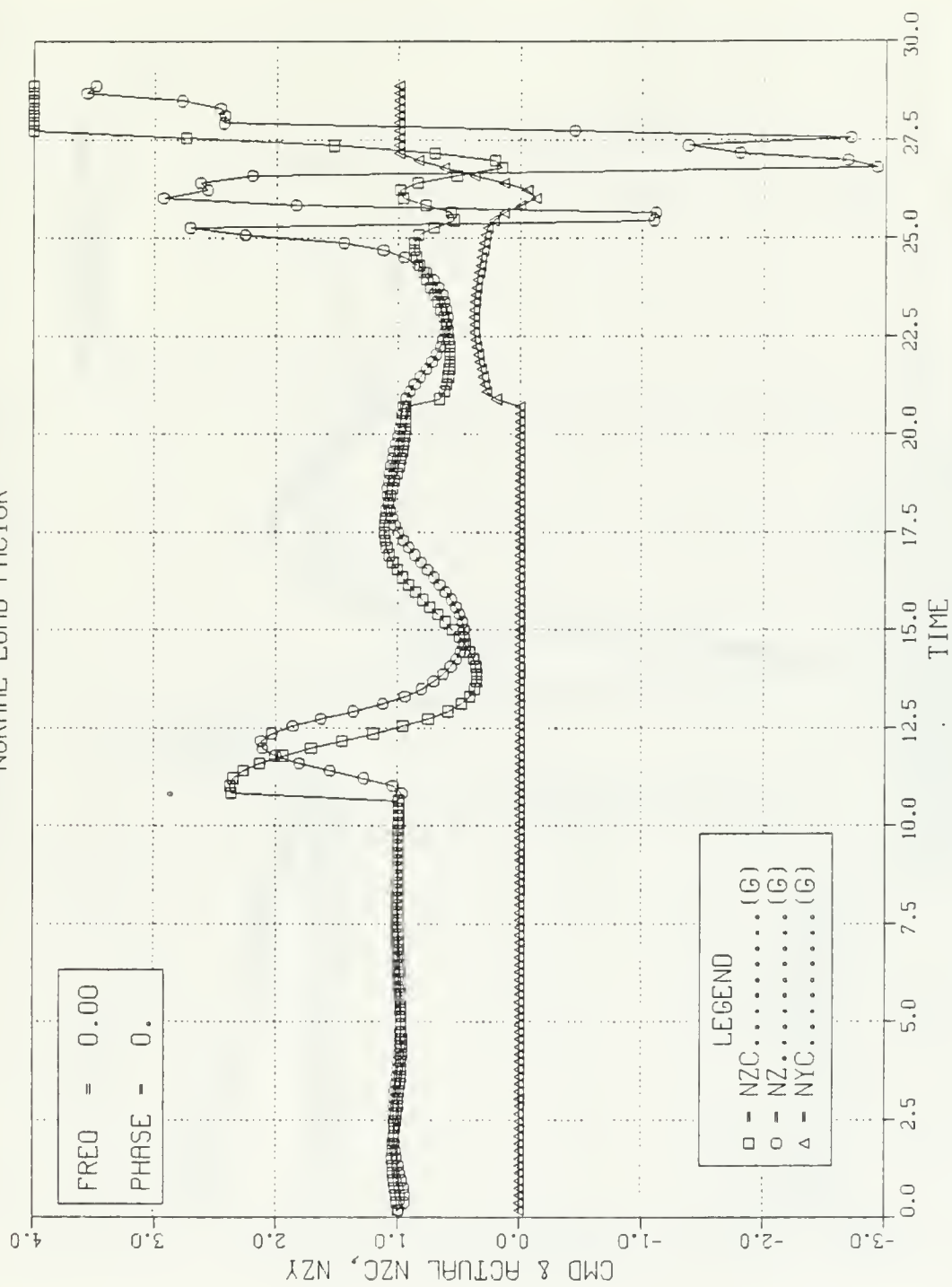


Figure A.76 Conf. V Mission Set - Load Factor.

CRUISE MISSILE TESTS  
 SEA-SKIMMER (STT) - NO GLINT  
 HI-FREQUENCY SCAN 0.0-21. HZ  
 . BANK ANGLE CONTROL

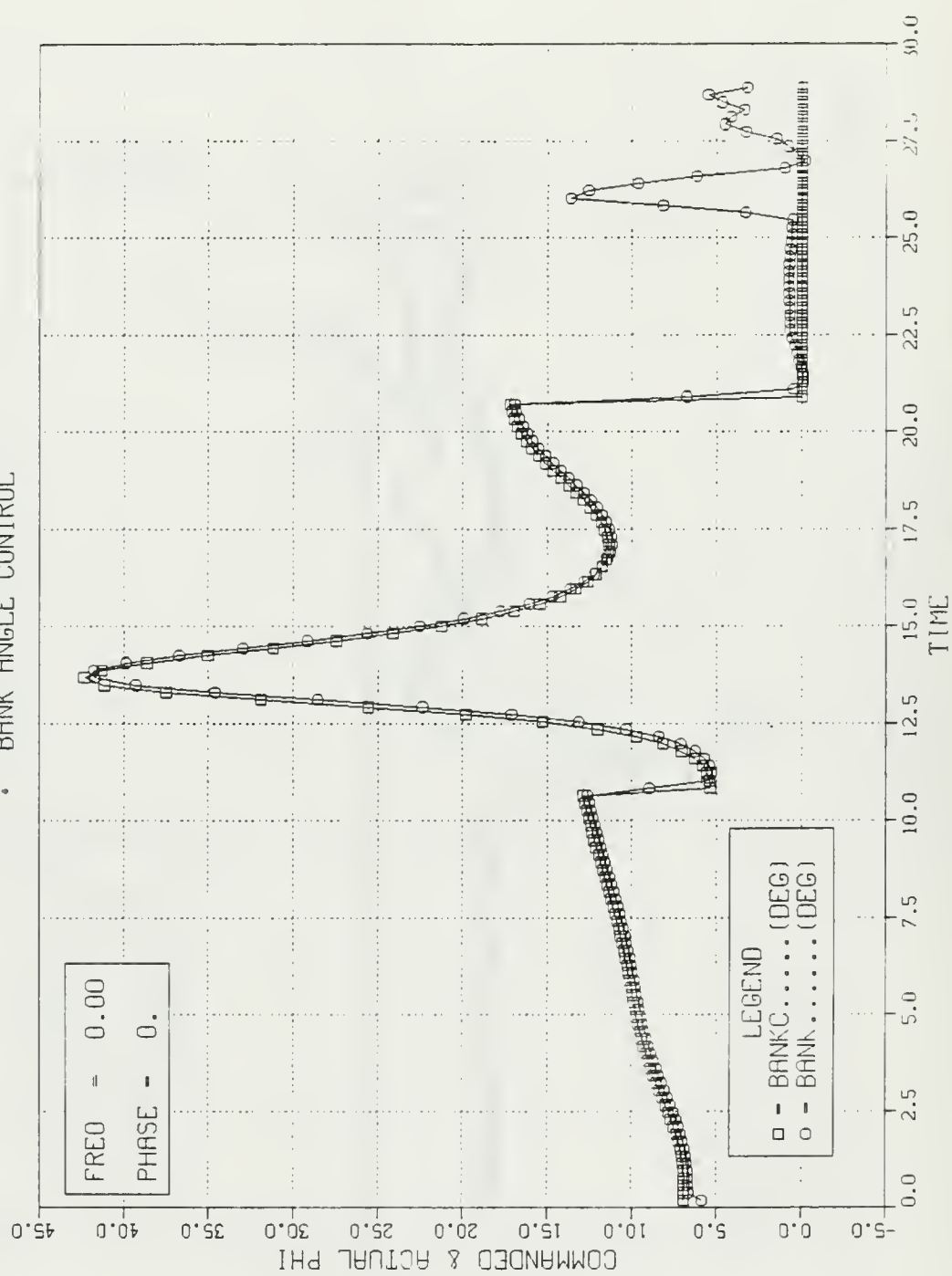


Figure A.77 Conf. V Mission Set - Bank.

CRUISE MISSILE TESTS  
SEA-SKIMMER (STT) - NO GLINT  
HI-FREQUENCY SCAN 0.0-21. HZ  
ROLL RATE CONTROL

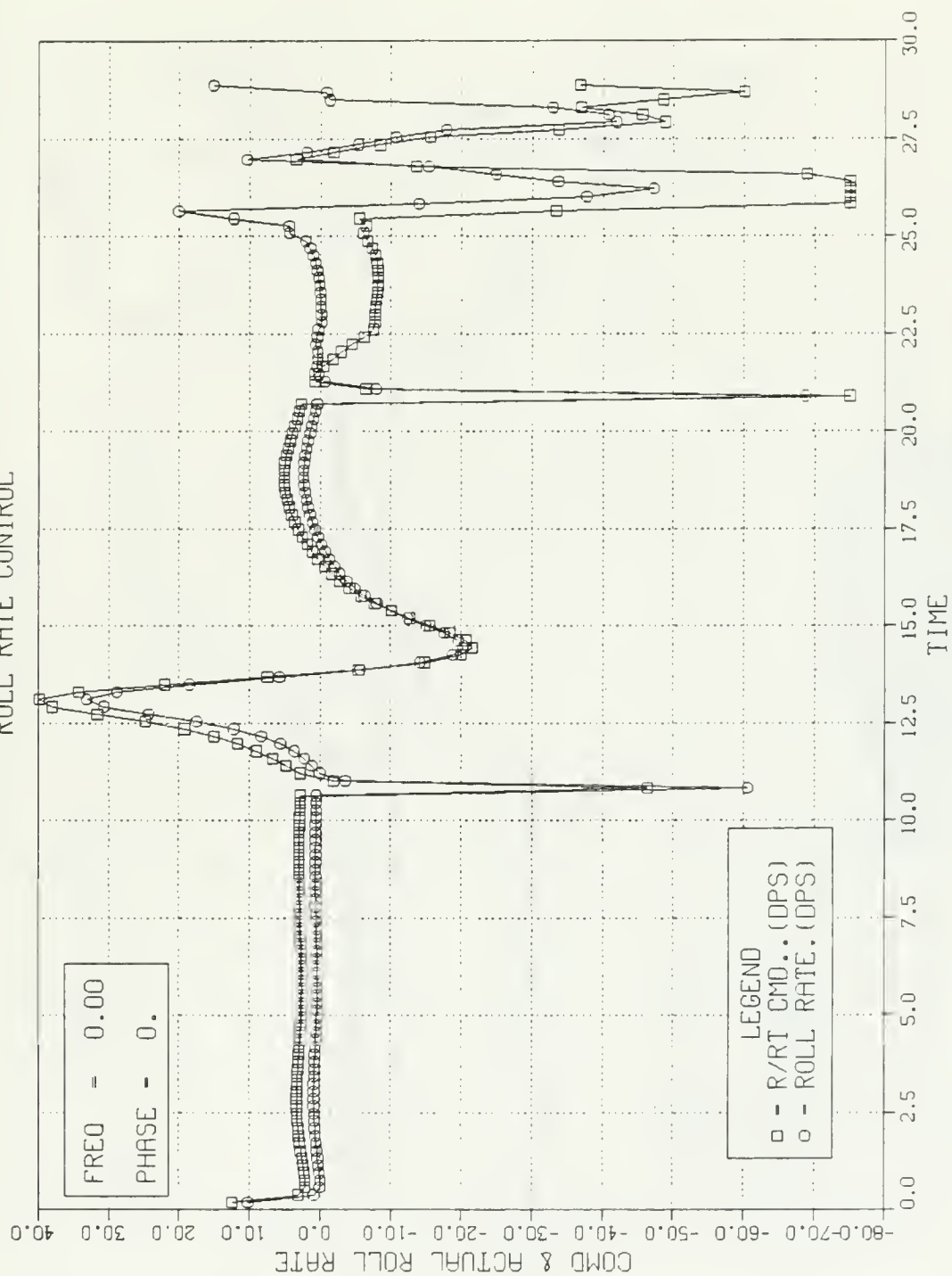


Figure A.78 Conf. V Mission Set - Roll Rate.

CRUISE MISSILE TESTS  
SEA-SKIMMER (STT) - NO GLINT  
HI-FREQUENCY SCAN 0.0-21. HZ  
FLIGHT CONTROLS

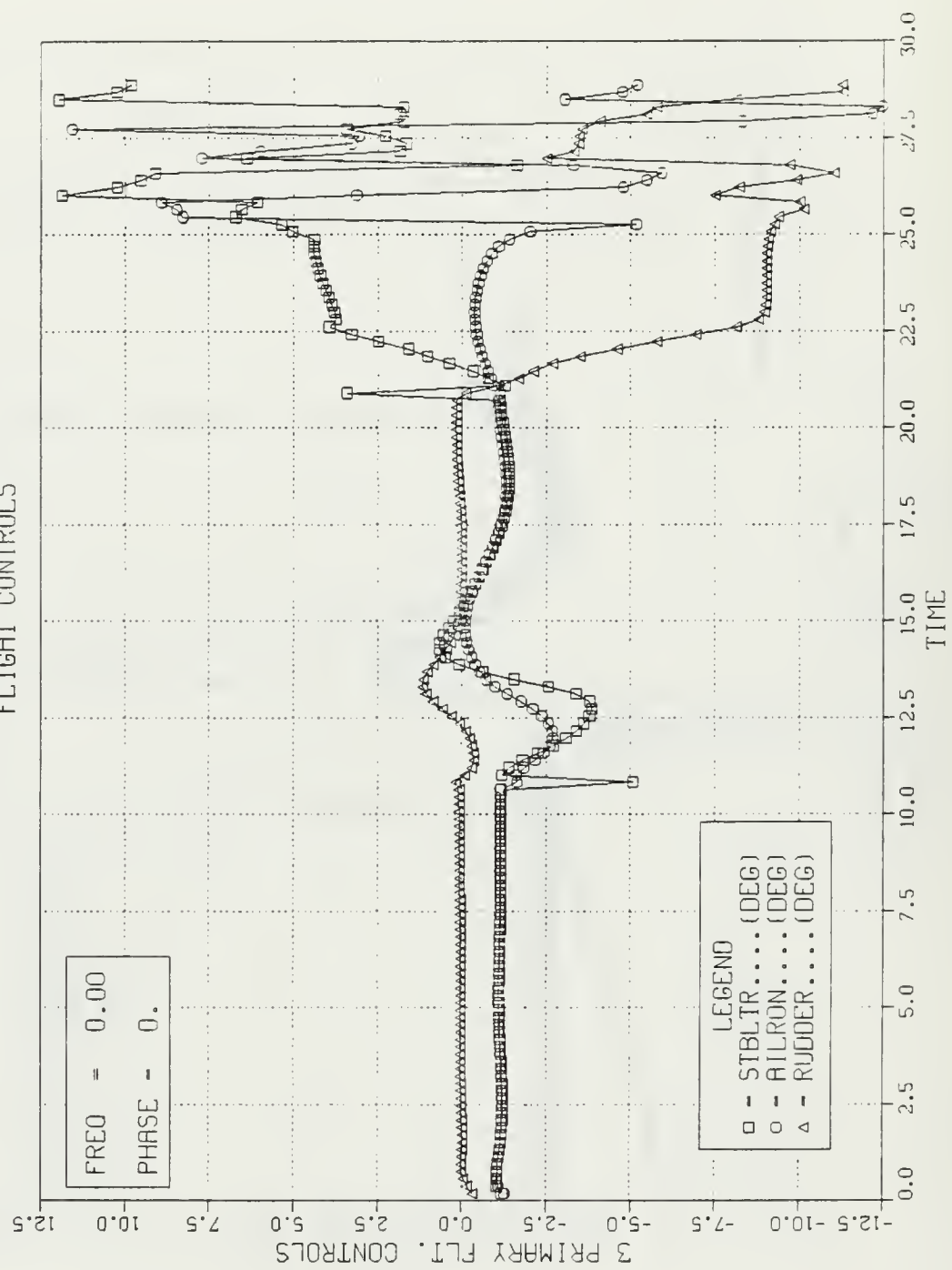


Figure A.79 Conf. V Mission Set - Controls.

CRUISE MISSILE TESTS  
SEA-SKIMMER (STT) - NO GLINT  
HI-FREQUENCY SCAN 0.0-21. HZ  
ALTITUDE CONTROL

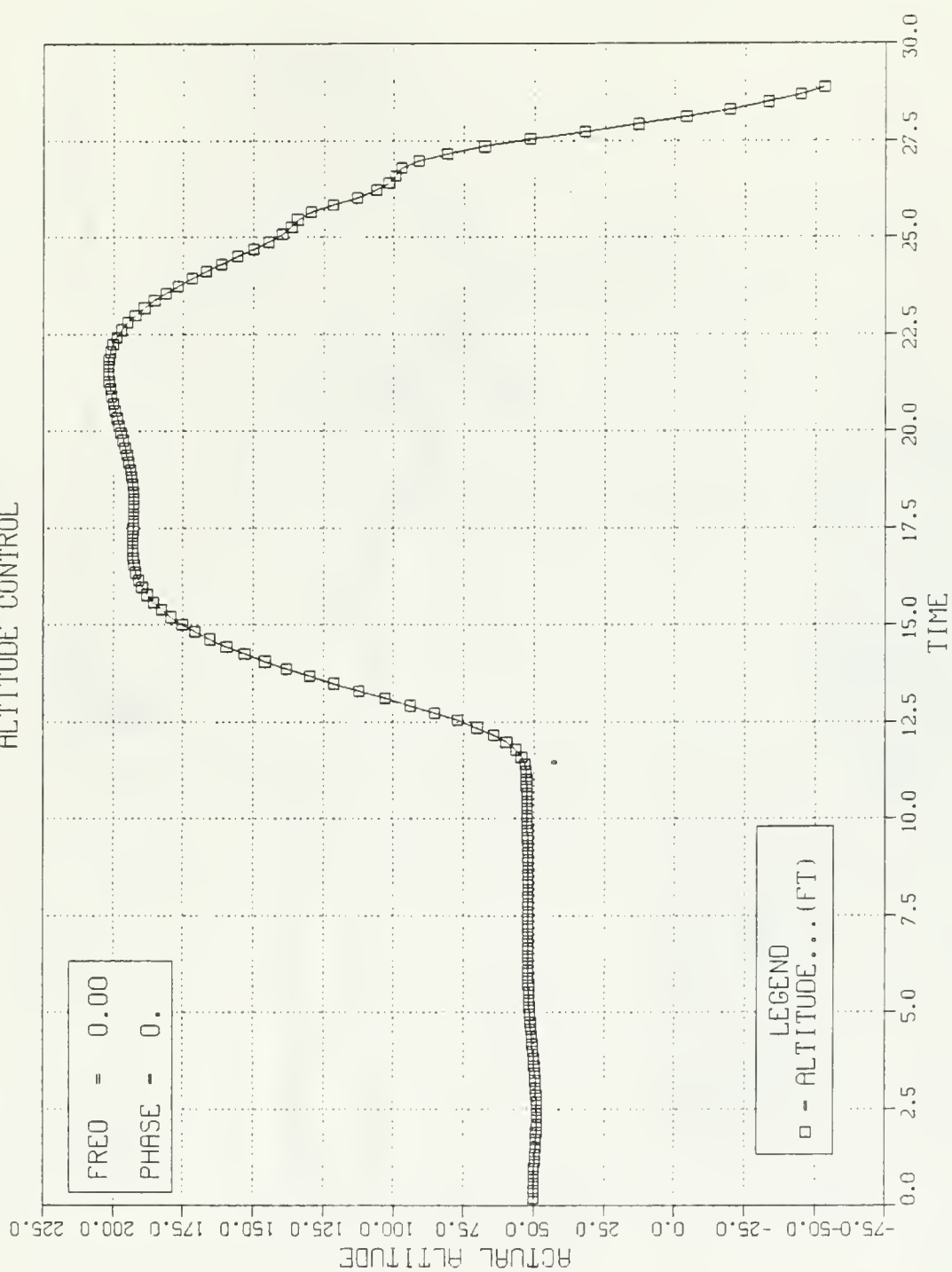


Figure A.80 Conf. V Mission Set - Altitude.



CRUISE MISSILE TESTS  
 SEA-SKIMMER (STT) - NO GLINT  
 HI-FREQUENCY SCAN 0.0-21. HZ  
 GEOGRAPHICAL TRACKS

FREQ	=	0.00
PHASE	=	0.

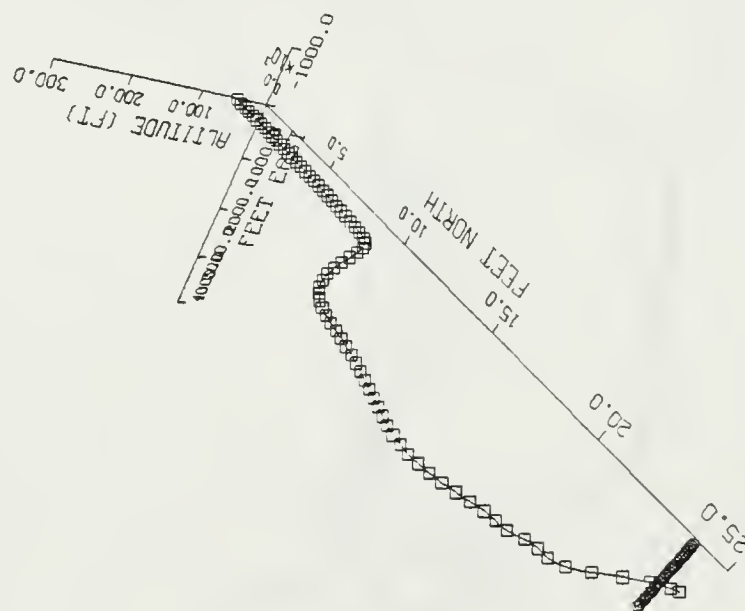


Figure A.81 Conf. V Mission Set - Geo Plot.

CRUISE MISSILE TESTS  
 BALLISTIC (BTT) GUIDANCE  
 NO GLINT OR ECM  
 NORMAL LOAD FACTOR

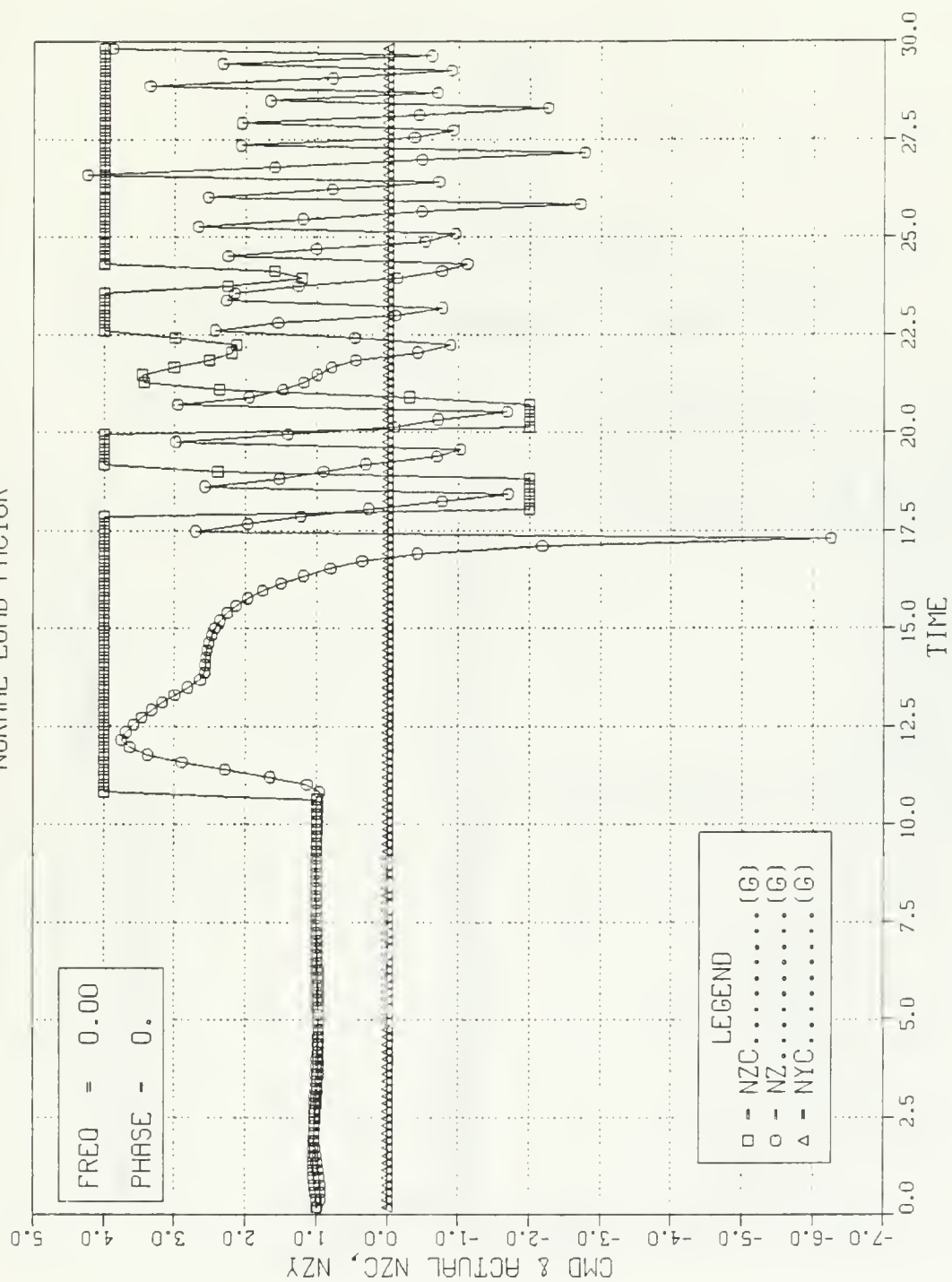


Figure A.82 Conf. VI Mission Set - Load Factor.

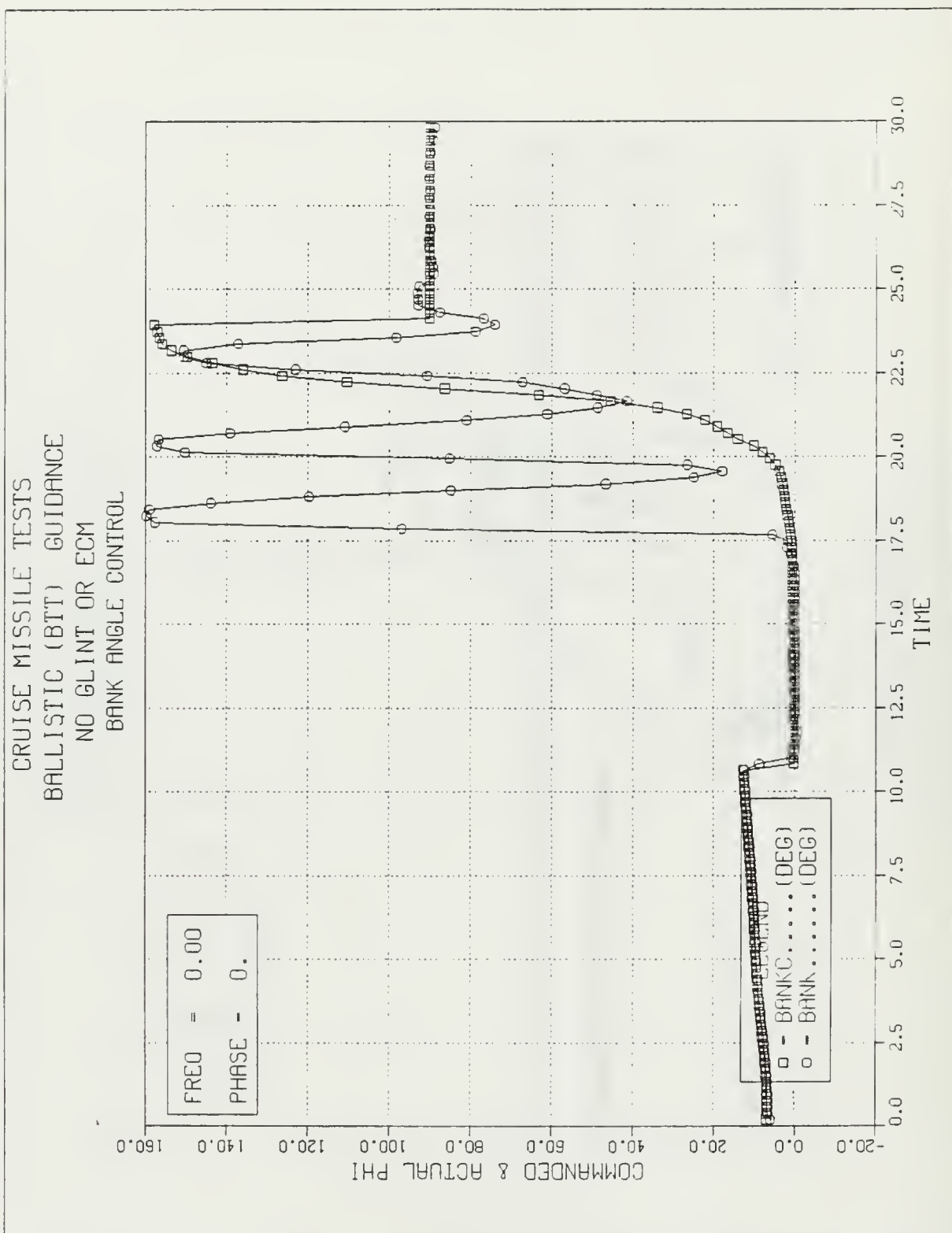


Figure A.83 Conf. VI Mission Set - Bank.

CRUISE MISSILE TESTS  
 BALLISTIC (BTT) GUIDANCE  
 NO GLINT OR ECM  
 ROLL RATE CONTROL

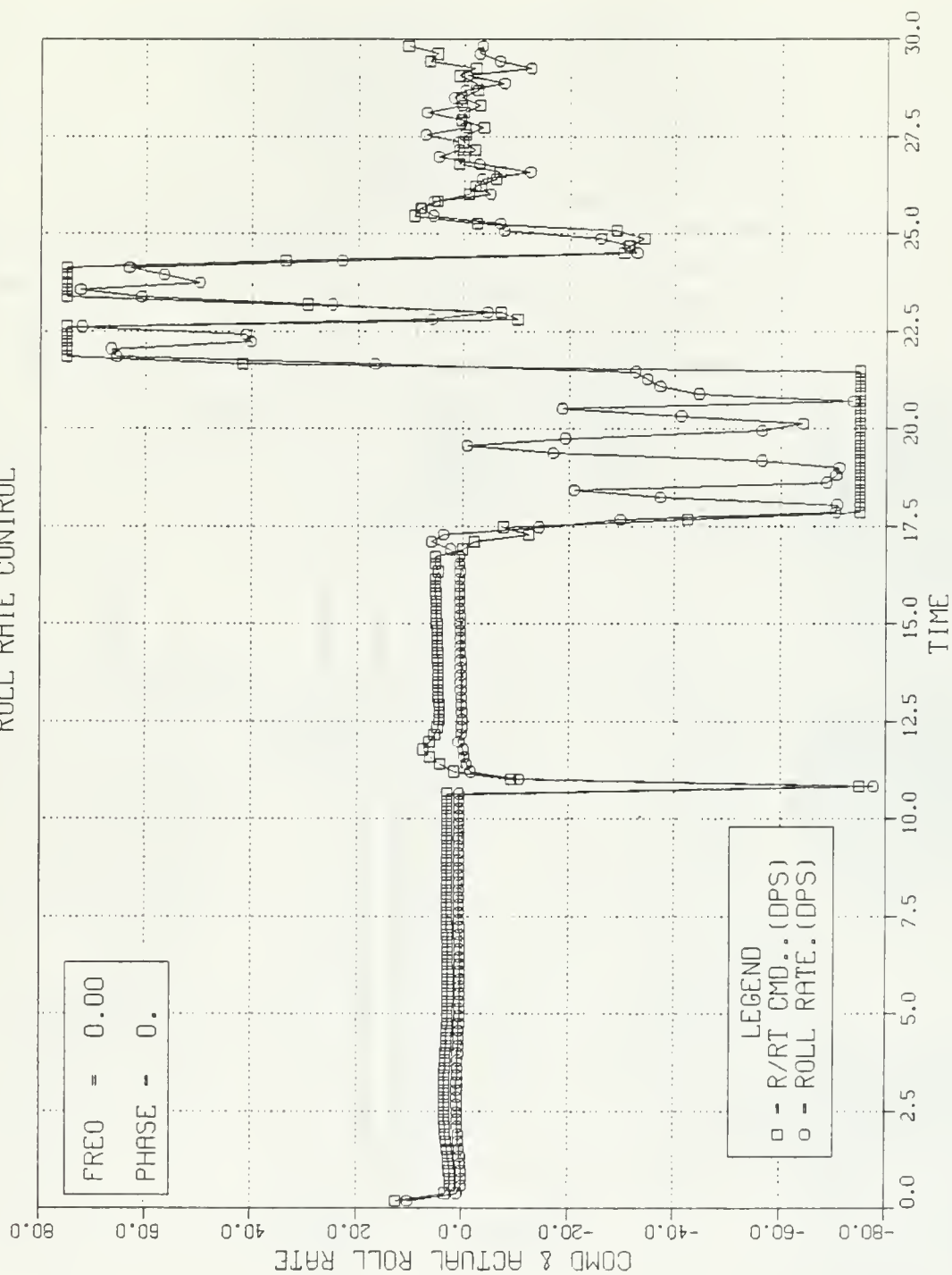


Figure A.84 Conf. VI Mission Set - Roll Rate.

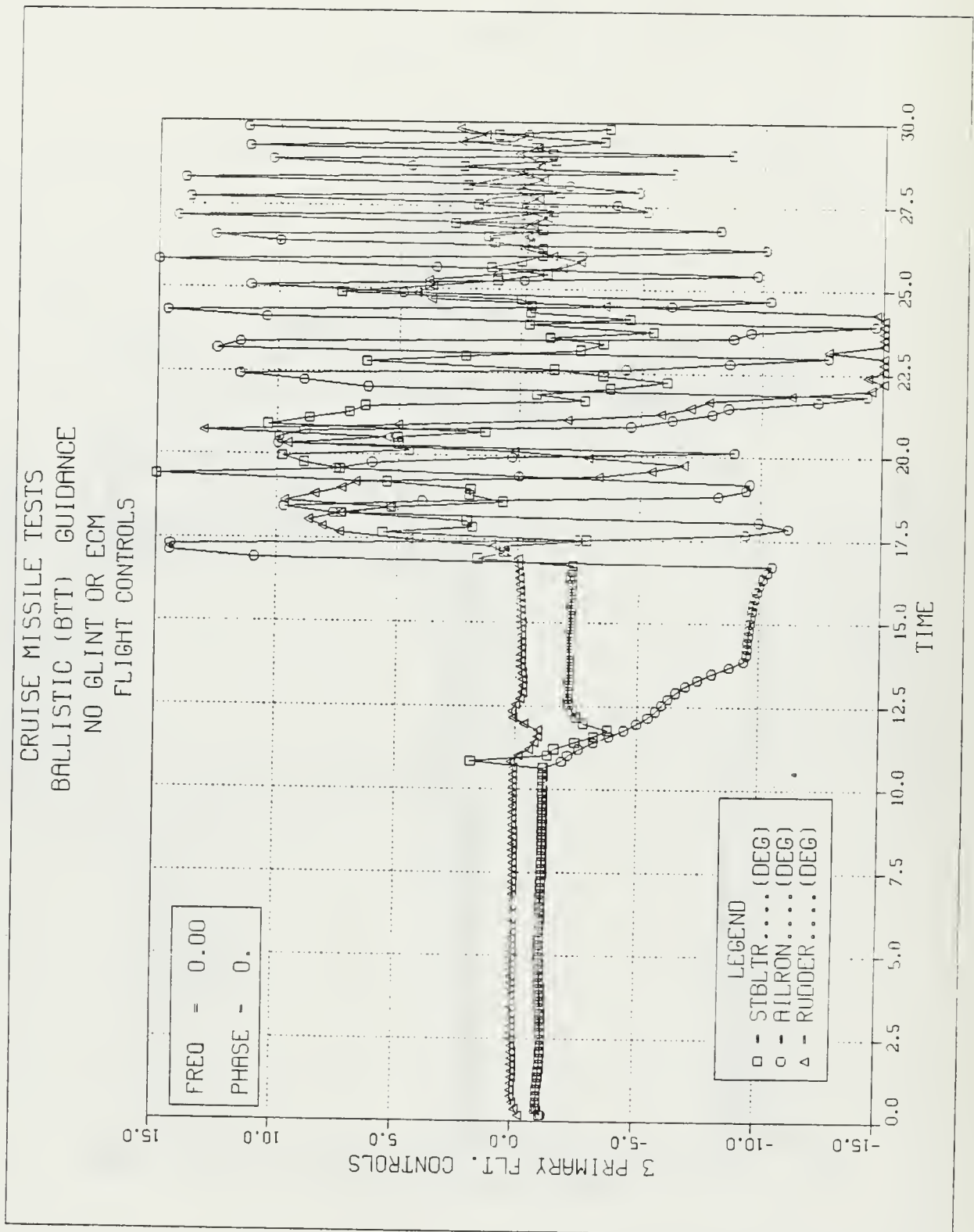


Figure A.85 Conf. VI Mission Set - Controls.

## SIMULATION PROGRAM TABULAR DATA OUTPUT

CRUISE MISSILE TESTS  
BASELINE MISSION SET  
GLINT PLUS ECM AT 0.2 FZ  
9-19-84

SIMULATION TERMINATED DUE TO CPA  
\*\*\* BLINKER FREQUENCY= 0.20  
\*\*\* BLINKER PHASE 0.

* MISS	* BANK	* ROLLRATE	* EKRUR	* FUNCTIONS	* AZIMUTH	* ELEVATION	* *
DISTANCE							
42.87372	0.20466	0.11202	0.03046			0.00866	*

\*\*\*\*\* RANGES FOR ALL SAVED VARIABLES \*\*\*\*\*

	MINIMUM	MAXIMUM
TIME..... (SEC)	0.190000	25.061737
NZC..... (G)	0.289882	4.000000
NZ..... (G)	0.551692	3.750864
BANK..... (DEG)	-115.634293	92.840149
BANK..... (DEG)	-115.765106	84.187943
RR/RT CMD..... (DPS)	-74.999985	74.999985
RRCLL RATE..... (DPS)	-73.526184	73.167145
ECM SHIFT..... (FT)	-75.000000	75.000000
GLINT SHIF T..... (FT)	-47.924805	47.070313
STBLTR..... (DEG)	-15.000000	7.934396
AILRCN..... (DEG)	-6.261881	0.000000



RUDCER... (DEG)  
 ALTITUDE... (FT)  
 XM... (FT NORTH)  
 YM... (FT EAST)  
 XT... (FT NORTH)  
 XM... (FT EAST)  
 RANGE... (FT)  
 PHASE MARKER

-3.446685  
 13.361130  
 159.440155  
 -3.526452  
 24000.000000  
 6.649995  
 116.888184  
 0.000000

2.952714  
 250.106537  
 23887.324200  
 17771.405030  
 24000.000000  
 1017.160640  
 23840.589800  
 4.000000

CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 FZ  
 9-19-84

\*\*\* BLINKER FREQUENCY=

0.20

DATA SET NUMBER 1 OF 4

TIME... (SEC) NZC... (G) NZ... (G) BANKC... (DEG) BANK... (DEG)

0.190000	0.996454	0.984984	0.838765	5.825313
0.380000	1.002067	0.939250	6.808969	6.542444
0.570000	1.012286	0.935853	6.645293	6.510144
0.759999	1.022474	0.946949	6.546911	6.356442
0.949999	1.030748	0.962120	6.503017	6.327555
1.139989	1.036386	0.977738	6.458877	6.279075
1.329975	1.039639	0.991862	6.585023	6.328140
1.519961	1.040093	1.004217	6.606047	6.380812
1.709948	1.038448	1.014323	6.744779	6.470833
1.899934	1.034911	1.021769	6.918423	6.623720
2.089920	1.029593	1.027047	7.007813	6.747380
2.279906	1.023017	1.030146	7.091106	6.834517
2.469893	1.015957	1.030586	7.323808	7.001084
2.659879	1.008910	1.028598	7.696206	7.254130
2.849865	1.002075	1.024892	8.092773	7.688922
3.039851	0.995503	1.020577	8.427500	8.050633
3.229837	0.989452	1.015759	8.742263	8.377364
3.419824	0.983882	1.010625	8.969087	8.645678
3.609810	0.979212	1.005136	9.224430	8.892548
3.799796	0.975287	0.999566	9.405898	9.108006
3.989782	0.972403	0.994111	9.605278	9.302847
4.179765	0.970392	0.988990	9.752930	9.474633
4.369755	0.965642	0.984181	9.988882	9.674054







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1.1625877
1.0333371
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26.628387
29.875137
33.380920
37.201050
41.270721
46.588922
51.988113
57.266112
62.538022
67.825088
73.156738
78.429143
83.651144
88.814499
94.067169
99.289008
104.512891
109.735605
114.953304
120.175912
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-20.514221
-21.803818
-23.991735
-26.628387
-29.875137
-33.380920
-37.201050
-41.270721
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-51.988113
-57.266112
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-109.735605
-114.953304
-120.175912
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-41.153802
-54.749466
-67.457657
-80.066727
-92.754532
-105.360977
-110.729401
-112.752167
-113.975922
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-115.765106
-115.013672
-112.811676
-108.906342
-102.649292
-93.434158
-81.214630

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CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 9-19-84

\*\*\* BLINKER FREQUENCY= 0.20

DATA SET NUMBER 1 OF 4

TIME.....(SEC) NZC.....(G) NZ.....(G) EANKC.....(DEG) BANK.....(DEG)

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24.314346
24.504242
24.694138
24.884033
25.073929
25.263824
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0.312690
0.289882
0.233168
0.411515
0.560545
0.793154
***
0.819130
0.748993
0.893249
0.642170
0.600143
0.574242
***
-41.207794
-12.722169
7.391577
14.987059
13.566038
11.100000
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-68.769150
-56.286392
-43.769882
-31.229416
-18.679732
-6.130711

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25.643351
25.833340
26.023340
26.213338
26.403335
26.593330
26.782990
26.972885
27.162781
27.352676
27.542572
27.732468
27.922363
28.112259
28.302155
28.492050
28.681946
28.871841
29.061737
***

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0.933357
1.042595
1.151395
1.261064
1.375287
1.493239
1.614298
1.749816
1.893453
1.728691
2.022277
2.183992
2.359669
2.545422
2.740000
2.940000
3.140000
3.340000
3.540000
3.740000
4.000000
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0.699352
0.796295
0.873536
0.945175
1.020734
1.093145
1.170446
1.246133
1.302967
1.323800
1.368543
1.460158
1.654933
2.019216
2.458335
2.864714
3.297837
3.747063
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7.270296
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-1.089107
-3.873116
-3.584943
-5.545876
1.781992
10.870007
14.335903
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92.840149
84.516556
87.914276
78.001495
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5.787602
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2.606247
0.250407
-1.234868
-2.835641
-3.809777
-4.924376
-1.654127
6.405855
8.333620
19.853433
31.915710
43.756592
55.290161
66.378754
77.037064
84.187943
81.152344
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```

CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 9-19-84

\*\*\* BLINKER FREQUENCY= 0.20

DATA SET NUMBER 2 OF 4

TIME.....(SEC) R/RT CMD...(DPS) ROLL RATE...(DPS) ECM SHIFT...(FT) GLINT SHIFT(FT)

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***
0.150000
0.380000
0.570000
0.759999
0.949999
1.139985
1.329975
1.519961
1.709948
1.899934
2.089920
***

12.067198
2.970557
1.389124
1.571068
1.868235
1.916773
2.881227
2.381867
3.031082
3.278272
2.867801
***

9.865781
0.744763
-0.660753
-0.488012
-0.235456
-0.222514
0.608558
0.131125
0.685417
0.850394
0.508729
***

-75.000000
-75.000000
-75.000000
-75.000000
-75.000000
-75.000000
-75.000000
-75.000000
-75.000000
-75.000000
-75.000000
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19.921875
47.070313
-43.310547
-25.952148
-15.886780
-47.524805
45.071082
-43.750000
19.897461
52.354405
-27.535063
***

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**	11.399245	*	-74.999985	*	-67.783478	*	-75.000000	*	-24.087524
**	11.589231	*	-10.854013	*	-11.366899	*	-75.000000	*	42.173767
**	11.779218	*	0.305608	*	-1.175964	*	-75.000000	*	-10.717773

CRUISE MISSILE TESTS  
BASELINE MISSION SET  
GLINT PLUS ECM AT 0.2 FZ  
9-19-84

\*\*\* BLINKER FREQUENCY= 0.20

DATA SET NUMBER 2 OF 4

TIME.....(SEC) R/RT CMD...(DPS) ROLL RATE...(DPS) ECM SHIFT...(FT) GLINT SHIFT(FT)

**	11.969204	*	1.725770	*	-0.077368	*	-75.000000	*	21.826172
**	12.159190	*	1.766047	*	0.153380	*	-75.000000	*	-22.363281
*	12.349176	*	1.522860	*	0.138551	*	-75.000000	*	-15.866780
*	12.539163	*	1.307849	*	0.090493	*	75.000000	*	-47.924805
*	12.729149	*	1.175968	*	0.044148	*	75.000000	*	45.671082
*	12.919135	*	1.126412	*	0.008935	*	75.000000	*	-43.750000
*	13.109121	*	1.140405	*	0.015377	*	75.000000	*	15.857461
*	13.299108	*	1.198962	*	-0.031489	*	75.000000	*	32.354405
*	13.489094	*	1.287829	*	-0.049077	*	75.000000	*	-27.539063
*	13.679080	*	1.422542	*	-0.068103	*	75.000000	*	-42.953164
*	13.869066	*	1.591445	*	-0.075865	*	75.000000	*	37.622070
*	14.059052	*	1.777146	*	-0.078154	*	75.000000	*	-5.277191
*	14.249039	*	1.954254	*	-0.075742	*	75.000000	*	2.807617
*	14.439025	*	2.131940	*	-0.069467	*	75.000000	*	-5.204102
*	14.629011	*	2.456958	*	-0.060213	*	75.000000	*	-0.720215
*	14.818997	*	2.443621	*	-0.048666	*	75.000000	*	33.416748
*	15.008984	*	2.566847	*	-0.035191	*	75.000000	*	-33.823735
*	15.198970	*	2.663178	*	-0.021065	*	75.000000	*	-33.227533
*	15.388956	*	2.731251	*	-0.007072	*	75.000000	*	-14.042664
*	15.578942	*	2.777195	*	0.006111	*	75.000000	*	31.372070
*	15.768929	*	2.784501	*	0.017965	*	75.000000	*	22.955322
*	15.958915	*	2.773720	*	0.028139	*	75.000000	*	43.412781
*	16.148833	*	2.742187	*	0.036394	*	75.000000	*	-34.065247
*	16.338730	*	2.653789	*	0.042625	*	75.000000	*	2.059605
*	16.528622	*	2.632695	*	0.046833	*	75.000000	*	1.255770
*	16.718521	*	2.563117	*	0.045088	*	75.000000	*	-12.655513
*	16.908417	*	2.489133	*	0.049957	*	75.000000	*	-28.857422
*	17.098312	*	2.414161	*	0.048846	*	75.000000	*	-24.087524

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TIME.....(SEC)	R/RT CMC...(CPS)	ROLL RATE...(DPS)	ECM SHIFT...(FT)	GLINT SHIFT(FT)
24.314346	74.995985	65.562851	75.000000	-43.750000
24.504242	74.995985	65.786819	75.000000	-15.897461
24.654138	74.995985	65.964462	75.000000	32.354409
24.840333	74.995985	66.055204	75.000000	-27.539063
25.073925	74.995985	66.085938	75.000000	-42.953164
25.263824	74.995985	66.059158	75.000000	37.622070
25.453720	22.935425	22.956116	75.000000	-35.271912
25.643616	-5.669250	-6.440586	75.000000	2.807617
25.833511	-10.200819	-10.561381	75.000000	-9.204102
26.023407	-13.224416	-14.461498	75.000000	-0.720215
26.213303	-17.424454	-17.331482	75.000000	3.416748
26.403158	1.460428	-13.733393	75.000000	-35.682373
26.593094	-12.643291	-13.444024	75.000000	-33.227535
26.782990	3.271104	0.505555	75.000000	-14.042664
26.972885	-7.714266	-9.377487	75.000000	-31.372070
27.162781	40.710358	33.784058	75.000000	22.955322
27.352676	53.080215	44.795210	75.000000	43.412781
27.542572	66.124893	25.035751	75.000000	-34.065247
27.732468	74.995985	63.833176	75.000000	31.209960
27.922363	74.995985	62.675156	75.000000	31.255776
28.112255	74.995985	61.318130	75.000000	-12.655313
28.302155	74.995985	58.976955	75.000000	-28.857422
28.492050	74.995985	56.138641	75.000000	-24.087524
28.681946	74.995985	54.246460	0.000000	42.173767
28.871841	43.046890	24.955106	0.000000	-10.717773
29.061737	-38.403168	-41.171707	0.000000	21.826172

CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 9-19-84

\*\*\* BLINKER FREQUENCY= 0.20

DATA SET NUMBER 3 OF 4

TIME.....(SEC) STBLTR.....(DEG) AILRCN.....(DEG) RUDDER.....(DEG) ALTITUDE....(FT)





TIME.....(SEC)	STBLTR.....(DEG)	AIRLON.....(DEG)	RUDDER.....(DEG)	ALTITUDE....(FT)
9.119411	3.569754	-3.22716	0.192114	41.688568
9.309397	-3.802303	-3.288725	0.248152	41.337570
9.499383	-3.889286	-3.262568	0.364863	41.600983
9.689365	-3.815103	-3.148677	0.489636	42.873740
9.879355	-3.543250	-2.976035	0.613086	43.858743
10.069342	-3.206109	-2.761302	0.718114	45.777054
10.259328	-2.801994	-2.526126	0.790657	47.981018
10.449314	-2.403330	-2.292121	0.826747	50.369045
10.639300	-2.053359	-2.077678	0.831036	52.759927
10.829287	-2.769983	-2.031552	0.837751	55.198746
11.019273	3.203503	-1.638245	0.107612	57.602005
11.209255	3.445362	-1.337570	-0.511320	60.053918
11.399245	3.550609	-1.067041	-0.863214	62.670746
11.589231	-0.761881	-0.860477	-1.133111	65.250519
11.779218	-0.806800	-0.768132	-1.088782	67.735687

CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 FZ  
 9-19-84

\*\*\* BLINKER FREQUENCY= 0.20

DATA SET NUMBER 3 OF 4

TIME.....(SEC) STBLTR.....(DEG) AIRLON.....(DEG) RUDDER.....(DEG) ALTITUDE....(FT)

11.969204	-0.915540	-0.65329	-0.792145	70.043457
12.159190	-0.818488	-0.525124	-0.461040	72.077484
12.349176	-0.699540	-0.417514	-0.218913	73.742950
12.539163	-0.612691	-0.339986	-0.095435	74.960114
12.729149	-0.566952	-0.305909	-0.054526	75.877820
12.919135	-0.557567	-0.324278	-0.055930	75.877914
13.109121	-0.575181	-0.376057	-0.073167	75.567383
13.299108	-0.611483	-0.457703	-0.093069	74.777695
13.489094	-0.661711	-0.561647	-0.110690	73.558517
13.679080	-0.739960	-0.676090	-0.125492	71.971645
13.869066	-0.826459	-0.795570	-0.138116	70.086105
14.059052	-0.917423	-0.928560	-0.148669	67.978912
14.249038	-1.008072	-1.056622	-0.156873	65.730785
14.439025	-1.094344	-1.177841	-0.162444	63.421967
14.629011	-1.172998	-1.287473	-0.165273	61.128418
14.818999	-1.241513	-1.381750	-0.165445	58.919155

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11157. 130630  
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2227. 984005  
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[illegible]

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1.202142

[illegible][illegible]





# GLINT PLUS ECM AT 0.2 HZ 9-19-84

\*\*\* BLINKER FREQUENCY=

0.20

DATA SET NUMBER 4 OF 4

TIME.....(SEC) XM....(FT NORTH) YM.....(FT EAST) XT....(FT NORTH) XM....(FT EAST)

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0.190000 0 159.440155 11275.43486 1115.99146 09810 -0.009810 24000.00000 6.49999
0.380000 0 13478.30175 11275.43486 1115.99146 09810 -0.009810 24000.00000 13.29998
0.570000 0 637.72827 11275.43486 1115.99146 09810 -0.009810 24000.00000 15.29998
0.759995 9 797.15161 11275.43486 1115.99146 09810 -0.009810 24000.00000 26.55997
0.949995 9 56.57348 11275.43486 1115.99146 09810 -0.009810 24000.00000 33.24996
1.139995 9 115.99146 11275.43486 1115.99146 09810 -0.009810 24000.00000 35.24996
1.329995 5 115.99146 11275.43486 1115.99146 09810 -0.009810 24000.00000 46.54911
1.519961 1 1275.43486 11275.43486 1115.99146 09810 -0.009810 24000.00000 53.15863
1.709948 8 1434.82031 11275.43486 1115.99146 09810 -0.009810 24000.00000 59.84816
1.899934 0 1594.22876 11275.43486 1115.99146 09810 -0.009810 24000.00000 66.45768
2.089920 6 1753.03247 11275.43486 1115.99146 09810 -0.009810 24000.00000 73.14720
2.279906 3 1913.03247 11275.43486 1115.99146 09810 -0.009810 24000.00000 75.14720
2.469893 5 2072.42651 11275.43486 1115.99146 09810 -0.009810 24000.00000 86.44622
2.659879 5 2231.15775 11275.43486 1115.99146 09810 -0.009810 24000.00000 93.05574
2.849865 1 2391.15775 11275.43486 1115.99146 09810 -0.009810 24000.00000 95.74527
3.039851 7 2550.94409 11275.43486 1115.99146 09810 -0.009810 24000.00000 106.35477
3.229837 4 2709.30786 11275.43486 1115.99146 09810 -0.009810 24000.00000 113.04429
3.419824 0 2869.30786 11275.43486 1115.99146 09810 -0.009810 24000.00000 119.09381
3.609810 6 3028.66553 11275.43486 1115.99146 09810 -0.009810 24000.00000 126.34333
3.799796 2 3188.01636 11275.43486 1115.99146 09810 -0.009810 24000.00000 133.95285
3.989782 5 3347.70027 11275.43486 1115.99146 09810 -0.009810 24000.00000 146.25188
4.179765 5 3506.60327 11275.43486 1115.99146 09810 -0.009810 24000.00000 152.94140
4.369741 7 3666.03596 11275.43486 1115.99146 09810 -0.009810 24000.00000 159.55092
4.559727 3 3825.38140 11275.43486 1115.99146 09810 -0.009810 24000.00000 166.24044
4.749713 0 3984.98437 11275.43486 1115.99146 09810 -0.009810 24000.00000 172.88990
4.939698 6 4143.25781 11275.43486 1115.99146 09810 -0.009810 24000.00000 179.53949
5.129686 2 4302.53125 11275.43486 1115.99146 09810 -0.009810 24000.00000 186.18899
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6.269603 9 5258.17187 11275.43486 1115.99146 09810 -0.009810 24000.00000 226.08610
6.459589 5 5417.44531 11275.43486 1115.99146 09810 -0.009810 24000.00000 232.73562

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** ** ** ** **
6.839576 736.703120 0.485856 24000.000000 39.0365147
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11.589231 9676.562500 375.463623 24000.000000 196.9230471
11.779218 9831.382810 407.341797 24000.000000 203.272461

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CRUISE MISSILE TEST IS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 HZ  
 9-19-84

\*\* BLINKER FREQUENCY= 0.20

DATA SET NUMBER 4 OF 4

TIME... (SEC) XM... (FT NORTH) YM... (FT EAST) XT... (FT NORTH) XM... (FT EAST)

```

** ** ** **
11.969204 * 9986.203120 * 439.127930 * 24000.000000 * 418.922119
12.159190 * 10141.023400 * 470.755654 * 24000.000000 * 425.571533
12.349176 * 10295.843700 * 502.336670 * 24000.000000 * 432.220947
12.539163 * 10450.683600 * 533.751709 * 24000.000000 * 438.877005

```



[illegible][illegible]

\*\*\*\*\*

**	10	6	0	5	5	7	8	1	0	0
**	10	7	6	0	4	7	2	7	0	0
**	10	9	1	5	3	9	8	4	0	0
**	11	0	7	0	3	6	7	2	0	0
**	11	2	2	5	3	3	5	9	0	0
**	11	3	8	0	3	7	5	0	0	0
**	11	5	3	5	4	1	8	0	0	0
**	11	6	9	0	5	2	3	4	0	0
**	11	8	4	5	6	4	0	6	0	0
**	12	0	0	0	8	2	8	1	0	0
**	12	1	5	6	0	2	7	3	0	0
**	12	3	1	1	2	5	3	0	0	0
**	12	4	6	6	5	7	4	2	0	0
**	12	6	2	1	9	1	4	1	0	0
**	12	7	7	7	2	6	1	7	0	0
**	12	9	3	2	6	7	5	8	0	0
**	13	0	8	8	0	8	9	8	0	0
**	13	2	4	3	5	5	0	8	0	0
**	13	3	9	9	0	3	9	1	0	0
**	13	5	5	4	5	2	7	3	0	0
**	13	7	1	0	0	5	4	7	0	0
**	13	8	6	5	6	1	7	2	0	0
**	14	0	2	1	1	7	9	7	0	0
**	14	1	7	6	7	4	2	2	0	0
**	14	3	3	2	3	5	1	6	0	0
**	14	4	8	3	9	8	8	3	0	0
**	14	6	4	3	6	2	5	0	0	0
**	14	7	9	9	2	6	1	7	0	0
**	14	9	5	4	9	4	9	2	0	0
**	15	1	1	0	6	6	0	2	0	0
**	15	2	6	6	3	7	1	1	0	0
**	15	4	2	7	0	8	2	0	0	0
**	15	5	7	7	8	6	7	2	0	0
**	15	7	3	3	6	5	2	3	0	0
**	15	8	9	4	3	7	5	0	0	0
**	16	0	4	5	2	4	6	1	0	0
**	16	2	0	1	1	0	9	4	0	0
**	16	3	5	7	0	5	4	7	0	0
**	16	5	1	3	0	7	8	1	0	0
**	16	6	6	5	1	6	0	2	0	0
**	16	8	2	5	2	4	2	2	0	0
**	16	9	8	1	2	6	9	5	0	0
**	17	1	3	9	1	3	6	7	0	0
**	17	2	9	2	7	8	9	1	0	0
**	17	4	4	8	1	5	6	2	0	0
**	17	6	0	3	2	0	3	1	0	0
**	17	7	5	7	9	7	2	7	0	0
**	17	9	1	2	5	1	5	6	0	0

\*\*\*\*\*

TIME.....(SEC)	XM... (FT NORTH)	YM... (FT EAST)	XT... (FT NORTH)	XM... (FT EAST)	DATA SET NUMBER	UF
21.845703	18066.9	10200	1770.7	707280	24000.0	000000
22.035595	18221.2	03100	1767.5	811790	24000.0	000000
22.225494	18375.4	29700	1762.4	311400	24000.0	000000
22.415390	18529.6	09400	1755.4	13820	24000.0	000000
22.605286	18683.7	22700	1746.5	58110	24000.0	000000
22.795181	18837.7	46100	1735.8	56970	24000.0	000000
22.985077	18991.0	44500	1725.4	93900	24000.0	000000
23.174973	19145.4	02300	1709.4	31880	24000.0	000000
23.364868	19299.0	07800	1693.8	09570	24000.0	000000
23.554764	19452.4	37500	1676.7	30710	24000.0	000000
23.744659	19605.6	95300	1658.2	95170	24000.0	000000
23.934555	19758.7	85200	1638.6	00340	24000.0	000000
24.124451	19911.6	99200	1617.7	746830	24000.0	000000

CRUISE MISSILE TESTS  
 BASELINE MISSION SET  
 GLINT PLUS ECM AT 0.2 FZ  
 9-19-84

\*\*\* BLINKER FREQUENCY= 0.20

TIME.....(SEC) XM... (FT NORTH) YM... (FT EAST) XT... (FT NORTH) XM... (FT EAST)

24.314346	20064.4	60900	1555.8	48880	24000.0	000000
24.504242	20217.0	89800	1573.0	31490	24000.0	000000
24.694138	20369.6	17200	1549.4	32370	24000.0	000000
24.884033	20522.0	62500	1525.1	58730	24000.0	000000
25.073924	20674.4	41400	1500.4	4370	24000.0	000000
25.263824	20826.8	12500	1475.4	40190	24000.0	000000
25.453720	20979.1	83600	1450.2	01660	24000.0	000000
25.643616	21131.5	78100	1424.8	48630	24000.0	000000
25.833511	21284.0	23400	1399.4	23830	24000.0	000000
26.023407	21436.5	27300	1373.9	27490	24000.0	000000
26.213303	21589.0	078100	1348.3	37400	24000.0	000000
26.403198	21741.6	71900	1322.6	15970	24000.0	000000
26.593094	21894.3	39800	1296.7	26810	24000.0	000000
26.782990	22047.0	39100	1270.6	28660	24000.0	000000
26.972885	22199.7	81200	1244.2	85160	24000.0	000000
27.162781	22352.5	66400	1217.6	80910	24000.0	000000
27.352676	22505.3	50600	1190.8	84520	24000.0	000000
27.542572	22658.2	85200	1164.0	029050	24000.0	000000

\*\*\*\*\*

27.732468  
27.9112255  
28.1302155  
28.3452050  
28.4819461  
28.6871841  
28.871737

22811.2361700  
22914.343700  
23117.585900  
23271.027300  
23424.718700  
23578.683600  
23732.902300  
23887.324200

\*\*\*\*\*

1137.2862230  
1110.862550  
1085.108890  
1060.465970  
1037.558840  
1017.097900  
999.782715  
986.245850

\*24000.000000  
\*24000.000000  
\*24000.000000  
\*24000.000000  
\*24000.000000  
\*24000.000000  
\*24000.000000  
\*24000.000000

\*\*\*\*\*

970.6271530  
977.2827155  
983.9289555  
990.5275195  
997.2216800  
1003.8679200  
1010.5144000  
1017.1606400



## TASM SIMULATION PROGRAM NCMENCLATURE

TIME IN SECONDS  
INTEGRATION INTERVAL  
OUTPUT INTERVAL  
NUMBER OF OUTPUTS  
FLAG SET TO INDICATE TERMINATION & REASON  
ARRAY CONTAINING ALL SAVED DATA  
SETS THE PHASE APPLIED TO ECM BLINKER  
SETS THE RANGE AT WHICH CLIMB IS COMMENCED

U,V,W	BODY AXIS LINEAR VELOCITIES (FT/SEC)
UCCCT,VDDOT,WDDOT	BODY AXIS LINEAR ACCELERATIONS
P,C,R	BODY AXIS ANGULAR VELOCITIES (RAD/SEC)
PRCLLRT,PTCHRT,YAWRT	BODY AXIS ANGULAR VELOCITIES (DEG/SEC)
PCCCT,QDDOT,RDDOT	BODY AXIS ANGULAR ACCELERATIONS
X,Y,Z	BODY AXIS AERODYNAMIC FORCES (LBS)
L,C	LIFT, DRAG AERODYNAMIC FORCES (LBS)
L,A,M,A,N,A	BODY AXIS AERODYNAMIC MOMENTS (FT-LBS)
PHI,I,THETA,SY	EULER ANGLES (RAD)
BANK,PITCH,HEADNG	EULER ANGLES (DEG)
PHICOT,THETAD,SYDDOT	ANGLE OF ATTACK, RATE OF CHANGE OF
ALFA,BETA	ANGLE OF ATTACK, SIDESLIP (RAD)
ACA,SIDESL	RATE OF CHANGE OF ALFA, BETA
ALFADOT,BETADOT	FLIGHT PATH ANGLE (RAD)
GAMMA	FLIGHT PATH ANGLE (DEG)
FLTPTH	LATERAL ACCELERATION, LOAD FACTOR (G'S)
WV,NZ	EARTH COORDINATES OF MISSILE (FT)
XM,YM,ALTUDE	(XM-NORTH, YM-EAST)
XMECT,YMDOT,HMDOT	RATES OF CHANGE OF XM, YM, ALTITUDE
VT	TOTAL MISSILE VELOCITY (FT/SEC)
CHCRD,SPAN	MEAN AERODYNAMIC CHORD, SPAN (FT)
CHCRD2,SPAN2	HALF CHORD, HALF SPAN

WT,M,G GROSS WEIGHT, MASS, ACCEL DUE TO GRAVITY  
T,S THRUST, WING AREA  
R,FC AIR DENSITY  
QS DYNAMIC PRESSURE X WING AREA  
C-- AERODYNAMIC COEFFICIENTS  
DC-- INCREMENTS IN  
IXX,IYY,IZZ,IXZ MOMENTS AND PRODUCTS OF INERTIA  
IA- IK FUNCTIONS OF  
ELE,AIR,RUD CONTROL DEFLECTIONS (DEG)  
STBLTR,AIRLON,RUDDER STANDARD CONTROL DEFLECTIONS WITH LIMITS  
RSTAB1,LSTAB1 TASM UNLIMITED CONTROL DEFLECTIONS (DEG)  
RSTAB,LSTAB TASM LIMITED CONTROL DEFLECTIONS (DEG)  
---1 INITIAL CONDITION

# AUTCPILOT

K--- AUTOPILOT GAINS  
CGARM- ACCELEROMETER LOCATION WRT CG  
E--- COMPARATOR ERRORS  
---LIM LIMITED VALUES  
---SERI SERVO INPUTS  
---SERC SERVO OUTPUTS  
---C COMMANDED VALUES  
---F,---FF,---FFF FILTERED SENSOR VARIABLE  
FNCCF-,FDCOF- NOTCH FILTER COEFFICIENTS

# GUIDANCE

AZC,AYC COMMANDED VERTICAL AND HORIZONTAL  
XT,YT,HT ACCELERATIONS IN EARTH AXES (G'S)  
XR,YR,HR EARTH COORDINATES OF TARGET (FT)  
XRECM,YRECM,HRECM POSITION OF THE TARGET WRT MISSILE IN  
XDCTR,YDCTR,HDCTR EARTH COORDINATES (FT)  
XECM,YECM,HECM AND GLINT OF RADAR TARGET (XR,YR,HR WITH ECM  
XGLNT,YGLNT,HGLNT RATES OF CHANGE WRT MISSILE (FT)  
RANGE (RELATIVE VELOCITY OF TGT WRT MISSILE)  
RNGECM,RGECMT INCR. IN TARGET RADAR POSITION DUE TO ECM  
TSPEED RANGE IN TARGET RADAR POSITION DUE TO GLINT  
SYT,THETAT RANGE TO RADAR TARGET (TGT WITH ECM+GLINT)  
HEADT,ELEVVT TARGET SPEED (FT/SEC)  
VTANAZ,VTANEL HEADING, ELEV. TGT TARGET FROM MISSILE (RAD)  
TRAKAZ,TRAKEL COMPONENT OF RELATIVE VEL. PERPENDICULAR  
TO LOS IN AZIMUTH AND ELEVATION (FT/SEC)  
COMPONENT OF MISSILE VELOCITY VECTOR IN

SIGAZ, SIGEL  
 DSIGAZ, DSIGEL  
 SIGDAZ, SIGDEL  
 DSGCAZ, DSGDEL  
 SIGDAF, SIGDEF  
 DSGCAF, DSGDEF  
 LAMCAZ, LAMDEL  
 FREQ  
 SHIFTY, SHIFTH  
 BRNTHR  
 KNFAZ, KNFEL  
 AZIMUTH AND ELEVATION (FT/SEC)  
 EARTH AZIMUTH, ELEVATION LOS ANGLES (RAD)  
 EARTH AZIMUTH, ELEVATION LOS ANGLES (DEG)  
 RATES OF CHANGE OF EARTH REFERENCED LOS  
 (RAD/SEC)  
 SAME AS ABOVE (DEG/SEC)  
 FILTERED SIGDAT, SIGDET (RAD/SEC)  
 FILTERED DSGCAT, DSGDET (DEG/SEC)  
 PROPORTIONAL NAVIGATION CONSTANTS  
 FREQUENCY OF ECM BLINKING  
 DISTANCE OF ECM BLINKER FROM TARGET AIM  
 POINT (FT)  
 BURN-THROUGH RANGE  
 AZIMUTH AND ELEVATION NAVIGATION FILTER  
 CONSTANTS

# APPENDIX D

## MAIN PROGRAM LISTING FOR TACTICAL CRUISE MISSILE SIMULATION

\*\*\*  
TRANSLATED BY  
CDR BARTON P. ANDERSON, USN  
\*\*\*  
NAVY POSTGRADUATE SCHOOL  
DEPARTMENT OF AERONAUTICAL ENGINEERING  
MCNTEREY, CA 93943  
\*\*\*  
TRANSLATED FROM CSMP PROGRAM BY  
DR. MARLE HEWETT  
LCDR KENT WATTERSON, USN

\*\*\*  
PROGRAM TCMC  
\*\*\*  
CONTROLS THE OVERALL EXECUTION OF THE SIMULATION. CALLS THE  
NECESSARY SUBROUTINES, DETERMINES WHEN THE DATA MUST BE STORED  
FOR OUTPUT AND WHEN THE RUN HAS COMPLETED DUE TO CPA OR FINTIM.  
\*\*\*  
9-10-84  
\*\*\*

IMPLICIT REAL(A-Z)  
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NOUT,PCOUNT,NFAZE

\*\*\*  
COMMON BLOCK /A/: MISCELLANEOUS CONSTANTS  
\*\*\*

COMMON /A/ TIME , FINTIM,DT ,CPUT ,NCUT ,NPTS ,CPA ,PCOUNT,  
G , IXX , IYY , IZZ , IY , IZ , IY , IZ , IY , IZ , IY , IZ ,  
ID , IE , IF , IG , IH , II , IJ , IK , IS ,  
CHORD2,CHORD ,SPAN2,SPAN ,NFAZE

\*\*\*  
COMMON BLOCK /H/: ECM/GLINT PARAMETERS  
\*\*\*

```

C
COMMON /H/  FREQ      ,SHIFTH  ,BRNTHR ,
             XECM      ,HECM     ,XGLNT  ,
             YGLNT     ,XTECM    ,YTECM   ,
             HTECM      ,          ,
**
**
**
C
*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****
C
COMMON /F/  PH1  PH2  PH3  PH4  MISDST ,
             OFFSET  ALTATT  SGDZPU  MISDST ,
             LAMCAZ  LAMDEL  KNFAZ  KNFEL  ,
             NZC     PHIC   GAMMAC  PCLIM  ,
             PC      QC     RANGDEF  RANGE ,
             SIGAZ   SIGEL  SIGCAF  SIGDEF ,
             SYT     THETAT  XT      YT     ,
             HT      NYC     POPRNG  ,
**
**
**
C
*****
COMMON BLOCK /I/: CUTPUT ARRAY
*****
C
COMMON /I/  PTS(300,20)
*****
**
**
**
C
*****
INITIALIZE ALL VARIABLES
*****
C
PLCTTING SURFACE
*****
C
CALL TEK618
CALL CCMPRS
CALL SWISSM
*****
C
1 CALL INIT
*****
C
**
**
**
C
*****
BEGIN DYNAMIC SIMULATION
*****
C
10 IF (CPA.GE.1.0) GO TO 100
   TIME=TIME+DT
   IF (TIME.GE.FINTIM) CPA=2.0
   PCCUNT = PCCUNT+1
*****
C
**
**
**
C
*****
FROM MISSION PROFILE/GUIDANCE, GENERATE NZC,PHIC
*****

```



```

C      CALL MISSN1
C
C      *** GENERATE CONTROL MOVEMENTS: STBLTR, AILRON, RUDDER
C      CALL APILOT
C
C      *** GENERATE MISSILE MCTION AND POSITION
C      CALL AERO
C
C      *** GENERATE APPARENT RADAR TARGET POSITION & MCTION
C      CALL TGTNAV
C
C      *** STCRE REQUIRED PLOT DATA IN THE PTS ARRAY.
C      IF (PCOUNT.LT.NOUT) GO TO 50
C      CALL PREPAR
C      PCOUNT = 0.0
C      50 CONTINUE
C      GC TO 10
C      100 CONTINUE
C      *** END DYNAMIC SIMULATION *****
C      *** INVOKE DISPLA AND TABULAR OUTPUT ROUTINES
C      CALL CLTPUT(NPTS,CPA)
C      ***** TESTPATCH TO BYPASS ITERATIONS (KTEST = 1)
C      KTEST = 0
C      IF (KTEST.EQ.1) GC TO 150
C      ***** ENDTEST
C      *** ITERATE THE PHASE VARIABLE IN THE ECM PACKAGE
C      NFAZE = NFAZE + 1
C      IF (NFAZE.LE.4) GO TO C 1
C      NFAZE = 1
C

```





```

C
**      AOA1      PITCHR1      ROLLR1      YAWR1      ,
**      XT1      ,YT1      ,HT1      ,TSPEED      ,
C
COMMON /F/ PH1 OFF SET      PH3      PH4      ,
*      LAMDAZ      ,ALTAIT      ,SGDZPU      ,MISDST      ,
*      NZC      ,LAMDEL      ,KNFAZ      ,KNFEL      ,
*      PC      ,PHIC      ,GAMMAC      ,PC LIM      ,
*      SIGAZ      ,QC      ,RC      ,RANGE      ,
*      SYT      ,SIGEL      ,SIGDEF      ,
*      HT      ,THETAT      ,YT      ,
C
COMMON /H/ FREQ      SHIFTH      BRNTHR      ,
*      XECM      ,YECM      ,XGLNT      ,
*      HTECM      ,HGLNT      ,XTECM      ,
C
COMMON /I/ PTS(300,20)
C
EXECUTABLE STMTS *****
C
**      COMPUTEL CONSTANTS
C
PI I= 18C.0/PI
IA = IXX*IZZ-I XZ**2
IB = IZZ/IA
IC = I XZ/IA
ID = I XZ*(IYY-I XX-I ZZ)/IA
IE = (IZZ**2-I YY*IZZ+I XZ**2)/IA
IF = I/IYY
IG = (I XX-I ZZ)/IYY
IH = I XZ/IYY
II = I XX/IA
IJ = (I XX*I YY-I XX**2-I XZ**2)/IA
IK = (I XX+I ZZ-I YY)*I XZ/IA
C
PLIM = RRLIM/PI I
C
*****
C
PARAMETERS TO BE INITIALIZED FOR EACH RUN FOLLOW.
*****
C
TIME = C.0
CPA = 0
PCCUNT = 0
NOUT = INT(CPDT/DT)
IF (AMGC(CPDT,DT).GE.0.5) NOUT=NOUT+1

```

```

C      NP TS = C
DO 100 I=1,300
DC 50 J=1,20
      PTS(I,J) = 0.0
      CCNT INLE
50 CONTINUE
100 CONTINUE
C      U = L1
      W = L1*TAN(AOAL/PII)
      V = SQR(U**2+W**2)*TAN(SIDES1/PII)
      VT = SQR(U**2+V**2+W**2)
      QS = 12.0*RHO*(VT**2)/2.0
C      P = RCLLRI/PII
      Q = FTCHRI/PII
      R = YAWRI/PII
C      PDCT = 0.0
      QDCT = 0.0
      RDOT = 0.0
C      THETA = PITCH1/PII
      PHI = BANK1/PII
      SY = HEDNG1/PII
      GAMMA = 0.0
      NZ = 1.0
C      XM = XM1
      YM = YM1
      ALTUDE = ALTUD1
C      AOA = ACAL
      ALFA = ACAL/PII
      ALFADT = 0.0
C      SIDESL = SIDES1
      BETA = SIDES1/PII
      BETADT = 0.0
C      XT = XT1
      YT = YT1
      HT = HT1
      RANGE = SQR((XT-XM)**2+(YT-YM)**2+(HT-ALTUDE)**2)
C      PH1 = 0
      PH2 = C

```





```

**          YGLNT      ,HGLNT      ,XTECM      ,YTECM      ,
**          FTECM
C C C C C
*****
COMMON BLOCK / I/: OUTPUT ARRAY
*****
COMMON / I/ PTS(300,20),PLTN(6,7),XN(6,7),YN(6,7),TITLE(8,4),
*          LEG(4,20)
C C C C C
*****
INITIALIZE THE DATA
*****
COMMON ELCCCK / A/: MISCELLANEOUS CONSTANTS
*****
DATA      TIME      ,FINTIM ,DT      ,CPA      /
*          /0.0      ,30.0      ,0.01      ,0.20      ,0
DATA      C          ,T          ,RHU      ,PI      ,WT      ,MASS
*          /32.17      ,242.3      ,.002377      ,3.141593      ,2200.      ,68.38      /
DATA      IXX      ,IYY      ,IZZ      ,IXZ      ,S          /
*          /27.8      ,1507.0      ,1512.0      ,11.7      ,12.0      ,
DATA      CHURD2,CHORD      ,SPAN2      ,SPAN      ,NFAZE      /
*          /0.707      ,1.414      ,4.2425      ,8.485      ,1
C C C C C
*****
COMMON ELCCCK / B/: AERODYNAMIC COEFFICIENT TABLES
*****
** STATIC AERODYNAMIC CCEFFICIENTS
* 1. LIFT COEFFICIENT DATA
A. CLBAS VS. AOA (BASIC LIFT CCEFFICIENT AS A FUNCTION
CF ANGLE OF ATTACK)
DATA LFT1/ -12.0,-0.32, -11.0,-0.29, -10.0,-0.46, -9.0,-0.57,
*          -8.0,-0.70, -7.0,-0.69, -6.0,-0.65, -5.0,-0.58,

```



```

* * * * *
-4.0,-0.50, -3.0,-0.42, -2.0,-0.30, -1.0,-0.18,
0.0,-0.08, 1.0,0.04, 2.0,0.15, 3.0,0.25,
4.0,0.38, 5.0,0.47, 6.0,0.58, 7.0,0.69,
8.0,0.80, 9.0,0.87, 10.0,0.78, 11.0,0.70,
12.0,0.64, 22*9999.0/

```

C C C C C

# B. DCLSTE VS. STBLTR (INCREMENT IN LIFT COEFFICIENT DUE TO SYMMETRIC STABILATOR DEFLECTION)

```

DATA LFT2/ -15.0,-100, -14.0,-0.97, -13.0,-0.94, -12.0,-0.90,
-11.0,-0.84, -10.0,-0.78, -9.0,-0.71, -8.0,-0.65,
-7.0,-0.58, -6.0,-0.48, -5.0,-0.40, -4.0,-0.32,
-3.0,-0.24, -2.0,-0.16, -1.0,-0.08, 0.0,0.00,
1.0,0.08, 2.0,0.16, 3.0,0.24, 4.0,0.33,
5.0,0.41, 6.0,0.49, 7.0,0.57, 8.0,0.65,
9.0,0.73, 10.0,0.80, 11.0,0.86, 12.0,0.92,
13.0,0.96, 14.0,0.98, 15.0,1.00, 10*9999. /
* * * * *

```

C C C C C C C

## \* 2. DRAG COEFFICIENT DATA

# A. CDBAS VS. CLBAS (BASIC DRAG COEFFICIENT AS A FUNCTION OF BASIC LIFT COEFFICIENT)

```

DATA DRG1/ -9, -0.80, -8, -0.61, -7, -0.50, -6, -0.42,
-5, -0.35, -4, -0.31, -3, -0.26, -2, -0.23,
-1, -0.22, 0, -0.22, 0.1, -0.23, 0.2, -0.24,
0.3, -0.28, 0.4, -0.31, 0.5, -0.36, 0.6, -0.42,
0.7, -0.49, 0.8, -0.57, 0.9, -0.68, 1.0, -0.80,
32*9999. /
* * * * *

```

C C C C C

# B. LCDSTE VS. STBLTR (INCREMENT IN DRAG COEFFICIENT DUE TO SYMMETRIC STABILATOR DEFLECTION)

```

DATA DRG2/ -15., -0.106, -14., -0.091, -13., -0.077, -12., -0.05,
-10., -0.044, -9., -0.036, -8., -0.028, -7., -0.022,
-6., -0.016, -5., -0.011, -4., -0.007, -3., -0.003,
-2., -0.001, -1., 0.001, 0., 0.001, 1., 0.001,
2., 0.004, 3., 0.007, 4., 0.011, 5., 0.016,
6., 0.023, 7., 0.030, 8., 0.039, 9., 0.049,
10., 0.060, 11., 0.073, 12., 0.089, 13., 0.106,
14., 0.126, 15., 0.146, 22*9999. /
* * * * *

```

C C C C C

# C. DCDSTA VS. AILRON (INCREMENT IN DRAG COEFFICIENT DUE TO ASYMMETRIC STABILATOR DEFLECTION)

```

DATA DRG3/ -15., .0120, -14., .0102, -13., .0085, -12., .0071,
-10., .0048, -9., .0038, -8., .0030, -7., .0023,
-6., .0016, -5., .0011, -4., .0007, -3., .0003,
-2., .0001, -1., .0000, 0., .0000, 1., .0000,
2., .0001, 3., .0003, 4., .0007, 5., .0011,
6., .0017, 7., .0023, 8., .0030, 9., .0038,
10., .0048, 11., .0055, 12., .0071, 13., .0085,
14., .0100, 15., .0120, 12*9999./
** ** ** ** **

```

CCCC

#### D. DCDSTR VS. RUDDER (INCREMENT IN DRAG COEFFICIENT DUE TO RUDDER DEFLECTION)

```

DATA DRG4/ -15., .0059, -14., .0054, -13., .0048, -12., .0043,
-10., .0032, -9., .0027, -8., .0022, -7., .0017,
-6., .0013, -5., .0009, -4., .0006, -3., .0003,
-2., .0002, -1., .0001, 0., .0000, 1., .0001,
2., .0001, 4., .0006, 5., .0009, 6., .0013,
7., .0017, 8., .0022, 9., .0027, 10., .0032,
11., .0037, 12., .0043, 13., .0048, 14., .0054,
15., .0059, 12*9999./
** ** ** ** **

```

CCCCCCCC

### \* 3. PITCHING MOMENT COEFFICIENT DATA

#### A. CMBAS VS. ACA (BASIC PITCHING MOMENT COEFFICIENT AS A FUNCTION OF ANGLE OF ATTACK)

```

DATA PTCH1/ -10., 1.13, -8., 0.80, -6., 0.50, -4., 0.31,
-2., 0.16, 0., 0.08, 2., -0.03, 4., -0.13,
6., -0.22, 8., -0.32, 10., -0.46, 12., -0.62,
48*9999./
** ** **

```

CCCC

#### B. DCMSTE VS. STBLTR (INCREMENT IN PITCHING MOMENT COEFFICIENT DUE TO SYMMETRIC STABILATOR DEFLECTION)

```

DATA PTCH2/ -15., .90, -14., .88, -12., .78, -10., .68,
-8., .56, -6., .42, -4., .27, -2., .12,
0., .00, 2., -.10, 4., -.20, 6., -.32,
8., -.45, 10., -.58, 12., -.69, 14., -.78,
15., -.80, 38*9999./
** ** **

```

CCCCCCCC

### \* 4. SIDESLIP COEFFICIENT DATA

#### A. CYBAS VS. SIDESL AND AGA (BASIC SIDE FORCE COEFFICIENT AS A FUNCTION OF SIDESLIP AND ANGLE OF ATTACK. THE IN- DEPENDENT VARIABLE IS SIDESLIP, THE PARAMETER IS ANGLE OF ATTACK).

C

```

DATA SIC1/  0.0,      -8.0,      -6.0,      4.0,      8.0,      9999. /
            -8.0,      -6.0,      0.148,  0.149,  0.140,  0.137,  9999. /
            -6.0,      0.111,  0.110,  0.100,  0.100,  0.077,  9999. /
            -4.0,      0.073,  0.072,  0.063,  0.060,  0.060,  9999. /
            -2.0,      0.034,  0.034,  0.025,  0.022,  0.022,  9999. /
            0.0,      -0.002,  -0.003,  -0.013,  -0.020,  -0.020,  9999. /
            2.0,      -0.040,  -0.042,  -0.050,  -0.060,  -0.060,  9999. /
            4.0,      -0.077,  -0.078,  -0.085,  -0.096,  -0.096,  9999. /
            6.0,      -0.114,  -0.116,  -0.127,  -0.129,  -0.129,  9999. /
            8.0,      -0.151,  -0.153,  -0.162,  -0.162,  -0.162,  9999. /
*
*
*
*
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*
*

```

C C C C C

# B. CRBAS VS. SIDESL AND ACA (BASIC ROLL COEFFICIENT AS A FUNCTION OF SIDESLIP AND PARAMETER ANGLE OF ATTACK)

```

DATA SIC2/  0.0,      -8.0,      2.0,      6.0,      10.0,      9999. /
            -8.0,      -0.048,  -0.046,  -0.040,  -0.044,  9999. /
            -6.0,      -0.038,  -0.036,  -0.028,  -0.030,  9999. /
            -4.0,      -0.026,  -0.022,  -0.015,  -0.020,  9999. /
            -2.0,      -0.014,  -0.010,  -0.004,  -0.008,  9999. /
            0.0,      -0.004,  -0.004,  -0.004,  -0.002,  9999. /
            2.0,      -0.005,  -0.014,  -0.020,  -0.014,  9999. /
            4.0,      -0.016,  -0.026,  -0.032,  -0.025,  9999. /
            6.0,      -0.030,  -0.038,  -0.042,  -0.036,  9999. /
            8.0,      -0.044,  -0.052,  -0.057,  -0.048,  9999. /
*
*
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*
*
*
*
*

```

C C C C C

# C. CNBAS VS. SIDESL AND ACA (BASIC YAW COEFFICIENT AS A FUNCTION OF SIDESLIP AND PARAMETER ANGLE OF ATTACK)

```

DATA SIC3/  0.0,      -8.0,      0.0,      6.0,      8.0,      9999. /
            -8.0,      -0.034,  -0.037,  -0.042,  -0.042,  9999. /
            -6.0,      -0.025,  -0.028,  -0.033,  -0.033,  9999. /
            -4.0,      -0.016,  -0.019,  -0.022,  -0.023,  9999. /
            -2.0,      -0.007,  -0.009,  -0.012,  -0.014,  9999. /
            0.0,      -0.010,  -0.001,  -0.004,  -0.004,  9999. /
            2.0,      -0.010,  -0.009,  -0.007,  -0.007,  9999. /
            4.0,      -0.019,  -0.018,  -0.016,  -0.016,  9999. /
            6.0,      -0.028,  -0.026,  -0.024,  -0.024,  9999. /
            8.0,      -0.036,  -0.034,  -0.032,  -0.032,  9999. /
*
*
*
*
*
*
*
*

```

C C C C C C C

## \* 5. DIRECTIONAL CONTROL COEFFICIENT DATA

A. CCYSTR VS. RUDDER AND ACA (INCREMENT IN SIDE FORCE  
COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER  
ANGLE OF ATTACK)

C

```

DATA DREC1/ 0.0, -8.0, 2.0, 6.0, 8.0, 999.
-15.0, -0.90, -0.97, -0.95, -1.02, 999.
-10.0, -0.60, -0.62, -0.62, -0.69, 999.
-5.0, -0.32, -0.36, -0.37, -0.42, 999.
0.0, -0.04, -0.02, -0.03, -0.03, 999.
5.0, -0.40, -0.42, -0.38, -0.04, 999.
10.0, -0.70, -0.66, -0.62, -0.66, 999.
15.0, -1.00, -0.98, -0.92, -0.96, 999.
12*99955./

```

C C C C C C

B. CCNSTR VS. RUDDER AND AGA (INCREMENT IN YAWING MOMENT  
COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER  
ANGLE OF ATTACK)

```

DATA DREC2/ 0.0, -8.0, 2.0, 6.0, 8.0, 999.
-15.0, -0.70, -0.68, -0.62, -0.65, 999.
-10.0, -0.50, -0.49, -0.48, -0.48, 999.
-5.0, -0.26, -0.24, -0.22, -0.18, 999.
0.0, -0.00, -0.00, -0.00, -0.00, 999.
5.0, -0.22, -0.20, -0.18, -0.14, 999.
10.0, -0.52, -0.48, -0.47, -0.46, 999.
15.0, -0.80, -0.79, -0.74, -0.75, 999.
12*99955./

```

C C C C C C

C. DCRSTR VS. RUDDER AND AGA (INCREMENT IN ROLLING MOMENT  
COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER  
ANGLE OF ATTACK)

```

DATA DREC3/ 0.0, -8.0, 2.0, 4.0, 6.0, 8.0, 999.
-15.0, -0.50, -0.38, -0.32, -0.22, 0.02, 999.
-10.0, -0.34, -0.29, -0.26, -0.20, -0.04, 999.
-5.0, -0.18, -0.18, -0.18, -0.14, -0.08, 999.
0.0, -0.04, -0.00, -0.03, -0.08, -0.13, 999.
5.0, -0.24, -0.12, -0.04, -0.05, -0.14, 999.
10.0, -0.48, -0.28, -0.16, -0.00, -0.16, 999.
15.0, -0.70, -0.53, -0.40, -0.12, -0.25, 999.
12*99955./

```

C C C C C C C C

\* 6. LATERAL CONTROL COEFFICIENT DATA

A. CCYSTA VS. AIRLON AND AGA (INCREMENT IN SIDE FORCE  
COEFFICIENT DUE TO ASYMMETRIC STABILATOR DEFLECTION AND  
PARAMETER ANGLE OF ATTACK)



```

DATA LTRL1/ 0.0, -8.0, , -1.0, , 4.0, , 10.0, , 9999.,
-15.0, -015, , -019, , -017, , -006, , 9999.,
-10.0, -013, , -014, , -010, , -002, , -002, , 9999.,
-5.0, -010, , -009, , -002, , -010, , -002, , 9999.,
0.0, -007, , -002, , -007, , -018, , -007, , 9999.,
5.0, -002, , -003, , -014, , -026, , -026, , 9999.,
10.0, -005, , -009, , -020, , -033, , -033, , 9999.,
15.0, -010, , -014, , -025, , -042, , -042, , 9999.,
12*99999./

```

CCCCC

B. CCNSTA VS. AIRLON AND ADA (INCREMENT IN YAWING MOMENT  
COEFFICIENT DUE TO ASYMMETRIC STABILATOR DEFLECTION AND  
PARAMETER ANGLE OF ATTACK)

```

DATA LTRL2/ 0.0, -8.0, , -4.0, , 0.0, , 4.0, , 8.0, ,
-15.0, -0075, , -0050, , -0075, , -0120, , -0120, ,
-10.0, -0040, , -0030, , -0050, , -0050, , -0085, ,
-5.0, -0015, , -0020, , -0025, , -0025, , -0060, ,
0.0, -0020, , -0010, , -0008, , -0008, , -0020, ,
5.0, -0070, , -0030, , -0025, , -0025, , -0050, ,
10.0, -0120, , -0045, , -0040, , -0040, , -0120, ,
15.0, -0175, , -0070, , -0070, , -0070, , -0175, ,
12*99999./

```

CCCCC

C. DCRSTA VS. AIRLON AND ADA (INCREMENT IN ROLLING MOMENT  
COEFFICIENT DUE TO ASYMMETRIC STABILATOR DEFLECTION AND  
PARAMETER ANGLE OF ATTACK)

```

DATA LTRL3/ 0.0, -8.0, , -4.0, , 0.0, , 4.0, , 8.0, ,
-15.0, -0087, , -0095, , -0100, , -0092, , -0084, ,
-10.0, -0060, , -0066, , -0068, , -0064, , -0058, ,
-5.0, -0030, , -0033, , -0034, , -0036, , -0030, ,
0.0, -0004, , -0004, , -0004, , -0003, , -0030, ,
5.0, -0012, , -0024, , -0030, , -0030, , -0020, ,
10.0, -0030, , -0058, , -0072, , -0046, , -0047, ,
15.0, -0050, , -0080, , -0092, , -0088, , -0067, ,
12*99999./

```

CCCCC

\*\* 2. DYNAMIC STABILITY DERIVATIVES

```

DATA CLADT ,CCADT ,CMADT ,
/2.00 ,0.10 , -10.0 , /,
CL2 ,CDC ,CMC , /,
/5.0 ,0.1 , -15.0 , /,
CFBDT ,CYR ,CNBT , /,

```

```

* * * * *
/0.0      ,0.4      ,0.15      /
CPR       ,CYP      ,CNR      /
/0.2      ,0.1      ,0.2      /
CPR       ,CYBDT    ,CNP      /
/-C.4     ,0.1      ,0.01     /

```

CCCCCCCC

```

*****
COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
*****

```

# \*\*\* CONTROL SYSTEM PARAMETERS

```

* * * * *
DATA      KPTCHR      ,KROLLR      ,KYAWRT      ,KBANK
* * * * *      /0.28      ,0.10      ,0.40      ,10.8
* * * * *      KGAMMA      ,KALT      ,CGARML      ,CGARMLN
* * * * *      /1.0      ,0.3      ,0.0      ,0.0
* * * * *      RRTLIM      ,KNY      ,KNZ      /
* * * * *      /75.0      ,0.35      ,0.05/

```

CCCCCCCC

```

*****
COMMON BLOCK /E/: INITIAL CONDITIONS
*****

```

# \*\*\* MISSILE INITIAL CONDITIONS

```

* * * * *
DATA      XM1      ,YM1      ,ALTUD1
* * * * *      /0.0      ,0.0      ,50.0
* * * * *
DATA      PITCH1      ,BANK1      ,HEDNG1
* * * * *      /3.00      ,0.0      ,0.0
* * * * *
DATA      AOA1      ,PTCHR1      ,ROLLR1
* * * * *      /3.00      ,0.0      ,0.0

```

C

C

CCCC

# \*\*\* TARGET INITIAL CONDITIONS

```

* * * * *
DATA      XT1      ,YT1      ,HT1
* * * * *      /24000.0      ,0.0      ,10.0

```

CCCC

```

*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****

```





```

** *
** *
** *
IXX      ,IYY      ,IZZ      ,IXZ      ,IA      ,IB      ,QS
ID        ,IE        ,IF        ,IG        ,IH      ,II      ,IK
CHORD2,CHORD ,SPAN2,SPAN ,NFAZE

```

CCCCC

```

*****
COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
*****

```

```

COMMON /C/ KPTCHR      ,KROLLR      ,KYAWRT      ,KBANK
KGAMMA      ,KALT      ,CGARML      ,CGARMLN
RRTLIM      ,PLIM      ,KNY      ,KNZ
AILLRN      ,STBLTR      ,RUCCER      ,
BSERO      ,NZSERO      ,NYSERO

```

CCCCC

```

*****
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
*****

```

```

COMMON /D/ ALFA      ,BETA      ,VT      ,HMDOT
U      ,V      ,W      ,
PHI      ,GAMMA      ,THETA      ,SY
CD      ,CY      ,CL      ,CR
CM      ,CN      ,P      ,Q      ,
R      ,ALFADT      ,BETADT      ,PDOT
QDOT      ,RDOT      ,NZ      ,ALTUDE
XM      ,YM      ,XMDCT      ,YMDCT

```

CCCCC

```

*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****

```

```

COMMON /F/ PH1      ,PH2      ,PH3      ,PH4
CFFSET      ,ALATT      ,SGDZPU      ,MISDST
LAMDAZ      ,LAMDEL      ,KNFAZ      ,KNFEL
NZC      ,PHIC      ,GAMMAC      ,PCCLIM
PC      ,QC      ,RC      ,RANGE
SIGAZ      ,SIGEL      ,SIGDAF      ,SIGDEF
SYT      ,THETAT      ,XT      ,YT
FT      ,NYC      ,PDP RNG

```

CCCCC

```

*****
COMMON BLOCK /G/: OUTPUT PARAMETERS
*****

```

```

COMMON /G/ AUA      ,SIDESL      ,BANK      ,FLTPHC
BANKC      ,PITCH      ,ROLLRT      ,RULKTC
PTCHRT      ,YAWRT      ,HEADNG      ,FLTPTH

```



```

C      C      EANK ANGLE HCLD (60 DEG)
      AYC      = 0.0
      PFIC      = 60.0/PI I
      NZC      = AZC/COS(PHI)
      GC TO 100
      PF2      = 1
19
C      C      C      COURSE HCLD ON OFFSET HEADING TO POPUP
C      C      C      ABDSCZ = ABS(CSGGAZ)
C      C      C      IF(AEDSDZ.GT.SGDZPU) GO TO 29
20
C      C      C      ALTITUDE HCLD
C      C      C      ALTC      = 50.0
C      C      C      ALTUDF      = KALT*(ALTC-ALTUDF)/VT
C      C      C      GAMMAC      = GAMMA
C      C      C      GAMMAF      = GAMMA
C      C      C      AZC      = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
      BANK ANGLE HCLD (0 DEG)
      AYC      = 0.0
      PFIC      = 0.0
      NZC      = AZC/COS(PHI)
      GC TO 100
      PF3      = 1
25
C      C      C      PULLUP TO ATTACK ALTITUDE
C      C      C      PROFCRTICUAL NAVIGATION IN AZIMUTH
C      C      C      IF(ALTUDE.GT.ALTAIT) GO TO 39
30
C      C      C      VERTICAL FLIGHT PATH ANGLE HCLD (8.5 DEG)
C      C      C      ALTC      = 0.0
C      C      C      GAMMAC      = 8.5/PI I
C      C      C      GAMMAF      = GAMMA
C      C      C      AZC      = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
      PROFCRTICUAL NAVIGATION IN AZIMUTH
      AYC      = LAMDZ*VT*SIGDAF/G
      NZC      = AZC*COS(PHI)+AYC*SIN(PHI)
      PFIC      = ATAN2(AYC,AZC)
      GC TO 100
      PF4      = 1
35

```

```

**      ATTACK
**      PROFCRTICNAL NAVIGATION IN AZIMUTH AND ELEVATION
**
40      ALTIC      = 0.0
      GAMMAC      = 0.0
      GAMMAF      = GAMMAA
      AYC          = LAMCAZ*VT*SIGDAF/G
      AZC          = LAMDEL*VT*SIGDEF/G+CCS(GAMMAF)
      NZC          = AZC*CCS(PHI)+AYC*SIN(PHI)
      NYC          = 0.0

      BANK ANGLE CCMMAND ROUTINE INSURES ROLL
      IN SHORTEST DIRECTION

      PHIC      = ATAN2(AYC,AZC)
      CELPHI    = PHIC-PHI
      CPHIAB    = ABS(CELPHI)
      IF(OPHIAB.LT.PI) GO TO 100
      IF(PHIC.GE.0.0) GC TO 90
      PHIC      = PHIC+2.0*PI
      GC TO 100
      PHIC      = PHIC-2.0*PI
      PHIC
100 CONTINUE
**
**      NZ COMMAND LIMITED TO -2 & +4 G'S
      NZC = LIMIT(-2.0,4.0,NZC)

      RETURN
      END

**      SUBROUTINE APILOT
**      LIMIT, FEALPL
**      MODELS THE INNER LCOP AUTOPILOT AND CONTROL MIXER. CALCULATES
      REQUIRES THE ELEVATOR, AILERON & RUDDER REQUIRED, MIXES THESE TO GET
      THE FIN STABILATOR COMMANDS, APPLIES THE FIN LIMITS OF +-15 DEG.
      AND ADJUSTS THE THREE CONTROL OUTPUTS TO ACCOUNT FOR THE LIMITS.
**
      IMPLICIT REAL(A-Z)
      INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NOUT,PCOUNT,NFAZE

```



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\*\*\*\*\*  
COMMON BLOCK /A/: MISCELLANEOUS CONSTANTS  
\*\*\*\*\*

COMMON /A/ TIME , FINITIM,DT , GPDT , NCUT , NPTS , CPA , PCOUNT,  
G , T , RHO , PI , PII , WT , S ,  
IXX , IYY , IZZ , IXZ , IA , IC ,  
ID , IE , IF , IG , IH , IJ , IK ,  
CHORD2,CHORD , SPAN2,SPAN , NFAZE

CCCCCCC

\*\*\*\*\*  
COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS  
\*\*\*\*\*

COMMON /C/ KPTCHR , KRCLLR , KYAWRT , KBANK ,  
KGAMMA , KALT , CGARML , CGARMN ,  
RRTLIM , PLIM , KNY , KNZ ,  
AILRON , STBLTR , RUDDER ,  
BSERO , NZSERO , NYSERO

CCCCCCC

\*\*\*\*\*  
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS  
\*\*\*\*\*

COMMON /C/ ALFA , BETA , VT , HMDOT ,  
U , V , W , THETA , SY ,  
PHI , GAMMA , CL , CR ,  
CD , CY , CN , P , Q ,  
CM , CN , ALFADT , BETADT , PDOT ,  
R , RDOT , NZ , ALTUDE ,  
QDOT , XM , YM , YMDCT

CCCCCCC

\*\*\*\*\*  
COMMON BLOCK /F/: GUIDANCE PARAMETERS  
\*\*\*\*\*

COMMON /F/ PH1 OFF SET , PH2 , PH3 , PH4 ,  
LAMDZ , LAMDAZ , SGDZPU , MI SDST ,  
NZC , LAMDEL , KNFEL , KNFEL ,  
PC , PHIC , GAMMAC , PCLIM ,  
SIGAZ , QC , RC , RANGE ,  
SYT , SIGEL , SIGDEF , YT ,

```

*          HT          ,NYC          ,POPRNG
C EXECUTABLE STMTS *****
C
C INNER LCCF AUTOPILOT
C
C NORMAL ACCELERATION COMMAND SYSTEM
C
C NZCLIM = LIMIT(-2.0,4.0,NZC)
C NZZ = NZ+CGARMN*CCOT/G
C ENZ = NZCLIM-NZZ
C ENZKNZ = ENZ*KNZ
C QC = ENZKNZ*DT
C NZSERI = QC-KPTCHR*C
C NZSEFC = REALPL(NZSERO,0.025,NZSERI,DT)
C
C ELE = -PII*NZSERO
C
C BANK ANGLE COMMAND SYSTEM
C
C EPHI = PHIC-PHI
C PC = KBANK*EPHI
C PCLIM = LIMIT(-PLIM,PLIM,PC)
C EP = PCLIM-P
C BSERI = EP*KROLLR
C BSERC = REALPL(BSERO,0.025,BSERI,DT)
C
C AIL = -PII*BSERO
C
C TURN COORDINATOR
C
C IF(PT4.EG.1) GO TO 30
C   NYC = 0.0
C   CONTINUE
C   NY = NY+CGARM*ROOT/G
C   ENY = NYC-NY
C   RC = ENY*KNY*DT
C   NYSEFI = RC-KYAWRT*R
C   NYSEFC = REALPL(NYSERO,0.025,NYSERI,DT)
C
C   RUD = -PII*NYSERC
C   CONTRCLS MIXER AND LIMITS
C
C   LSTABI = ELE-AIL
C   RSTABI = ELE+AIL
C   LSTAB = LIMIT(-15.0,15.0,LSTABI)

```



```

** ** ** ** **
** ** ** ** **
** ** ** **  TABLE1, SUPRES
** ** ** **  TABLE2, SUPRES
** ** ** **  TABLE LOOKUP ROUTINES (TABLE1,2) TO CONSTRUCT THE AERO-
** ** ** **  DYNAMIC COEFFICIENTS FOR THE MISSILE GIVEN THE CONTROL
** ** ** **  INPUTS, ANGLE OF ATTACK, SIDESLIP AND ANGULAR RATES P, Q, R, ADT, BDT.
** ** ** **  THE MISSILE ALLOCATES MOMENTS, FORCES, RATES, ANGLES AND RETURNED WITHIN
** ** ** **  THE COMMON BLOCKS. CUT-OFF-RANGE WARNINGS ARE SUPPRESSED AFTER
** ** ** **  20 CONSECUTIVE CALLS CUT OF RANGE.
** ** ** **  *****
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NQUT,PCOUNT,NFAZE

** ** ** **  *****
** ** ** **  COMMON BLOCK /A/: MISCELLANEOUS CONSTANTS
** ** ** **  *****
COMMON /A/ TIME , FINTIM,DT ,OPDT ,NQUT ,NPTS ,CPA ,PCOUNT,
* * * * *
* * * * *  G , TIVY ,RHO ,PII ,MASS ,WT ,S ,
* * * * *  ID , IY , IZZ , IXL , IA , IB , IC ,
* * * * *  CHORD2,CHORD ,SPAN2,SPAN ,NFAZE ,IH ,IJ ,IK ,
* * * * *

** ** ** **  *****
** ** ** **  COMMON BLOCK /B/: AERODYNAMIC COEFFICIENT TABLES
** ** ** **  *****
COMMON /B/ LFT1(2,36) ,LFT2(2,36) ,DRG1(2,36) ,DRG2(2,36) ,
* * * * *
* * * * *  DRG3(2,36) ,DRG4(2,36) ,PTCH1(2,36) ,PTCH2(2,36) ,
* * * * *  SID1(6,10) ,SID2(6,10) ,SIC3(6,10) ,DREL1(6,10) ,
* * * * *  DREC2(6,10) ,DREC3(6,10) ,LTR1(6,10) ,LTR2(6,10) ,
* * * * *  LTR3(6,10) ,CLADT ,CDACT ,CMADT ,
* * * * *  CLQ ,CDQ ,CMQ ,CRBDT ,CRBDT ,
* * * * *  CYR ,CNBDT ,CRP ,CRP ,CYECT ,CNP ,
* * * * *

** ** ** **  *****
** ** ** **  COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
** ** ** **  *****
COMMON /C/ KPTCHR ,KRGLLR ,KYAWRT ,KBANK ,
* * * * *
* * * * *  KGAMMA ,KALT ,CGARML ,CGARML ,
* * * * *  RRTLIM ,PLIM ,KNY ,KNZ ,
* * * * *

```

```

**
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
**
COMMON /C/ ALFA
      U
      PHI
      CD
      CM
      R
      QDOT
      XM
      BETA
      V
      GAMMA
      CY
      CN
      ALFADT
      RDOT
      YM
      VT
      W
      THETA
      CL
      P
      BETADT
      NZ
      XMDCT
      HMDOT
      SY
      CR
      Q
      PDOT
      ALTUDE
      YMDCT
**

SIDESL = PII*BETA
AOA = PII*ALFA
CLEAS = TABLE1(LFTI1,ACA)
DCLSTE = TABLE1(LFTI2,STBLTR)
CDBAS = TABLE1(DRGI1,CLBAS)
DCDSTE = TABLE1(DRGI2,STBLTR)
DCCSTA = TABLE1(DRGI3,AILRON)
DCCSTR = TABLE1(DRGI4,RUDDER)
CMBAS = TABLE1(PTCHI1,AOA)
DCMSTE = TABLE1(PTCHI2,STBLTR)
CYBAS = TABLE2(SIDI1,ACA,SIDESL)
CRBAS = TABLE2(SIDI2,ACA,SIDESL)
CNBAS = TABLE2(SIDI3,AOA,SIDESL)
DCYSTR = TABLE2(DRECI1,AOA,RUDDER)
DCNSTR = TABLE2(DRECI2,AOA,RUDDER)
DCRSTR = TABLE2(DRECI3,AOA,RUDDER)
DCYSTA = TABLE2(LTRL1,AOA,AILRCN)
DCNSTA = TABLE2(LTRL2,AOA,AILRCN)
DCRSTA = TABLE2(LTRL3,AOA,AILRCN)
AERCDYNAMIC COEFFICIENTS
CL = CLEAS+DCLSTE+CHORD2*(CLADT*ALFADT+CLQ*Q)/VT
CD = CCEAS+DCCDSTE+CCDSTA+DCCDSTR+CHORD2*(CYR*P+CYBDT*BETADT)/VT
CY = CCEAS+CCYSTA+CCYSTA+SPAN2*(CMADT*ALFADT+CMQ*Q)/VT
CM = CMEAS+DCMSTE+CHORD2*(CNBDT*BETADT+CNRR*P+CNPP)/VT
CN = CNEAS+DCNSTA+CCNSTA+SPAN2*(CRBDT*BETADT+CRKR*P+CKP)/VT

```



```

C C C C C
AERODYNAMIC FORCES AND MOMENTS
L = CL*CS
D = CD*CS
LA = SPAN*CR*QS
MA = CFCRD*CM*QS
NA = SPAN*CN*QS
X = L*SIN(ALFA)-D*COS(ALFA)
Y = CY*QS
Z = -L*CCS(ALFA)-D*SIN(ALFA)

C C C
NORMAL & LATERAL ACCELERATIONS
NZ = -Z/(MASS*G)
NY = Y/(MASS*G)

C C C C C
** COMMENCE INTEGRATION OF EQUATIONS OF MOTION
EULER ANGLES
PHIDOT = P+TAN(THETA)*(Q*SIN(PHI)+R*COS(PHI))
THETAD = G*COS(PHI)-R*SIN(PHI)
SYDDOT = (Q*SIN(PHI)+R*COS(PHI))/COS(THETA)
PHI = PHI + PHIDOT*DT
THETA = THETA + THETAD*DT
SY = SY + SYDDOT*DT

C C C
LINEAR ACCELERATIONS AND VELOCITIES
UDOT = -G*SIN(THETA)+V*R-W*Q+X/MASS+T/MASS
VDDOT = G*SIN(PHI)*COS(THETA)-U*R+W*P+Y/MASS
WDDOT = G*CCS(PHI)*COS(THETA)+U*Q-V*P+Z/MASS
U = U + UDDOT*DT
V = V + VDDOT*DT
W = W + WDDOT*DT
VT = SQRT(U**2+V**2+W**2)
VTDOT = SQRT(UDOT**2+VDDOT**2+WDDOT**2)

C C C
ANGULAR ACCELERATIONS AND VELOCITIES
PDCT = IE*LA+IC*NA-ID*P*Q-IE*R*Q
QDDOT = IF*MA-IG*P*R-IH*(P**2-R**2)
RDDOT = IC*LA+II*NA-IJ*P*Q-IK*R*Q
P = P + PDCT*DT
Q = Q + QDDOT*DT

```



```

C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,101) IP, TABLE1
C      RETURN
C      END IF
C
10 DO 90 I=1,30
    IF(.NOT.ARRAY(1,I).EQ.9999.0) GO TC 20
    TABLE1=ARRAY(2,I-1)
    IF(SUPRES(J,K,N).EQ.1) WRITE(6,102) IP, TABLE1
    RETURN
20  IF(.NOT.IP.GT.ARRAY(1,I)) GC TC 30
    GC TO 90
30  IF(.NOT.IP.EQ.ARRAY(1,I)) GO TC 40
    TABLE1 = ARKAY(2,I)
    RETURN
40  IF(.NOT.IP.LT.ARRAY(1,I)) GO TC 90
    C= (IP-ARRAY(1,I-1))/(ARRAY(1,I)-ARRAY(2,I-1))
    TABLE1= ARRAY(2,I-1) +C*(ARRAY(2,I)-ARRAY(2,I-1))
    RETURN
C      END IF
C      9C CONTINUE
C      WRITE(6,103)
C      RETURN
C
C      FORMAT STATEMENTS FOR SUBROUTINE TABLE1*****
101  FORMAT('0','SUBROUTINE TABLE1: INPUT BELOW INDEPENDENT VARIABLE DA
    *TA.//',
    *      USED LOWEST DATA AVAILABLE = ',F10.2,
102  FORMAT('0','SUBROUTINE TABLE1: INPUT ABOVE INDEPENDENT VARIABLE DA
    *TA.//',
    *      USED HIGHEST DATA AVAILABLE = ',F10.2,
103  FORMAT('0','SUBROUTINE TABLE1: ERROR. SUBROUTINE DID NOT END.')
C      END
C
C      9-07-84
C      *****
C      FUNCTION TABLE2 (A,IP,IV)
C      *****
C      TABLE LCKUP WITH LINEAR INTERPOLATION FOR A FUNCTION
C      OF TWO VARIABLES, Z=F(X,Y). MAXIMUM NUMBER OF INPUT PARAMETERS IS
C      LIMITED TO 5. INDEPENDENT VARIABLE DATA POINTS TO 9 BY THE VALUES
C      DIMENSION OF THE ARRAY. A(1,I) IS ACT USED. THE PARAMETER VALUES
C      ARE STORED IN COL 1, INDEP. VAR. VALUES IN ROW 1. THE COEFFICIENT
C      TABLE2 ARE STORED IN THE GRID CREATED BY ROW AND COL 1.
C      *****
C      MAKE SURE STORING ARE SUPPRESSED AFTER 5 CONSECUTIVE OCCURRENCES.
C      *****

```

```

C      REAL A(6,10), IP, IV, CP, CV, LFT, RGT, TABLE2
C      INTEGER I, LI, UI, J, K, N, SUPRES
C      DATA J, K, N /3*0/

C      K = K+1
C      IF(.NOT. IP.LT. A(2,1)) GO TO 10
C      CP = 0.
C      LI = 2
C      UI = 2
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1001) IP, A(2,1)
C      GO TO 55

C      10  DC 50 I=2,6
C           IF(.NOT. A(I,1).EQ.9999.0) GO TO 20
C           IF(SUPRES(J,K,N).EQ.1) WRITE(6,1002) IP, A(I-1,1)
C           CP = 0.
C           LI = I-1
C           UI = I-1
C           GO TO 55

C      20  IF(IP-A(I,1)) 30,40,50
C      30  IP < A(I,1)
C           CP = (IP-A(I-1,1))/(A(I,1)-A(I-1,1))
C           LI = I-1
C           UI = I
C           GO TO 55

C      40  IF = A(I,1)
C           CP = 0
C           LI = I
C           UI = I
C           GO TO 55

C      50  END IF
C      CCNTINUE
C      END IF

C      55 IF(.NOT. IV.LT. A(1,2)) GO TO 60
C           IF(SUPRES(J,K,N).EQ.1) WRITE(6,1003) IV, A(1,2)
C           TABLE2=A(LI,2)+CP*(A(UI,2)-A(LI,2))
C           RETURN

C      60  DC 100 I=2,10
C           IF(.NOT. A(1,I).EQ.9999.0) GO TO 70
C           IF(SUPRES(J,K,N).EQ.1) WRITE(6,1004) IV, A(1,I-1)
C           TABLE2=A(LI,I-1)+CP*(A(UI,I-1)-A(LI,I-1))
C           RETURN

```

```

7C      IF(IV-A(1,I)) 80,90,100
C      IV < A(1,I)
80      CV = (IV-A(1,I-1))/(A(1,I)-A(1,I-1))
      LFT = A(1,I-1)+CP*(A(1,I)-A(1,I-1))
      RGT = A(1,I)+CP*(A(1,I)-A(1,I-1))
      TABLE2 = LFT+CV*(RGT-LFT)
      RETURN
C      IV = A(1,I)
90      TABLE2 = A(1,I)+CP*(A(1,I)-A(1,I))
      RETURN
C      IF
100      END IF
      CCNTINCE
C      WRITE(6,1005)
C      RETURN
C      FORMAT STATEMENTS FOR SUBROUTINE TABLE2 *****
1001  FORMAT('0','SUBROUTINE TABLE2: INPUT PARAMETER BELOW DATA.',
*      'INPUT PARAMETER =',F10.2,
*      'USED LOWEST PARAMETER =',F10.2)
1002  FORMAT('0','SUBROUTINE TABLE2: INPUT PARAMETER ABOVE DATA.',
*      'INPUT PARAMETER =',F10.2,
*      'USED HIGHEST PARAMETER =',F10.2)
1003  FORMAT('0','SUBROUTINE TABLE2: INPUT INDEP. VAR. BELOW DATA.',
*      'INPUT INDEP. VAR. =',F10.2,
*      'USED LOWEST INDEP. VAR. =',F10.2)
1004  FORMAT('0','SUBROUTINE TABLE2: INPUT INDEP. VAR. ABOVE DATA.',
*      'INPUT INDEP. VAR. =',F10.2,
*      'USED HIGHEST INDEP. VAR. =',F10.2)
1005  FORMAT('0','SUBROUTINE TABLE2: ERROR. SUBROUTINE DID NOT END.')
      END
C
C
C ***** 9-05-84 *****
C ***** FUNCTION SUPRES(J,K,N) *****
C ***** DETERMINES TO SUPPRESS WARNINGS FROM TABLE1 OR TABLE2 AFTER THEY *****
C ***** HAVE BEEN CALLED ABOUT 20 TIMES IN A ROW. (ABOUT 5 DT INTERVALS.) *****
C ***** INTEGER J,K,N, SUPRES *****
C      IF(K-J.EG.1)GO TO 10
      N = 0
      K = 0
      J = 0
      GC TO 15

```



```

10 CONTINUE
15 CONTINUE
105 IF(N.EC.20)WRITE(6,105)
105 FORMAT('0','TABLE LCKUP WARNINGS SUPPRESSED')
105 IF(N.GE.20) SUPRES = 1
105 IF(N.LT.20) SUPRES = 0
105 RETURN
105 END
105 SUBROUTINE TGTNAV
105 RNG, SCV
105 NAVIGATES THE TARGET AND COMPUTES RELATIVE RANGE, RANGE RATES.
105 INCCRPCRTS ECM AND GLINT MODELS TO GIVE APPARENT TARGET
105 POSITIONS. ALSO CALCULATES LINE OF SIGHT ANGLES AND RATES.
105 IMPLICIT REAL(A-Z)
105 INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CFA,NOUT,PCOUNT,NFAZE
105 COMMON /A/ TIME , FINTIM,DT , CPDT ,NCLT ,NPTS ,CPA ,PCOUNT,
105 G , IXX , IYY , RHO , PI ,PII ,MASS ,WT ,S ,
105 ID , IZZ , IFZ , IA , IH , IB , IC ,GS ,
105 CHORD2,CHORD ,SPAN2 ,SPAN ,IH ,IJ ,IK ,
105 COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
105 BETA ,VT ,HMDOT ,
105 V ,W ,SY ,
105 GAMMA ,THETA ,CR ,
105 CY ,CL ,Q ,
105 CN ,P ,
105 COMMON /D/ ALFA ,
105 U ,PHI ,
105 CD ,CM ,
105

```

```

* * *
R      QUOT      XM      ,ALFADT      ,BETADT      ,PDOT      ,
      ,RDOT      ,YM      ,NZ      ,ALTUDE      ,
      ,YM      ,XMDCT      ,YMDOT      ,

```

CCCCC

```

*****
COMMON BLOCK /E/: INITIAL CONDITIONS
*****

```

```

COMMON /E/  XM1  PITCH1  ,YMI      ,ALTUDI      ,UI      ,
      ,AOA1      ,BANK1      ,HEDNGI      ,SI DESI      ,
      ,XTI      ,PITCHR1      ,KOLLRI      ,YAWRI      ,
      ,XTI      ,YTI      ,HTI      ,TSPEED      ,

```

CCCCC

```

*****
COMMON ELCK /F/: GUIDANCE PARAMETERS
*****

```

```

COMMON /F/  PH1  CFFSET      ,PH2      ,PH3      ,PH4      ,
      ,LAMDAZ      ,ALTATT      ,SGCZPU      ,MISDST      ,
      ,NZC      ,LAMDEL      ,KNFAZ      ,KNFEL      ,
      ,PC      ,PHIC      ,GAMMAC      ,PCFLIM      ,
      ,SIGAZ      ,QC      ,RC      ,RANGE      ,
      ,SYT      ,SIGEL      ,SIGDAF      ,SIGDEF      ,
      ,FT      ,THETAT      ,XT      ,YT      ,

```

CCCCC

```

*****
COMMON ELCK /H/: ECM/GLINT PARAMETERS
*****

```

```

COMMON /H/  FREQ      ,SHIFTY      ,SHIFTH      ,BRNTHR      ,
      ,XECM      ,VECM      ,HECM      ,XGLNT      ,
      ,YGLNT      ,HGLNT      ,XTECM      ,YTECM      ,

```

CCCCC

EXECUTABLE STATEMENTS:

\*\*\* TARGET ACTION

```

XI = XI1
YT = YT1+TSPEED*TIME
HT = HT1

```

RELATIVE RANGE TO TARGET

CC



```

105 CONTINUE
C
  POPRNG = PHASE*PII
  IF (RANGE.LT.BRNTHR) GO TO 350
  XECMW = SIN(2*PI*FREQ*TIME+PHASE)
  XECM = SQWV(XECMW,SHIFTX)
C
  YECMW = SIN(2*PI*FREQ*TIME+PHASE)
  YECM = SQWV(YECMW,SHIFTY)
C
  HECMW = SIN(2*PI*FREQ*TIME+PHASE)
  HECM = SQWV(HECMW,SHIFTH)
  GC TO 400
350 CONTINUE
  XECM = 0.0
  YECM = 0.0
  HECM = 0.0
400 CONTINUE
C
  XTECM = XI+XECM+XGLNT
  YTECM = YT+YECM+YGLNT
  HTECM = HT+HECM+HGLNT
C
  *** RELATIVE RANGE AND RANGE RATE TO RADAR TARGET
C
  XRECM = XTECM-XM
  YRECM = YTECM-YM
  HRECM = HTECM-ALTUCE
  RNRECM = SQRT(XRECM**2+YRECM**2)
  RGECMT = SQRT(XRECM**2+YRECM**2+HRECM**2)
C
  XDCTR = -XMDOT
  YDCTR = TSPEED-YMCDOT
  HDCTR = -HMDOT
  HORDTR = SQRT(XDCTR**2+YDCTR**2)
C
  *** SEEKER LCS AND LCS RATE CALCULATIONS
C
  SYT = ATAN2(YRECM,XRECM)
  TRAKAZ = ATAN2(YMDCT,XMDOT)
  SIGAZ = SYT-TRAKAZ
C
  VTANAZ = -XDCTR*SIN(SYT)+YDCTR*CGS(SYT)
  SIGLAZ = VTANAZ/RNGECM
  SIGDAF = REALPL(SIGDAF,KNFAZ,SIGDAZ,DT)
C

```

```

C      THETAT = ATAN2 (HRECM, RNGECHM)
C      HURDOT = SQRT (XMDOIT**2 + YMDOT**2)
C      TRAKEL = ATAN2 (HMDCT, HCRDOT)
C      SIGEL  = THETAT - TRAKEL
C
C      VTANEL = HDOTR * COS (THETAT) + HORDTR * SIN (THETAT)
C      SIGDEL = VTANEL / RGECHM
C      SIGDEF = REALPL (SIGDEF, KNFEL, SIGDEL, DT)
C
C      RETURN
C      END
C
C      8-01-84
C      SUBROUTINE RNG (RAND)
C      ***
C      *** GENERATES A RANDOM NUMBER BETWEEN -1.0 & 1.0
C      ***
C      ***
C      IMPLICIT REAL (A-Z)
C      DATA SEED / 4.0 /
C
C      RAND = (SEED + 3.14159) ** 5.04
C      RAND = (RAND - IFIX (RAND) - 0.5) * 2.0
C      SEED = RAND
C
C      RETURN
C      END
C
C      9-07-84
C      FUNCTION SQWV (WAVE, AMPL)
C      ***
C      *** GENERATES A SQUAREWAVE FROM A SINWAVE
C      ***
C      IMPLICIT REAL (A-Z)
C
C      IF (WAVE .GT. 0.0) SQWV = AMPL
C      IF (WAVE .LT. 0.0) SQWV = -AMPL
C      IF (WAVE .EQ. 0.0) SQWV = 0.0
C
C      RETURN
C      END
C
C      8-20-84

```





```

C      * * *      SIGAZ      ,SIGDAF      ,SIGDEF      ,
      * * *      SYT        ,XT        ,YT        ,
      * * *      HT        ,POPRNG      ,
C      COMMON /G/  AOA      ,BANK      ,FLTPHC      ,
      * * *      BANC      ,ROLLRT      ,ROLKTC      ,
      * * *      PTC      ,HEACNG      ,FLTPTH      ,
      * * *      HEDT      ,DSIGAZ      ,DSIGEL      ,
      * * *      DSGDAZ      ,ERFBK      ,ERFRR      ,
      * * *      ERF      ,
C      COMMON /H/  FREQ      ,SHIFTH      ,BRNTHR      ,
      * * *      XECM      ,HECM      ,XGLNT      ,
      * * *      YGLNT      ,XTECM      ,YTECM      ,
      * * *      HTECM      ,
C      COMMON /I/  PTS(300,20),PLTN(6,7),XN(6,7),YN(6,7),TITLE(6),
      *      LEG(4,20)
C      EXECUTABLE STMTS *****
C      RACIAN TO DEGREE CONVERSIONS FOR OUTPUT
C      AOA      = ALFA*PI I
C      SIDESL    = BETA*PI I
C      BANK      = PHI*PI I
C      FLTPHC    = GAMMAC*PI I
C      BANC      = PHIC*PI I
C      PITCH     = THETA*PI I
C      ROLLRT    = P*PI I
C      ROLKTC    = PCLIM*PI I
C      PTC      = Q*PI I
C      YAWRT     = R*PI I
C      HEADNG    = SY*PI I
C      FLTPTH    = GAMMA*PI I
C      HEDT      = SYT*PI I
C      ELEVT     = THETA*PI I
C      DSIGAZ    = SIGAZ*PI I
C      DSIGEL    = SIGEL*PI I
C      DSGCAZ    = SIGDAF*PI I
C      DSGDEL    = SIGDEF*PI I
C      * * *      CREATE THE MISSION PHASE MARKER (MARK)
C      MARK = C.0
C      IF (PH1.EQ.1)MARK = 1.0
C      IF (PH2.EQ.1)MARK = 2.0

```

```

C      IF (PH3.EQ.1)MARK = 3.0
C      IF (PH4.EQ.1)MARK = 4.0
C      NPTS = NPTS+1
C      K = NPTS+2
C      *** COMPUTE THE ERROR FUNCTIONS
C      IF (MARK.EQ.4) GO TC 50
C      ERRBK = 0.0
C      ERRRR = 0.0
C      ERRRAZ = 0.0
C      ERREL = 0.0
C      GC TC 100
C      50 CONTINUE
C      ERRBK = ERRBK + ABS(BANKC-BANK) *DT
C      ERRRR = ERRRR + ABS(RCLRTC-ROLLRT) *DT
C      ERRRAZ = ERRRAZ + ABS(DSGDAZ) *DT
C      ERREL = ERREL + ABS(DSGDEL) *DT
C      100 CONTINUE
C      ERFBK = ERFBK/TIME
C      ERRFR = ERRRR/TIME
C      ERFAZ = ERRRAZ/TIME
C      ERFEL = ERREL/TIME
C      *** SELECT THE VARIABLES TO BE STORED
C      KEEP(1) = TIME
C      GRAPH 1
C      KEEP(2) = NZC
C      KEEP(3) = NZ
C      GRAPH 2
C      KEEP(4) = EANKC
C      KEEP(5) = BANK
C      GRAPH 3
C      KEEP(6) = ROLRTC
C      KEEP(7) = ROLLRT
C      GRAPH 4
C      KEEP(8) = YECM
C      KEEP(9) = YGLNT
C      GRAPH 5
C      KEEP(10) = AILRON

```

```

KEEP(11) = STBLR
KEEP(12) = RUDDER

GRAPH 6
KEEP(13) = ALTUDE

GRAPH 7
KEEP(14) = XM
KEEP(15) = YM
KEEP(16) = XT
KEEP(17) = YT

SPARES
KEEP(18) = RANGE
KEEP(19) = MARK
KEEP(20) = NYC

*** STORE MINIMUM AND MAXIMUM VALUES OF EACH VARIABLE
DO 20 I=1,20
  IF (NPPTS.GT.1) GO TO 10
  PTS(1,I) = KEEP(1)
  PTS(2,I) = KEEP(1)
  10  CONTINUE
  PTS(1,I) = AMIN1(PTS(1,I),KEEP(I))
  PTS(2,I) = AMAX1(PTS(2,I),KEEP(I))
  20 CONTINUE
*** STORE VALUES OF EACH VARIABLE WITH THE TIME
DO 30 I=1,20
  PTS(K,I) = KEEP(I)
  30 CONTINUE
*** CHECK FOR ARRAY OVERFLOW AND TERMINATE AT 255 POINTS
  IF (NPPTS.GE.295) CPA = 3.0

RETURN
END

```

```

*** **
*** ** SUBROUTINE CUTPUT(NPTS,CPA)
*** **
*** ** HEADER, PLOT1, PLOT2, PLOT21, PLOT3
*** **
*** **
9-07-84
*** **

```





ARE THE NUMBERS (BETWEEN 1 AND 20) CF THE DEPENDENT  
VARIABLES TO BE PLOTTED AGAINST TIME.

DATA	NEV	/	0	2	3	2C	0
*				2	3	0	
*			0	4	5	0	
*			0	6	7	0	
*			0	8	9	0	
*			0	10	11	0	
*			0	13	0	0	
*			0	0	0	0	

\*\* LOAD THE MESSAGES AND VARIABLES TO APPEAR IN THE UPPER  
LEFT HAND CORNER OF EACH GRAPH.

DATA MESS1 /:FREQ = '//  
DATA MESS2 /:PHASE = '//

EXECUTABLE STMTS:

VAR1 = FREQ  
VAR2 = PUPRNG

\*\*\*\*\* READ TITLE CAPTIONS FOR GRAPHS AND PRINTOUT \*\*\*\*\*  
\*\*\*\*\* FROM FILE NO.2: LABELS DATA \*\*\*\*\*

IF (FLAG.EQ.1.0) GO TO 18

\*\* READ IN CVERALL TITLE LINES (4 LINES OF 32 CHARACTERS)

5 READ(2,5)((TITLE(J,I),J=1,8),I=1,4)  
FORMAT(20X,8A4)

\*\* READ IN EACH GRAPH TITLE & ITS AXIS LABELS (24 CHARACTERS EACH)

DO 10 J=1,7  
READ(2,12)(PLTN(I,J),I=1,6)  
READ(2,12)(XN(I,J),I=1,6)  
READ(2,12)(YN(I,J),I=1,6)

10 CONTINUE  
12 FORMAT(20X,6A4)

\*\* READ IN THE LEGEND LABEL FOR EACH OF THE 20 STORED VARIABLES  
(16 CHARACTERS EACH)

15 READ(2,15)((LEG(I,J),I=1,4),J=1,20)  
FORMAT(20X,4A4)

```

C      FLAG = 1.0
C      CONTINUE
C
C      ***** WRITE PRIMARY DATA OUTPUT *****
C      ***** TO FILE 6 (TERMINAL) AND THEN FILE 9 (TCMC DATA) *****
C
C      DO 100 K=1,2
C      IF(K.EQ.1)KFILE=6
C      IF(K.EQ.2)KFILE=9
C
C      ***** TITLES *****
C
C      20      WRITE(KFILE,20)((TITLE(I,J),I=1,8),J=1,4)
C      FORMAT('1',4(20X,8A4//))
C
C      ***** INDICATE HOW THE SIMULATION TERMINATED *****
C
C      GC TC(30,40,50),CPA
C
C      30      WRITE(KFILE,35)
C      35      FORMAT(1X,'SIMULATION TERMINATED DUE TO CPA')
C      GC TO 60
C
C      40      WRITE(KFILE,45)
C      45      FORMAT(1X,'SIMULATION TERMINATED DUE TO FINTIME')
C      GC TO 60
C
C      50      WRITE(KFILE,55)
C      55      FORMAT(1X,'SIMULATION TERMINATED DUE TO FULL ARRAY')
C
C      60      CONTINUE
C
C      ***** VALUE OF THE ITERATED PARAMETER *****
C
C      65      WRITE(KFILE,65) FREQ
C      65      FORMAT(1X,'*** BLINKER FREQUENCY= ',F8.2)
C
C      67      WRITE(KFILE,67) PCPRNG
C      67      FORMAT(1X,'*** BLINKER PHASE = ',F6.0//)
C
C      ***** LIST THE PRIMARY DATA OUTPUTS *****
C
C      75      WRITE(KFILE,75) MISDST,ERFBK,ERFR,R,ERFAZ,ERFEL
C      75      FORMAT(1X,'MISS ***** / ***** ERROR FUNC
***** DISTANCE ***** BANK *****')

```

```

* ROLL RATE * AZIMUTH * ELEVATION *'//
* 5(3X,F10.5,2X,'*')//)
C C C
** LIST THE VARIABLE RANGES
C
80 WRITE(KFILE,80)
FCFMAT(18X,'***** RANGES FOR ALL SAVED VARIABLES *****'
//30X,' MINIMUM
WRITE(KFILE,90)((LEG(I,J),I=1,4),PTS(1,J),PTS(2,J)),J=1,20)
FCFMAT(11X,4A4,4X,F12.6,3X,F12.6)
C 100 CONTINUE
C C C
***** TABULAR DATA OUTPUT *****
C C C
DO 200 I=1,4
J=(I-1)*4+2
K=J+3
WRITE(9,20)((TITLE(L,M),L=1,8),M=1,4)
WRITE(9,65) FREQ
WRITE(9,125) I
FCFMAT(50X,' DATA SET NUMBER ',I1,' [F 4'//)
WRITE(9,135)((LEG(L,1),L=1,4),((LEG(L,M),L=1,4),M=J,K)
FCFMAT(2X,20A4//)
C
NN=NPTS+2
DC 150 N=3,NN
START NEW PAGE EVERY 65 LINES
L=MOD(N,65)
IF(L.NE.0) GC TO 140
WRITE(9,20)((TITLE(L,M),L=1,8),M=1,4)
WRITE(9,65) FREQ
WRITE(9,125) I
WRITE(9,135)((LEG(L,1),L=1,4),M=J,K)
((LEG(L,M),L=1,4),M=J,K)
*
140 CONTINUE
WRITE(9,145) PTS(N,1),(PTS(N,L),L=J,K)
145 FCFMAT(1X,5('*,F12.6,3X))
150 GCNTINCE
200 CONTINUE
C C C C C
***** PRODUCE GRAPHIC OUTPUT USING DISPLA SUEROUTINES *****

```



```

DO 50 J=1,3
DC 30 I=1,8
      HC(I) = TITLE(I,J)
30  CONTINUE
      CALL HEADIN(HC ,32 , 1.1 ,4)
50  CONTINUE
DO 60 I=1,6
      HC(I) = PLTN(I,KP)
      XNM(I) = XN(I,KP)
      YNM(I) = YN(I,KP)
60  CONTINUE
      CALL HEADIN(HD ,24 , 1.0 ,4)
      CALL XNAME( XNM ,24)
      CALL YNAME( YNM ,24)
      RETURN
ENC
*** FILE: FLCT1 ***
*** CONTAINS ALL S/R'S THAT INTERFACE WITH CISSPLA EXCEPT HEADER ***
***
*** SUBROUTINE PLOT1(MESS1,MESS2,VARI,VAR2) ***
*** INITIALIZES DISSPLA FOR A NEW PAGE AND GRAPH ***
***
*** IMPLICIT REAL(A-H,C-Z),INTEGER(I-N) ***
*** DIMENSION MESS1(2),MESS2(2) ***
***
*** CALL NCCHEK ***
*** CALL GRACE(0.,647) ***
*** CALL BLCWUP(0.,8.5) ***
*** CALL PAGE(1.,8.5) ***
*** CALL HWRQT('AUTO') ***
*** CALL HWRCAL('SCREEN') ***
*** CALL NCERDR ***
*** CALL PFYSOR(1.,.75) ***
*** CALL AREA2C(9.,6.5) ***
*** CALL SWISSM ***
***
*** PUT THE MESSAGES INTO THE GRAPHS ***
*** CALL MESSAGE(MESS1,8,0.2,0.0) ***

```



```

C      CALL REALNC(VAR1,2,'ABUT','ABUT')
C      CALL MESSAG(MESS2,8,0.2,5.6)
C      CALL REALNC(VAR2,0,'ABUT','ABUT')
C      CALL BLFEC(0.1,5.5,1.8,0.8,0.01)

C      RETURN
C      END
C
C      *****8-26-84*****
C      *****SUBROUTINE PLOT2(PTS,LEG,DV,IV,NPTS)*****
C      *****LOADS THE LEGEND ARRAY WITH CURVE LABELS; GETS THE POINTS FOR*****
C      *****EACH CURVE FROM THE PTS ARRAY; PLOTS EACH CURVE. IV,DV ARE IN-*****
C      *****DEPENDENT, DEPENDENT VARIABLE INDEXES. THEY GIVE THE COLUMN IN*****
C      *****THE PTS ARRAY WHERE THEIR VALUES ARE FOUND. LEG IS THE PACKED*****
C      *****ARRAY CCNTAINING THE LABELS FOR EACH VAR. S. *****
C      *****ELEMENT ARRAY CCNTAINING THE INDEXES FCR UP TO 4 DEP VAR. S. *****
C      *****
C      IMPLICIT REAL (A-H,C-Z), INTEGER(1-N)
C      INTEGER DV(4),IPACK(100),LEG(4,20),LBL(5)
C      DIMENSION PTS(300,20),XP(300),YP(300)
C
C      DATA MCNEY /'$/
C
C      *****FIRST FIND OUT HOW MANY CURVES THERE ARE*****
C
C      I=1
C      5 IF (DV(I).EQ.0)GO TO 10
C      MCNV = I
C      IF (I.EQ.4)GO TO 10
C      I = I+1
C      GO TO 5
C      1C CONTINUE
C
C      *****NEXT PACK THE LEGEND ARRAY AND RANGE THE Y-AXIS*****
C
C      DO 30 I=1,MCNV
C      K = DV(I)
C      IF (I.GT.1) GO TO 15
C      YMIN = PTS(1,K)
C      YMAX = PTS(2,K)
C      GO TO 20
C      30 CONTINUE
C      YMIN = AMIN1(YMIN,PTS(1,K))
C      YMAX = AMAX1(YMAX,PTS(2,K))
C      15

```

```

C      20      CCNTINUE
C      DC 25 J=1,4
C      LBL(J) = LEG(J,K)
C      25      CCNTINUE
C      LBL(5) = MONEY
C      CALL LINES(LBL,IPACK,I)
C      30      CONTINUE
C      *** RANGE THE INDEPENDENT VARIABLE(S)
C      XMIN = PTS(1,IV)
C      XMAX = PTS(2,IV)
C      *** NOW PLOT THE CURVES
C      CALL GRAF(XMIN,SCALE,XMAX,YMIN,SCALE,YMAX)
C      DO 90 I=1,MCRV
C      DC 80 J=1,NPTS
C      XP(J) = PTS(J+2,IV)
C      YP(J) = PTS(J+2,DV(I))
C      80      CCNTINUE
C      CALL CURVE(XP,YP,NPTS,1)
C      90      CONTINUE
C      PLOT THE GRID & LEGEND AND FINISH THE GRAPH
C      CALL PLCT21(IPACK,MCRV)
C      RETURN
C      END
C      7-25-84
C      *** SUBROUTINE PLOT21(IPACK,MCRV)
C      *** PLOTS THE LEGEND & THE GRID AND ENDS THIS GRAPH
C      ***
C      IMPLICIT INTEGER(I-N)
C      DIMENSION IPACK(100)
C      XW=XLEGND(IPACK,MCRV)
C      YW=YLEGND(IPACK,MCRV)
C      CALL LEGEND(IPACK,MCRV,0.5,0.5)
C      CALL BLFEC(0.4,0.4,0.4,XW+0.2,YW+0.2,.01)
C      CALL DC1

```









# APPENDIX E

## LISTING FOR SUBROUTINE MISSN1

```

**          **          **          **          **          **          **          **          **          **
** SUBROUTINE MISSN1                                     9-07-84
**          **          **          **          **          **          **          **          **          **
** SEA SKIMMER GUIDANCE SCHEME. ALLOWS VARIABLE POPUP IN CLOSE
** WITH NC CFFSET TURN. AFTER POPUP, GUIDANCE IS STANDARD PRO-
** PORTIONAL. POPUP USES ONLY ALTITUDE COMMAND VICE GAMMAC.
**
** MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES
** OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT
** CONTRCL LOOPS. NYC IS ASSUMED TO ALWAYS BE ZERO. NZC IS LIMITED
** TO +4.C AND -2.0 G'S.
**
** IMPLICIT REAL(A-Z)
** INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCOUNT,NFAZE
**
** COMMON ELCK /A/: MISCELLANEOUS CONSTANTS
**
** COMMON /A/ TIME , FINTIM,DT ,CPDT ,NCLT ,NPTS ,CPA ,PCOUNT,
**          G ,T ,RHO ,PI ,PII ,MASS ,WT ,S ,
**          IXX ,IYY ,IZZ ,IXZ ,IA ,IB ,US ,
**          ID ,IE ,IF ,IG ,IH ,IJ ,IK ,
**          CHORD2,CHORD ,SPAN2,SPAN ,NFAZE
**
**
** COMMON BLCK /C/: CCNTROL SYSTEM PARAMETERS
**
** COMMON /C/ KPTCHR ,KRCLLR ,KYAWRT ,KBANK ,
**          KGAMMA ,KALT ,CGARML ,CGARMIN ,
**          RRTLLIM ,PLIM ,KNY ,KNZ ,
**          AILRON ,STBLTR ,RUDDER ,
**          BSERO ,NZSEKO
**
** COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS

```











## LISTING FOR SUBROUTINE MISSN2

```

9-07-84
*****
SUBROUTINE MISSSN2
*****
BALLISTIC GUIDANCE SCHEME. ALLOWS VARIABLE POPUP IN CLOSE
WITH NC OFFSET TURN. AFTER POPUP, MISSILE RCLLS TO 90 DEGREES
ANGLE CF BANK AND USES LATERAL AND VERTICAL PROPORTIONAL NAV.
*****
MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES
OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT
CONTRCL LGOPS. NYC IS ASSUMED TO ALWAYS BE ZERO. NZC IS LIMITED
TO +4.0 AND -2.0 G'S.
*****
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NOUT,PCOUNT,NFAZE
*****
COMMON /A/ TIME , FINTIM,DT , CPDT , NCUT , NPTS , CPA ,PCOUNT,
* * * * * G , T , RHO , PI ,PII ,MASS ,WT ,S ,
* * * * * IXX , IY , IZZ , IXZ , IA , IB , IC ,CS ,
* * * * * ID , IE , IF , IG , IH , II , IJ , IK ,
* * * * * CHORD2, CHORD , SPAN2, SPAN , NFAZE
*****
COMMON /C/ KPTCHR , KROLLR , KYAWRT , KBANK ,
* * * * * KGAMMA , KALT , CGARML , CGARMN ,
* * * * * RRT LIM , PLIM , KNY , KNZ ,
* * * * * AIRLON , STBLTR , RUCCER ,
* * * * * BSERO , NZSERO , NYSERO
*****
COMMON /C/ ALFA , BETA , VT , HMDOT ,
* * * * * L , V , THETA ,
* * * * * PHI , GAMMA , CL , SY ,
* * * * * CD , CY , CL , CR ,
* * * * * CM , CN , P , Q ,
* * * * * R , ALFADT , BETADT , PDOT ,
* * * * * QDOT , RDGT , NZ , ALTUDE ,
* * * * * XM , YM , YMDCT , YMDCT
*****
COMMON /F/ PH1 OFFSET , PH2 , PH3 , PH4 ,
* * * * * ALTATT , SGU2PU , MI SDUST
*****

```

```

C      * * * * *
C      LAMDAZ      ,LAMDEL      ,KNFAZ      ,KNFEL
C      NZC         ,PHIC        ,GAMMAC      ,PCCLIM
C      PC          ,QC          ,RC          ,RANGE
C      SIGAZ       ,SIGEL       ,SIGDAF      ,SIGDEF
C      SYT         ,THETAT      ,XT         ,YT
C      HT         ,NYC         ,POPRNG      ,Y
C
C      COMMON /G/  AOA         ,SIDESL      ,FLTPHC
C      BANKC       ,PITCH       ,ROLLRTRC  ,ROLTRIC
C      PTCHRT      ,YAWRT       ,HEADNG      ,FLTPTH
C      HEADT       ,ELEVT       ,DSIGAZ      ,DSIGEL
C      CSGDAZ      ,ERFEL       ,ERFBK      ,ERFRR
C      ERF AZ
C
C      EXECUTABLE $IMTS:
C      * * * * *
C      SET POPLF RANGE AND A PARABOLIC ALTITUDE TRACK
C
C      POPRNG = 15000
C      VH = SCRT(XMDDOT**2+YMDOT**2)
C      ALTATT = HMDDOT*RANGE/VH + (G/2.)*(RANGE/VT)**2 + 10.
C
C      MISSION PHASE LOGIC AND GUIDANCE COMMANDS
C
C      1 IF (PH4.EQ.1) GO TO 40
C      IF (PH1.EQ.1) GO TO 30
C
C      ** INGRESS FROM INITIAL CONDITION TO PCPUP MANEUVER
C
C      IF (RANGE.LT.POPRNG) GO TO 9
C
C      ALTITUDE HOLD
C
C      ALTC = 50.0
C      ALTUDF = ALTUDE
C      GAMMAC = KALT*(ALTC-ALTUDF)/VT
C      GAMMAF = GAMMA
C      AZC = COS(GAMMAF)*KGAMMA*VT*(GAMMAC-GAMMAF)/G
C
C      PFCPCRTIONAL NAVIGATION IN AZIMUTH
C
C      AYC = LAMDAZ*VT*SIGDAF/G
C      PFIC = ATAN2(AYC,AZC)
C      NZC = AZC*CDS(PHI)+AYC*SIN(PHI)
C      GC TO 100
C      PHI = 1
C
C      5

```

```

**      PULLLF TC ATTACK ALTITUDE
C      PROFCRTICNAL NAVIGATION IN AZIMUTH
C
C      ***** PATCH TC RETAIN BTT GUIDANCE TO IMPACT (KTEST=1)
C      KTEST = 1
C      IF(KTEST.EQ.1) GO TO 32
C      ***** ENDPATCH
C      3C      IF(ALTITUDE.GE.ALTTATT) GO TO 39
C
C      32      CONTINUE
C      CCMMAND BALLISTIC ATTACK ALTITUDE
C
C      ALTC = ALTTATT
C      ALTUDF = ALTITUDE
C      GAMMAC = KALTI*(ALTC-ALTUDF)/VT
C      GAMMAF = GAMMA
C      AZC = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
C
C      PROPORTIONAL NAVIGATION IN AZIMUTH
C
C      AYC = LAMDAZ*VT*SIGDAF/G
C      NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C      PHIC = ATAN2(AYC,AZC)
C      GC TO 100
C      PF4 = 1
C
C      39
C
C      **      ATTACK
C      PROFCRTICNAL NAVIGATION IN AZIMUTH AND ELEVATION
C
C      CCMMAND ATTACK ALTITUDE & ROLL TC 90 DEG BANK.
C
C      4C      PHIC = PI/2.
C      ALTC = ALTTATT
C      ALTUDF = ALTITUDE
C      GAMMAC = KALTI*(ALTC-ALTUDF)/VT
C      GAMMAF = GAMMA
C      AZC = KGAMMA*VT*(GAMMAC-GAMMAF)/G
C
C      PROPORTIONAL NAVIGATION IN AZIMUTH
C
C      AYC = LAMDAZ*VT*SIGDAF/G
C      NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C      NYC = AYC*COS(PHI)-AZC*SIN(PHI)
C      NYC = 0.0
C
C      10C CONTINUE
C      *****
C

```

```

C      NZ COMMAND LIMITED TO -2 E +4 G'S; NYC TO +- 0.5 G.
C
C      NZC= LIMIT(-2.0, 4.0,NZC)
C      NYC= LIMIT(-0.5, 0.5,NYC)
C
C      RETURN
C      ENC

```

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